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LOSS OF TAIL ROTOR EFFECTIVENESS EVALUATION OF THE OH-58C HELICOPTER WITH DIRECTIONAL SAS

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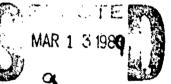
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INTRODUCTION

BACKGROUND

1. Loss of tail rotor effectiveness (LTE) has been a problem with the OH-58 series aircraft and has been identified as a contributing factor in many accidents. In an effort to understand LTE, the U.S. Army evaluated the Bell Helicopter Textron Incorporated (BHTI) model 206 helicopter with a ring-fin configuration (ref 1, app A), the OH-58C helicopter with a 3-axis Stability Control Augmentation System (SCAS) (ref 2), and the JOH-58C with the SFENA 3-axis SCAS and larger tail rotor (ref 3). Army efforts were directed toward a comparative evaluation of the OH-58C with a ring-fin configured tail rotor and with a single-axis directional stability augmentation system (SAS). The OH-58C ring-fin program was terminated prior to completion and the comparative evaluation was canceled. The U.S. Army Aviation Engineering Flight Activity (AEFA) was tasked by the U.S. Army Aviation Systems Command (AVSCOM) to conduct a test program to evaluate the OH-58C helicopter with single-axis directional SAS (ref 4). A test plan (ref 5) was submitted and approved.

TEST OBJECTIVES

2. The objectives of this test were to evaluate the capability of a directional SAS to minimize the occurrence of conditions conducive to encountering LTE and determine the handling qualities of the OH-58C with a directional SAS, increased diameter tail rotor, and engine droop kit installed.

DESCRIPTION

3. The JOH-58C test helicopter, U.S. Army S/N 70-15349, was a modified OH-58C configured with a limited authority (7% of full control travel) directional SAS, manufactured by SPENA Corporation. The OH-58C, manufactured by BHTI, has a single, two-bladed, semirigid, teetering main rotor and a single, two-bladed, delta-hinged, semirigid, teetering tail rotor. Maximum gross weight is 3200 pounds. The aircraft is powered by an Allison T63-A-720 engine with an uninstalled intermediate power rating (30 minutes) of 420 shaft horsepower (shp) at standard sea level conditions, derated to 317 shp (main transmission limit). A detailed description of the standard OH-58C is contained in the operator's manual (ref 6, app A). The test helicopter incorporated the larger tail rotor (65 in. diameter) and the OE-56C engine droop kit product improvement. The helicopter was modified with a SPENA directional SAS is described in appendix B.

TEST SCOPE

4. The LTE evaluation was conducted at Edwards AFB, California (elevation 2302 ft). Twenty-eight flights were conducted for a total of 26.7 productive flight test hours between 23 June and 25 September 1987. Testing was accomplished within the constraints of the airworthiness release (ref 7, app A) and the operator's manual (ref 6).

Handling qualities were evaluated using MIL-H-8501A (ref 8) as a guide. Test conditions are presented in table 1.

TEST METHODOLOGY

5. Flight test data were recorded on magnetic tape using an onboard instrumentation package. A description of test instrumentation is presented in appendix C. Established flight test techniques (ref 9, app A) were used to determine the basic handling qualities of the JOH-58C with directional SAS ON and OFF. Test techniques and data analysis methods are briefly discussed in appendix D. Additional tests were designed to evaluate the capability of the directional SAS to minimize the occurrence of conditions conducive to LTE. The conditions which are conducive to LTE are discussed in the OH-58C operator's manual (ref 6). These include: (a) weathercocking, combined with the inherent yaw characteristic of the aircraft, which results in increasing yaw rates; (b) tail rotor vortex ring state which results in pitch, roll, and yaw excursions; and (c) main rotor disc vortex interference with the tail rotor which results in sudden right yaw rate. These conditions are significantly influenced by aircraft gross weight and density altitude (power margin), low speed flight, and transient rotor speed droop. A Handling Qualities Rating Scale (HQRS) (fig. D-1) and a Vibration Rating Scale (VRS) (fig. D-2) were used to augment pilot comments.

Table 1. Test Conditions¹

Test	Average Gross Weight (lb)	Average Density Altitude (ft)	Trim Airspeed (kt)	Remarks	
			96, 63 KCAS ^a	Level Flight	
Static Lateral-Directional Stability	2890	6110	64 KCAS	MRP Climb	
J			62 KCAS	Autorotation	
Maneuvering Stability	2960	6650	64 KCAS	Left and Right Turns	
	2930	5900	100, 64 KCAS	Level Flight	
Dynamic Stability	2970	38 5 0	0, 10, 20, and 30 KTAS ⁴	Left and right directional pulses at 90, 120, 150, 180, 210, 240 and 270 relative wind azimuth	
Controllability	2910	3120	0, 10, 15 and 20 KTAS	Directional step inputs at 90 and 270 relative azimuth	
	2990	3750	7 to 32 KTAS	Steady heading at relative wind azimuths of 045, 090, 120, 150, 180, 210, 225, 240, 270, 280, 290, 300, 310, 320, 330, 340, 350, and 360. Azimuths 120, 180, and 240 repeated with pilot and copilot doors removed.	
Low Speed Flight	2700	3990	6 to 30 KTAS	Left/right yaw rates of 10 and 20 deg/sec established at 120/240 deg azimuth. Directional control fixed in the weathercock region (120 to 240 deg azimuth)	
Trim Changes with Power	3040	7910	31, 40 and 51 KCAS	SAS OFF only Sideally increments of 10 deg to ±30 deg. Power changes from 93% to 10% engine torque.	
Mission Maneuvers	2850	3020	0 to 100 KCAS	Hover, hover turns, quickstops, takeoffs to hover, landings from hover, stope landings and nap-tif-the earth flight. Performed in moderate to high winds.	

NOTES:

^{*}Tests conducted at mid longitudinal and lateral center of gravity, with SAS both ON and OPF, pilot and copilot doors installed, 109% main rotor speed (354 revolutions per minute) unless otherwise noted.

*KCAS: Knots calibrated airspeed.

*MRP: Maximum rated power.

*KTAS: Knots true airspeed.

RESULTS AND DISCUSSION

GENERAL

6. A loss of tail rotor effectiveness evaluation of the JOH-58C was conducted at Edwards AFB (elevation 2302 feet) at the test conditions listed in table 1. Primary emphasis of the test was to evaluate the handling qualities of the JOH-58C in comparison to the standard OH-58C. The limited authority (7% of full control travel) SAS will not significantly reduce the conditions conducive to encountering LTE. The overall handling qualities of the JOH-58C were moderately improved as compared to the standard OH-58C. Prior testing of the JOH-58C with a 3-axis SCAS installed revealed flying qualities of the JOH-58C were significantly improved in comparison to the standard OH-58C (ref 3, app A). The concept of a SAS which damps uncommanded yaw rates demonstrated potential for reducing the conditions conducive to LTE. However, the limited authority directional SAS saturated at small yaw rates (6 deg/sec) and did not significantly reduce the characteristic high yaw rates and moderate yaw attitude excursions observed in the JOH-58C. As a result, the test was terminated prior to completion of all scheduled tests. The JOH-58C helicopter exhibited moderate pitch, roll, and yaw excursions at 15 to 25 KTAS in azimuths from 240 degrees clockwise to 280 degrees. This characteristic was a shortcoming, upgraded from a deficiency for the standard OH-58 (ref 10). Five additional shortcomings, four of which were previously identified, were noted.

HANDLING QUALITIES

Control System Characteristics

- 7. The mechanical characteristics of the JOH-58C hydraulically boosted flight control system were measured on the ground with the rotors and engine stopped and were qualitatively verified in flight. Hydraulic and electrical power were provided by external sources. All adjustable control friction devices were set to minimum friction. The SAS was ON but had no effect on control system characteristics. Force trim was ON and collective was full down.
- 8. The limits of longitudinal and lateral cyclic control travel are presented in figure E-1. The variation of control position with applied control force for the longitudinal and lateral controls is presented in figures E-2 and E-3. The longitudinal and lateral cyclic control force gradients were positive and essentially linear with no discontinuities. Preakout forces, including friction, were similar to those of the standard OH-58C helicopter Longitudinal centering characteristics were positive but not absolute, resulting in a 0.8-inch longitudinal trim control displacement band. Lateral centering characteristics were positive but not absolute, resulting in a trim control displacement band of 1.3 inches. The large trim control displacement bands increased pilot workload when attempting to maintain desired attitudes during maneuvering flight (para 11). The large longitudinal trim control displacement bands of the JOH-58C remain a chorecoming as previously reported for the standard OH-58C helicopter (ref. 10, app. A).
- 9. The directional control breakout force (including friction) was 4.0 pounds right and 4.5 pounds left. The directional control breakout force (including friction) of the

standard OH-58C was 6.8 pounds right and 5.5 pounds left. The directional control system did not incorporate a force trim mechanism; therefore, no control centering existed. Although there was no directional control centering, the directional control system characteristics are satisfactory. The directional control system characteristics failed to meet the requirements of paragraph 3.3.10 of MIL-H-8501A, in that, there were no positive self-centering characteristics.

Static Lateral-Directional Stability

10. The static lateral-directional stability characteristics of the JOH-58C were evaluated at the conditions listed in table 1. Test results are presented in figures E-4 through E-9. Static directional stability was positive (left directional control required to maintain right sideslip). Effective dihedral was positive for right sideslips (right lateral control required) but approached neutral for left sideslips at most conditions. Side force characteristics were positive (increasing right roll attitude and increasing right sideslip). The directional SAS had no apparent effect on the static lateral-directional stability characteristics. The static lateral-directional stability characteristics of the JOH-58C were similar to the standard OH-58C (ref 10, app A). The pilot had adequate cues of an out-of-trim condition and was able to correct this condition easily. The static lateral-directional stability characteristics of the JOH-58C are satisfactory.

Maneuvering Stability

11. The maneuvering stability characteristics of the JOH-58C were evaluated in left and right steady turns at the conditions listed in table 1. Maneuvering stability data are presented in figure E-10. Maneuvering stability was positive (aft longitudinal control required to maintain increased center of gravity (cg) normal acceleration) at normal accelerations up to 1.4 g and was similar to the standard OH-58C. Maintaining airspeed control within 2 knots at a bank angle of 45 degrees (1.4g) required ±1 inch of longitudinal control displacement. Maintaining bank angle at 45 degrees was difficult because of the aircraft's pitch up divergence ("dig in" tendency), the large longitudinal and lateral trim control displacement bands, and the moderate airframe vibrations (VRS 4). The standard OH-58C had a similar "dig in" tendency and high pilot workload at bank angles of 45 degrees. At all bank angles the pilot workload in the JOH-58C was essentially the same as in the standard OH-58C. No qualitative or quantitative differences were noted SAS ON or OFF. The pitch up divergence at 1.4g or 64 knots calibrated airspeed (KCAS) in the JOH-58C remains a shortcoming as previously reported for the standard OH-58C (ref 10, app A).

Dynamic Stability

Short-Term (Gust Response):

12. The lateral-directional short-term dynamic stability characteristics of the JOH-58C were evaluated at the test conditions listed in table 1. Gusts were simulated by 0.5 second duration directional control pulse inputs of up to 1 inch, directional control doublets, and releases from steady-heading sideslips. The aircraft lateral-directional gust response characteristics were also evaluated in light turbulence. Data for pulses are presented in figures E-11 to E-127. Data for doublets are presented in figures E-128 to E-131. Data for releases from steady heading sideslips are presented in figures E-132 to E-139.

- 13. The short-term rate damping provided by the SAS improved the aircraft's gust response in light turbulence. The lateral-directional gust response observed in forward flight with SAS ON was highly damped. The highly damped lateral-directional response was an improvement over the easily excited lateral-directional oscillations of the standard OH-58C (ref 10, app A). The lateral-directional short-term dynamic stability characteristics of the JOH-58C in forward flight with SAS ON are satisfactory.
- 14. The lateral-directional gust response observed in forward flight with SAS OFF was oscillatory and easily excited. The SAS OFF lateral-directional short-term dynamic stability characteristics of the JOH-58C in forward flight are similar to those previously reported as a shortcoming for the standard OH-58C (ref 10).
- 15. One-inch directional pulse inputs at selected azimuths in low-speed flight were tested with SAS ON with pilot and copilot doors installed and removed. The JOH-58 helicopter response to a simulated gust (pulse input) was characterized by a rapid yaw acceleration. Consequently, moderate yaw rates developed. With SAS ON, these rates resulted in momentary saturation of the SAS actuator and the peak yaw rates were approximately 20 degrees/second. Generally, the aircraft returned to the trim condition following a directional pulse input. However, at the 210 degree relative azimuth at 30 KTAS a right pulse input was characterized by an increasing right yaw and divergence from the trim azimuth (fig. E-95). No qualitative or quantitative differences were observed with the pilot and copilot doors removed. The SAS ON directional gust response in low-speed flight was moderately damped.
- 16. The aircraft was hovered in gusty wind conditions with SAS ON. Rate damping provided by the SAS improved the JOH-58C gust response. Though increased damping provided by directional SAS reduced the yaw attitude excursions in a hover, yaw attitude excursions were greater than 3 degrees and frequent (every second), moderate (±1/4 to 1/2 inch) pedal inputs were required to maintain heading at these conditions (HQRS 5).
- 17. One-inch directional pulse inputs at selected azimuths in low-speed flight were conducted SAS OFF. Maximum yaw rates with SAS OFF were occasionally twice as high as those with SAS ON. SAS OFF aircraft response to the simulated gust was less predictable than with SAS ON, resulting in variable yaw rates. The aircraft seldom returned to the trim azimuth following a pulse input. Figure E-74 shows the variable yaw rate following a right directional polse at 20 KTAS which resulted in divergence from the trim azimuth. No qualitative or quantitative differences were observed with the pilot and copilor doors removed. The SAS OFF shot term dynamic stability characteristics observed in low-speed flight in the yaw axis were lightly damped.
- 18 The aircraft was hovered in gusty wind conditions SAS OFF. Aircraft response while hovering in gusty winds resulted in increasing yaw rates. Frequent (every second), moderate (±1/2 inch) pedal inputs were required to maintain heading within ±3 degrees in a hover (HORS 6).

Long Term:

19. Spiral stability characteristics of the JOH-58C were evaluated by observing aircraft response to control releases from left and right coordinated turns. Data are presented in

figures E-140 to E-147. The JOH-58C exhibited convergent spiral stability in both left and right turns SAS ON and OFF up to 5 degrees of bank. SAS ON, the spiral stability was convergent up to 10 degrees angle of bank. The spiral stability characteristics of the JOH-58C SAS ON and OFF are satisfactory.

20. Longitudinal long term response was evaluated by trimming the aircraft at the desired airspeed and then decreasing airspeed by 10 knots, using only cyclic control. The cyclic was then returned to the trim position and the helicopter response was observed. Time history data are presented in figures E-148 through E-151. The standard OH-58C longitudinal response was convergent and moderately damped and the JOH-58C showed a similar response. At 67 KCAS, SAS ON the aircraft was convergent in all axes. At 101 KCAS, SAS ON or OFF the predominant characteristic was a slowly diverging roll which was easily controlled. The longitudinal long term response of the JOH-58C is satisfactory.

Controllability

- 21. The directional control response (angular rate one second after a one-inch control displacement) and control sensitivity (maximum angular acceleration per one-inch control displacement) of the JOH-58C were evaluated at the conditions listed in table 1. Step inputs during low speed flight were limited to 1/4 inch due to the occurrence of main transmission overtorque during recovery from right yaw rates during a hover.
- 22. Data for directional controllability characteristics are presented in figures E-152 through E-157. The aircraft responded in the proper direction within 0.2 seconds after the input and no objectionable coupling was noted. The JOH-58C with SAS ON had increased yaw rate damping as compared to the standard Off-58C (ref. 10, app. A). However, SAS was quickly saturated and the high control sensitivity was similar to SAS OFF sensitivity. Yaw rate continually increased until recovery was initiated. Directional response was satisfactory during recovery but a tendency to overcontrol was noted at the 270 degree azimuth. At the moderate gross weights tested, increasing yaw rates and insufficient power margin required increased pilot attention to torque limits. Moderate (±1/2 inch) but smooth directional control movements were required to arrest right yaw rates. No repeatable data were obtained during controllability tests above 15 KTAS at the 270 degree aximuth due to frequent SAS saturation and the ±1/4 to 1/2 inch directional control inputs required to maintain trim conditions. The directional controllability characteristics of the JOH-58C with SAS OFF were characterized by more rapid accelerations in the yaw axis, and were similar to the standard OH-58C which were reported as a shortcoming. The high control sensitivity SAS ON and OFF resulting in directional overcontrol remains a shortcoming in the JOH-SSC.

Low-Speed Flight Characteristics

General:

23. Low-speed flight characteristics were evaluated to determine the effects on handling qualities due to the installation of the directional SAS, larger tail rotor, and engine droop kit. Low-speed flight testing was conducted to simulate hovering in winds by stabilizing in formation with a calibrated ground pace vehicle at a skid height of approximately 10 feet

at relative azimuths (measured clockwise from the nose of the aircraft) from 0 degrees to 350 degrees. The low-speed flight characteristics for this aircraft will be discussed by reference to one of three regions (fig. A): 290 degrees clockwise to 120 degrees (region A), 120 degrees clockwise to 240 degrees (region B) and 240 degrees clockwise to 290 degrees (region C). Additional low speed tests were conducted by initiating a left or right yaw rate and maintaining fixed directional and collective controls while in the weathercock stability region (120 to 240 deg). Upon reaching the region boundary, recovery was initiated.

24. HQRS were assigned in accordance with the scale in figure D-1 to describe the pilot workload to conduct a simulated mission task of hovering in winds. The standards for desired mission performance required maintaining the aircraft within ±3 degrees of desired heading and ±2 feet of desired skid height. Although the HQRS may be different for actual hover in winds (as opposed to the simulated task) the ratings are useful for quantifying the effects on pilot workload of the SAS and of varying wind speed and direction. Tests were conducted SAS ON and OFF at the test conditions listed in table 1. Low-speed flight characteristics data are presented in figures E-158 through E-208. No qualitative or quantitative differences were observed with the pilot and copilot doors removed. Figure B shows a HQRS summary for azimuths tested in low-speed flight.

Region A:

25. At 3410 feet, the JOH-58C had 30% margin remaining at 30 KTAS with SAS ON or OFF (fig. E-162 and E-163). Wind tunnel tests have shown main rotor vortex interference with the tail rotor to occur between 10 and 20 knots from the 280 to 320 azimuth (ref 10, app A). Although directional control excursions were small (±1/4 inch) from 290 to 300, large longitudinal cyclic trim changes were required. At the 300 degree azimuth there was a large (1 inch) aft longitudinal cyclic trim change required as airspeed was increased from 20 to 25 KTAS. A similar longitudinal trim change was observed at the 290 azimuth at 25 KTAS SAS ON and 30 KTAS SAS OFF. These large aft longitudinal trim changes were not observed at the 310 or 280 azimuths. The SAS ON handling qualities in region A from 290 degrees to 120 degrees were improved from the standard OH-58C (ref 10). The low speed handling qualities of the JOH-58C aircraft in Region A with SAS ON are satisfactory.

Region B.

26. In rearward flight (Region B), SAS ON handling qualities ratings were improve i from HQRS 5 (standard OH-58C) to HQRS 3 to 4. Only occasional moderate directional control inputs (±1/4 to 1/2 inch) were required to maintain the desired performance criteria (para 24). Excessive pitch and yaw excursions in rearward flight in the standard OH-58C were previously reported as a deficiency (ref. 10). The pilot workload in the directional axis (as indicated by directional control excursions) with the SAS ON was significantly reduced in the JOH-58C. The maximum workload occurred at the 225 azimuth at 25 KTAS (fig. E-170). The high pilot workload in the longitudinal axis (±1 inch longitudinal cyclic inputs) at the 325 degree azimuth from 10 to 20 KTAs

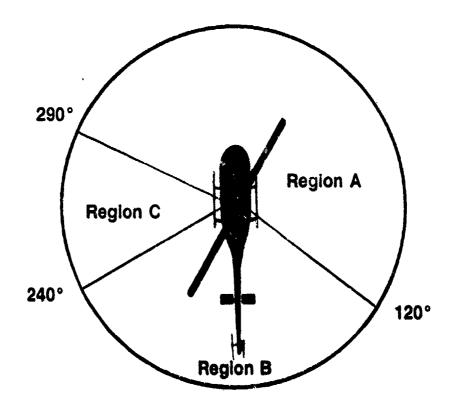


Figure A. Low Speed Flight Regions

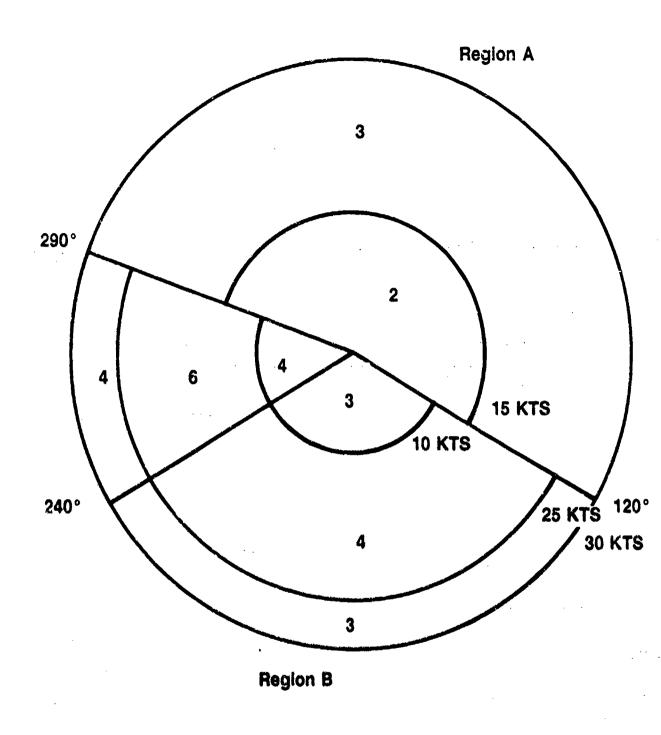


Figure B. SAS ON HQR Summary for Low Speed Flight

was similar to that reported in rearward flight in the standard OH-58C. Additionally, a large aft longitudinal cyclic trim change was required to maintain a 5 knot speed increase above 10 KTAS. The high pilot workload in the longitudinal axis in rearward flight from 10 to 20 KTAS is a shortcoming. Consideration should be given to installation of a SAS in more than one axis to improve the rearward flight handling qualities of the JOH-58C.

- 27. In addition to evaluating handling qualities in steady heading, constant airspeed flight, the following technique was used to simulate hovering turns in winds. Yaw rates of approximately 10 degrees/second and 20 degrees/second were established prior to entering the weathercock stability region (region B); then, directional and collective controls were fixed until recovery was initiated at the region boundary. Data are presented in figures E-193 through E-208. The limited authority (7% of full control travel) directional SAS was saturated at yaw rates greater than 6 degrees/second. Consequently, SAS was saturated at the initial trim conditions for these tests. Current Aircrew Training Manual (ATM) (ref 11, app A) standards require constant rate hover turns not to exceed 22.5 degrees/second. SAS would be almost continuously saturated during hover turns operationally.
- 28. Right yaw rates at 10 KTAS with SAS ON or OFF resulted in a continued right yaw rate which decreased to approximately 5 degrees/second when passing the 180 degree relative azimum. Upon reaching the 150 degree azimuth, a rapid right yaw acceleration occurred which resulted in a var rate of approximately 50 degrees/second at the recovery azimuth of 120 degrees. Recovery at the 120 degree azimuth with a right yaw rate of 50 gegrees/second (slowest observed) resulted in a 10 degree overshoot with SAS ON. Recoveries at the 120 azimuth were not further attempted due to the increased torque requirements and possibility of a main transmission overtorque. The recovery technique developed to prevent overtorque was to increase left pedal gradually, arresting the yaw rate at 360 degree azimuth (aircraft aligned in the direction of travel). At 15 KTAS, a 10 degrees/second right yaw rate with SAS ON and 20 degrees/second rate SAS ON or OFF were similar to the response at 10 KTAS. Flowever, the 10 degree/second right yaw rate with SAS OFF resulted in the yaw rate decreasing to zero at approximately 230 degrees relative azimuth, then an accelerating left yaw rate developed which was arrested easily at the 360 degree relative azimuth. At 20 KTAS, a 20 degree/second right yaw rate with SAS ON resulted in a response similar to the response at 10 KTAS. All other initial right yaw rates at 20 KTAS SAS ON and OFF resulted in a slight overshoot of the 240 degree azimuth followed by an acciderating left yaw rate which was easily arrested as the aircraft aligned in the direction of travel. No attempt to recover the resultant left yaw rate was made prior to the 360 degre-relative azimuth. SAS appeared to assist in maintaining trim yaw rate as evidenced by the delayed onset of the resultant left yaw rate which occurred with increasing airspeads. During this test, large cyclic trim changes were required to maintain desired speed. Passing from 210 through 150 degrees relative azimuth required approximately 2 inches of aft cyclic followed by approximately 2 inches of forward cyclic at the 120 degrees relative azimuth. An additional 1 to 2 inches of forward cyclic were used during recoveries in the direction of travel to maintain desired speed. Although SAS remained saturated through most of this test, the limited authority directional SAS appeared to assist in maintaining desired trim conditions. While attempting to maintain a constant turn rate in a right pedal spot turn,

with SAS ON, in winds of 10 to 12 knots, the pilot was frequently required to make left and right, moderate ($\pm 1/4$ to 1/2 inch) pedal inputs and occasionally required to make large (± 1 inch) pedal inputs (HQRS 5). The longitudinal cyclic trim change required to remain within 2 feet of a spot during a pedal turn was large (± 3 inches). Low speed flight effects on right yaw rates in the weathercock stability region were rapid right yaw accelerations from the 150 to 120 degree azimuths and decreasing right yaw rates from the 240 to 150 degree azimuths.

29. Left yaw rates SAS ON or OFF resulted in progressively increasing left yaw rates from 120 to 210 degrees. An extremely rapid left yaw acceleration occurred at the 210 azimuth. At 16 KTAS, recovery was accomplished at 10 degrees beyond the region boundary SAS ON and OFF. During application of right pedal to arrest yaw rate, a rapid, approximately 10 degree nose down pitch occurred. Recovery at the region boundary with speeds greater than 10 KTAS was not attempted due to the large (greater than ±30 percent) torque changes required and rapid pitch rate observed during recovery at 15 KTAS SAS ON. Instead, recovery was initiated at the region boundary and was completed by the 360 degree azimuth (direction of travel). No significant differences were noted SAS ON or OFF above 10 knots. At airspeeds greater than 10 KTAS and at the instant the yaw acceleration at the 210 azimuth was experienced, the Master Caution and Engine Oil Bypass Lights illuminated for approximately 1 second. Although the engine oil reservoir was fully serviced, severe sloshing of the oil probably caused activation of the caution lights. During left hover spot turns in winds of 10 to 12 knots, multiple left and right pedal inputs (±1/2 inch) were required in an attempt to maintain a constant turn rate with SAS ON. As the aircraft approached the 090 degree relative azimuth, larger (1 inch) left pedal inputs were required in an attempt to maintain the turn. Approaching the 210 degree relative azimuth required larger (1 inch) right pedal inputs to prevent an accelerating left turn. Throughout the maneuver, large longitudinal cyclic trim changes were required to remain within 2 feet of the spot. Low speed flight effects on left yaw rates in the weathercock stability region were increasing left yaw rates from the 120 to 210 degree azimuths and rapid left yaw acceleration from the 210 to 240 degree azimuth.

Region C:

30. In left sideward flight (Region C) yaw attitude excursions of ± 8 degrees observed in the standard OH-58C (reported deficiency, ref 10, app A) were reduced in the JOH-58C with SAS ON. HQRS for 15 to 25 KTAS were HQRS 6 (compared to HQRS 7 in the standard OH-58C), while all other speeds improved to HQRS 4. Moderate pitch, roll, and yaw excursions required moderate-sized control inputs to accomplish the simulated hover task. However, smaller and less frequent pedal inputs were required as compared to the standard OH-58C. Critical azimuths and airspeeds, determined by pilot workload, were 240 to 280 degrees at 15 to 25 KTAS. Large SAS actuator inputs as well as moderate-sized, frequent control inputs in all axes ($\pm 1/4$ -inch directional and $\pm 1/2$ -inch lateral and longitudinal) were required to achieve only adequate performance (HQRS 6). The directional SAS, improved tail rotor system, and engine droop kit moderately improved the low speed flight characteristics of the JOH-58C in Region C, however, workload remains high at the critical azimuths and airspeeds. The moderate pitch, roll,

and yaw excursions between 15 and 25 KTAS at relative wind azimuths between 240 and 280 degrees are a shortcoming.

All Regions with SAS OFF:

31. Low speed SAS OFF flight data are presented in figures E-159 through E-189. Larger and more frequent control inputs were required for all azimuths and airspeeds tested than were required with SAS ON. Qualitatively and quantitatively the directional control was more sensitive than the standard OH-58C. Except for increased directional sensitivity, the handling qualities of the JOH-58C with SAS OFF were similar to the standard OH-58C.

Trim Changes with Power Effects

32. Trim directional control requirements as a function of power were evaluated in an attempt to determine the conditions resulting in main rotor disc vortex interference with the tail rotor. Tests were conducted at the conditions listed in table 1. Results are presented in figures E-209 through E-216. Generally, decreasing engine power required increasing right directional control at all trim airspeeds and sideslips. At all trim airspeeds and sideslips, directional trim changes at 80% and 35% engine torque were accompanied by large (±10 degrees) sideslip excursions and required restabilizing on desired trim sideslip prior to further power reduction. The characteristic directional trim changes for right sideslips were similar at all airspeeds and power settings. The characteristic directional trim changes for left sideslips showed increasing left pedal requirements with decreasing airspeed at all power settings. Though accuracy of sideslip beyond 35 degrees and airspeed below 30 KCAS could not be determined due to instrumentation limitations. a significant directional trim discontinuity was observed at 20 KCAS with approximately 40 degrees left sideslip. Rapid right yaw accelerations requiring frequent large (1 inch) pedal inputs to remain ±10 degrees of desired sideslip occurred between 70 and 85% engine torque. Buffeting of the tail was felt by the pilot through the airframe. The right yaw accelerations and buffeting did not occur below 70% engine torque. No engine torque setting above 85% was attempted due to the possibility of main transmission overtorque when arresting the right yaw accelerations. On a subsequent flight, this significant trim discontinuity was not observed under similar conditions. Figure E-216 shows a time history of this occurrence. Directional trim changes with power did not provide sufficient data to determine the area of main rotor disc vortex interference with Recommend alternate methods of determining main rotor vortex interference be investigated using more accurate measurements of low airspeed, sideslip, and tail boom loads.

Mission Maneuvering Characteristics

33. Mission maneuvers were qualitatively evaluated in the JOH-58C at the conditions listed in table 1. Time histories of some maneuvers are presented in figures E-217 through E-254. The maneuvers were conducted in accordance with the OH-58 helicopter ATM (ref 11, app A) and were evaluated SAS ON and OFF. Pilot workload increased with the SAS OFF for all maneuvers conducted. Aircraft controllability was not in question, but SAS OFF flight required increased pilot compensation to maintain the ATM

standards of each maneuver. SAS ON flight, however, reduced pilot workload which enhanced mission capability. Slope landings, masking/unmasking and nap-of-the-earth flight were easier to accomplish in the JOH-58C than in the standard OH-58C because rate damping reduced aircraft yaw attitude excursions. Hovering in actual winds was moderately improved with SAS ON. The occasionally saturated SAS resulted in moderate yaw excursions at the critical azimuth from 15 to 25 KTAS. An OGE hover spot turn of approximately 10 degrees/second to the left resulted in a rapid left yaw acceleration when passing the 270 degree relative azimuth. Approximately 2 inches of right pedal were required to arrest the increasing yaw rate. The mission maneuver characteristics of the JOH-58C helicopter with a directional SAS improved mission capability. The limited authority (7% of full control travel) directional SAS was occasionally saturated during hover with a left crosswind and always saturated during maneuvers requiring yaw rates greater than approximately 6 degrees/second.

Directional SAS Effects

34. The effect of a directional SAS was to provide increased yaw rate damping which improved aircraft gust response (paras 13 and 16). However, the limited authority SAS saturated at low (6 degrees/second) yaw rates. The characteristic of the hovering aircraft with wind in the weathercock region is rapid yaw accelerations SAS ON and OFF from 150 to 120 and 210 to 240 relative wind azimuths (paras 26 and 27). In the region of tail rotor vortex ring state the aircraft demonstrated moderate pitch, roll, and yaw excursions with SAS ON and OFF (para 28). Sufficient data to define the area of main rotor disc vortex interference with the tail rotor were not obtained (para 32). Additionally, the small power margin remained a significant factor when arresting yaw rates despite testing at weights below 3000 lb (maximum gross weight is 3200 lb) and low density altitudes. The concept of a SAS which damps uncommanded yaw rates demonstrates potential for reducing the conditions conducive to LTE. However, the limited authority (7% or full control travel) directional SAS saturated at small yaw rates (6 degrees/second) and did not significantly reduced the characteristic high yaw rates of moderate yaw attitude excursions observed in the JOH-58C.

MISCELLANEOUS

Cockpit Evaluation

35. The ease of the inadvertent main transmission overtorque or engine overtemperature condition was previously reported as a shortcoming (ref. 10, app. A). With the improved tail rotor and engine droop modifications applied, the aircraft is more responsive to pedal or directional SAS inputs. Consequently, with the pilot's attention directed consider the cockepit during NOE flight, an increased engine and tail rotor response will result in an increased possibility of an overtorque or overtemperature condition. The ease of main transmission overtorque or engine overtemperature condition in the OH-58C remains a shortcoming in the JOH-58C.

Aircraft Pitot-Static System Calibration

36. The helicopter pitot-static system was calibrated in level flight, climbs, and autorotations using the trailing bomb technique. Data are presented in figure E-255. The position error of the JOH-58C helicopter was similar to the standard OH-58C. The JOH-58C ship airspeed system was satisfactory.

CONCLUSIONS

GENERAL

- 37. The following conclusions were reached upon completion of testing.
- a. The limited authority SAS will not significantly reduce the conditions conducive to encountering LTE.
- b. The limited authority directional SAS does not significantly reduce the characteristic high yaw rates and moderate yaw attitude excursions in the JOH-58C.
- c. The flying qualities of the JOH-58C were moderately improved in comparison to the standard OH-58C.
- d. The concept of SAS which damps uncommanded yaw rates demonstrates potential for reducing the conditions conducive to LTE.

SHORTCOMINGS

- 38. The following shortcoming was previously identified as a deficiency in the standard OH-58C: Moderate pitch, roll, and yaw excursions between 15 and 25 KTAS at relative wind azimuths between 240 and 280 degrees (para 30).
- 39. The following shortcoming was previously reported as high pilot workload: The high pilot workload in the longitudinal axis in rearward flight at 10 to 20 KTAS (para 26).
- 40. The following shortcomings were previously identified in the OH-S8C and remain shortcomings:
- a. Ease of main transmission overtorque or engine overtemperature condition (para 35).
 - b. The high control sensitivity resulting in directional overcontrol (para 22).
- c. Pitch up divergence ("dig in" tendencies) at load factors near 1.4g at 64 KCAS (para 11).
 - d. Large longitudinal and lateral trim control displacement bands (para 8).

SPECIFICATION COMPLIANCE

41. The JOH-58C failed to meet the requirement of paragraph 3.3.10 of MIL-H-8501A in that there were no positive self-centering characteristics for the directional control system (para 9).

RECOMMENDATIONS

- 42. The following recommendations were made:
- a. The shortcomings reported in paragraphs 38, 39, and 40 should be corrected as soon as possible.
- b. Consideration should be given to installation of a SAS in more than one axis to improve the rearward flight handling qualities of the JOH-58C (para 26).
- c. Alternate methods of determining main rotor vortex interference should be investigated using more accurate measurements of low airspeed, sideslip, and tailboom loads (para 32).

APPENDIX A. REFERENCES

- 1. Final Report, AEFA Project No. 83-12, Government Pilot Evaluation of the BHTI 206/Ring Fin Tail Rotor, January 1985.
- 2. Final Report, AEFA Project No. 83-15, Preliminary Airworthiness Evaluation of the OH-58C with 3-Axis Stability Control Augmentation System and Improved Tail Rotor, October 1983.
- 3. Final Report, AEFA Project No. 85-03, Airworthiness and Flight Characteristics of the JOH-58C (OH-58X Surrogate Helicopter), February 1986.
- 4. Letter, AVSCOM, AMSAV-8, 29 December 1986, subject: Loss of Tail Rotor Effectiveness (LTE) Evaluation of the OH-58C with Directional SCAS ONLY Operable. (Test Request)
- 5. Test Plan, AEFA Project No. 86-22, Loss of Tail Rotor Effectiveness (LTE) Evaluation of the OH-58C with Directional SCAS, January 1987.
- 6. Operator's Manual, TM 55-1520-235-10, Army OH-58C Helicopter, 7 April 1978, with change 40, 21 November 1986.
- 7. Letter, AVSCOM, AMSAV-E, 23 January 1987, with revision 4 dated 15 June 1987, subject: Airworthiness Release for JOH-58C, S/N 70-15349 for the Directional SCAS/Tail Rotor Boost Evaluation and HICAP Instrumentation Evaluation.
- 8. Military Specification, MIL-H-8501A, Helicopter Flying and Ground Handling Qualities; General Requirements for, 7 September 1961, with amendment 1, 3 April 1962.
- 9. Flight Test Manual, Naval Air Test Center, FTM No. 104, Stability and Control, 10 November 1983.
- 10. Final Report, AEFA Project No., 76-11-2, Airworthiness and Flight Characteristics Evaluation of the OH-58C Interim Scout Helicopter, April 1979.
- 11. Aircrew Training Manual (ATM), FC1-215, Observation Helicopter OH-58, 30 October 1984.
- 12. Aviation Unit and Intermediate Maintenance Manual, OH-58A and OH-58C, TM 55-1520-228-23-1, dated 4 August 1978, with change 39, 1 December 1985.

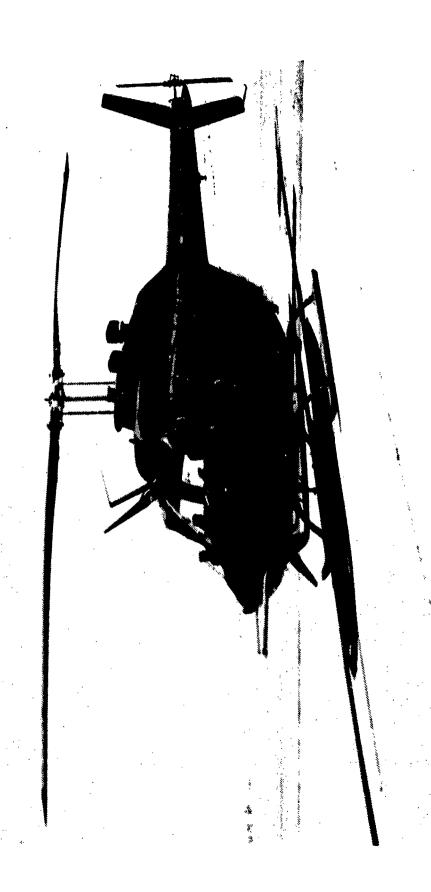
APPENDIX B. AIRCRAFT DESCRIPTION

- 1. The test helicopter, JOH-58C US S/N 70-15349, was a standard OH-58C (built by Bell Helicopter Textron, Inc. (BHTI)), modified with a SFENA directional Stability Augmentation System (SAS). The standard OH-58C has a single two-bladed, semirigid, teetering main rotor and a single two-bladed, delta-hinged, semirigid, teetering tail rotor. A detailed description of the OH-58C is included in the operator's manual (ref 6, app A). The major aircraft modifications included the Bell 206L-3 tail rotor (65 in. diameter) with accompanying drive shafting and gearbox (modification work order (MWO) 55-1520-228-50-25), the engine droop kit (MWO 55-1520-228-50-26), and the directional SAS. Figure B-1 shows the test aircraft. Figures B-2 and B-3 show the SAS cockpit controls. Figure B-4 shows the internally mounted test instrumentation.
- 2. The test helicopter was weighed by the U.S. Army Aviation Engineering Flight Activity (AEFA) personnel prior to testing. The weight and longitudinal center of gravity (cg) data were 2313/114.49, no fuel and 2770/114.87 full fuel.
- 3. A complete flight control rigging check was performed by AEFA quality control personnel prior to the initiation of testing. All flight control rigging was within tolerances specified in reference 7, appendix A. The data for the tail rotor rigging check is presented below:

Tail Rotor	Left	22 degrees 54 minutes		
rait Rotor	Right	-8 degrees 36 minutes		

Rigging was accomplished in accordance with the rigging procedures specified in reference 12 except that hydraulic power was applied, the directional SAS actuator was centered, and electrical power was OFF.

- 4. The improved tail rotor (MWO 55-1520-228-50-25) is depicted in figure B-5. It incorporates the same airfoil section as the standard OH-58C tail rotor but the diameter is increased by 3 inches to 65 inches. Maximum pitch angle values are increased to the values shown in paragraph 3. The tail rotor drive shafting and geatbox were changed per the MWO. The drive shaft is a seven piece shaft (fig. B-6). Each piece in the shaft is identical and has a larger diameter than the one-piece standard drive shaft. The tail rotor gearbox continuous rating is increased from 65 to 85 shaft horsepower.
- 5. The JOH-58C had a limited-authority (7% of full control travel), prototype single-axis SAS. The SAS uses a rate gyro computer and actuator to provide rate damping in the directional axis. No attitude retention or attitude hold feature was included in the system tested. Force trim was not provided in the directional controls. The directional SAS includes the following components:



20



Figure B-2. Cyclic Grip with SAS On/Off Switch

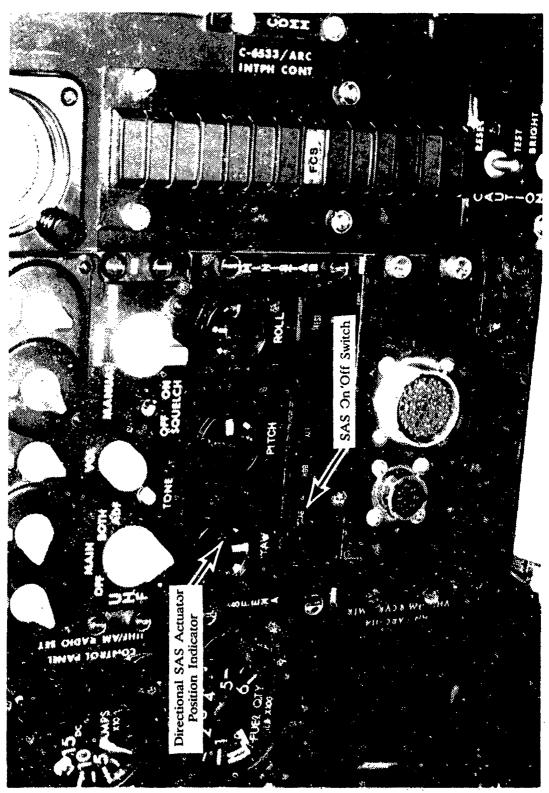


Figure B-3. Instrument Panel SAS Controls



Figure B-4. Test Instrumentation Installation

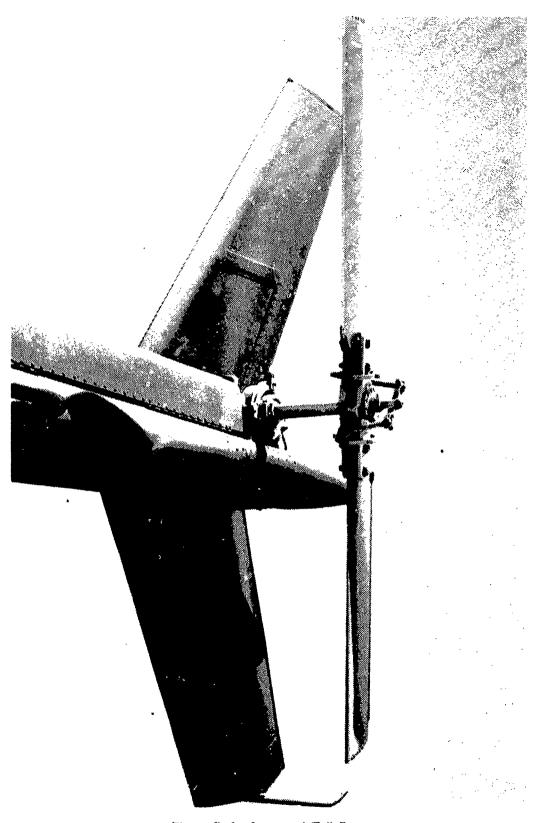


Figure B-5. Improved Tail Rotor

Figure B-6. Tail Rotor Drive Shaft

ITEM PART NUMBER QUANTITY	LOCATION
SAS Computer 75258V1M2 1	Avionics Compartment
Directional rod/	
actuator assy 10110-001 1	Entrance to tail boom
Air data computer 10980-002 1	Passenger compartment
Junction Box	Passenger compartment
Yaw Stop Assy 11530 1	Entrance to tail boom
SAS control panel K28AJM 1	
Pre-Fabricated Harness	•
yaw 11368 1 1	Passenger compartment
50 VA Inverter PC 50 1	
Hydraulic/boosted	• • • • • • • • • • • • • • • • • • • •
T/R/Assy 206-001-739-7 1	Entrance to tail boom
Actuator Position	
Indicator X60ACM 1	Instrument Panel

These components were designed for the SFENA 3-axis SAS and therefore the connections were modified for the directional-only configuration.

- 6. A SAS computer for the directional axis incorporates logic and gain networks to provide rate damping. A rate gyro in the computer senses changes of angular rate of 0.01 degree/second.
- 7. The SAS control panel is shown in figure B-3. The panel includes a Force Trim button, a STAB button (SAS ON/OFF), a button to engage altitude hold and a system test switch. Only the STAB button was functional for this test. Directional SAS actuator position is indicated on the yaw galvanometer.
- 8. The SAS power distribution system requires 28V DC, 26V AC and 115V AC single-phase electrical power. The 115V AC, 400 Hz, single-phase power, provided by the upgraded solid state inverter, is for the rate gyro motor and for the computer internal power supplies. The rate gyro output signal is demodulated and applied to a servo amplifier which drives the rate (damping) channels. When the system is OFF, resulting in a zero signal to the servo amplifier, the actuator centers. The actuator is mounted in a directional control tube and contains a DC permanent magnet motor driven by a pulse-width modulating type of servo-amplifier. The ±27V motor drive voltage and the ±15V feedback pot excitation voltage are derived in the computer power supply.
- 9. The SAS uses a single actuator mounted in series with the directional control tubes. The actuator has low force output and is used in conjunction with the hydraulically boosted control. The actuator is installed as close as possible to the input valve of the hydraulic booster to isolate the actuator motion from the pilot controls. The mass and friction on the booster side of the actuator is low compared to the pilot's side of the actuator. The SAS actuator stroke is limited to give 6.79% (of full control travel) SAS authority (approximately ±0.34 in.).
- 10. A SAS ON/OFF switch is located on the pilot cyclic grip as shown in figure B-2. If the switch is depressed, SAS will engage or disengage.
- 11. The force trim system is the standard OH-58 force trim system. However, the force trim ON/OFF switch is relocated to the position shown in figure B-3. The thumb button

on the pilot/copilot cyclic stick (fig. B-2) is used for momentary force trim release. There is no force trim in the directional axis.

- 12. A flight control system (FCS) caution light is provided in the segmented caution panel. When the SAS is disengaged, the series actuator automatically centers and the FCS caution light illuminates momentarily. The FCS light does not illuminate, however, if a SAS failure occurs.
- 13. SAS operation is accomplished by pressing the STAB button on the SAS control panel or the SAS ON/OFF switch located on the pilot's cyclic grip. SAS operation is monitored using the yaw actuator position indicator (fig. B-3).
- 14. Prior to flight, a system self-test may be performed. With the SAS OFF, the TEST button is depressed. The test button should light the "1" on the test button. The STAB indicator will show green stripes, the ALT indicator will show red stripes. The FCS caution light will illuminate and the three actuator position indicators will be centered. Position "1" tests only the system indicators. When the TEST button is depressed a second time, the "2" illuminates. The STAB and ALT indicators are initially black. Position "2" tests the system amplifiers and input/output logic. When the STAB indicator is depressed, the green stripes reappear. FCS caution light remains illuminated and the actuator position indicators remain centered. When the test button is depressed a third time to the "0" position, the STAB indicator remains green, the FCS caution light extinguishes. The SAS is then operational for flight.
- 15. The SAS operates normally when the STAB button or the pilot's SAS ON/OFF switch on the cyclic is depressed. Green and white diagonal stripes appear in the STAB indicator, indicating that power is applied to the system and rate damping is in effect. Attitude retention was not incorporated in the system modified for this test.
- 16. The FCS caution light and master caution light illuminate momentarily when the SAS is disengaged. the FCS caution light does not illuminate when the SAS fails.
- 17. The SAS is disengaged by depressing the STAB button. The SAS can also be disengaged by depressing the SAS ON/OFF switch on the pilot's cyclic. Disengagement does not remove power from the system gyro computer.

APPENDIX C. INSTRUMENTATION

- 1. The test instrumentation system was designed, calibrated, installed, and maintained by the U.S. Army Aviation Engineering Flight Activity. Digital and analog data were obtained from calibrated instrumentation and were recorded on magnetic tape and/or displayed in the cockpit. The instrumentation system consisted of various transducers, signal conditioning units, a 12-bit pulse code modulation encoder, and an Ampex AR 700 tape recorder. Time correlation was accomplished with an onboard, recorded and displayed, Inter-Range Instrumentation Group B format time of day. Various specialized test indicators displayed data to the pilot and engineer continuously during the flight. A boom with the following sensors was mounted on the nose of the aircraft: swiveling pitot-static head, sideslip vane and angle-of-attack vane. The boom airspeed system calibration is shown in figure C-1.
- 2 The following parameters were displayed on calibrated instruments in the cockpit:

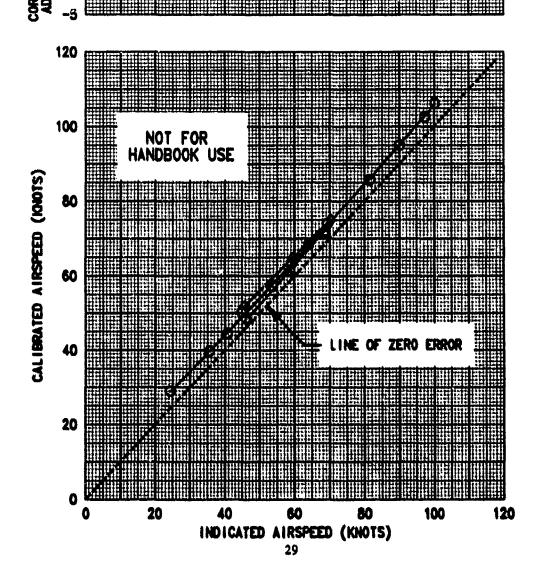
Airspeed (boom)
Airspeed (ship)
Altitude (boom)
Altitude (ship)
Rotor speed
Engine torque
Turbine outlet temperature
Fuel flow rate
Fuel used (totalizer)
Outside air temperature
Normal acceleration
Angle-of-sideslip
Time of day
Record counter

3. The following parameters were recorded on magnetic tape:

Time code Record number Fuel used Airspeed (boom) Altitude (boom) Airspeed (ship) Altitude (ship) Main rotor speed Outside air temperature Angle-of-sideslip Angle-of-attack Engine torque Turbine outlet temperature Gas producer speed Power turbine output shaft speed Fuel flow rate

FIGURE C-1 BOOM SYSTEM AIRSPEED CALIBRATION JOH-58C USA S/N 70-15349

SYM	AVG GROSS WEIGHT (LB)	AYG LOCAT LONG (FS)		AVG DENSITY ALTITUDE (FT)	AVG OAT (DEG C)	AVG ROTOR SPEED (RPM)	FLIGHT CONDITION
⊙ ♦	2940 2880 2900	108.1 107.8 107.9	0.0 0.0 0.0	6020 5980 5920	20.5 20.5 20.5	354 354 354	LEVEL CLIMB AUTOROTATION
LLI.	10	NOTES:	2. TRAI	IGURATION: LING BOMB I	CLEAN, DO	ors on	
ON TO BE KNOTS)	5						



Control positions Longitudinal

Lateral

Directional

Collective

Aircraft attitudes and rates

Pitch

Roll

Yaw

Aircraft vertical center of gravity acceleration Directional SAS actuator position

APPENDIX D. TEST TECHNIQUES AND DATA ANALYSIS METHODS

GENERAL

- 1. Stability and control data were collected and evaluated using standard test methods as described in reference 9, appendix A. Definitions of deficiencies and shortcomings used during this test are shown below.
- a. Deficiency. A defect or malfunction discovered during the life cycle of an item of equipment that constitutes a safety hazard to personnel; will result in serious damage to the equipment if operation is continued; or indicates improper design or other cause of failure of an item or part, which seriously impairs the equipment's operational capability.
- b. Shortcoming. An imperfection or malfunction occurring during the life cycle of equipment which must be reported and which should be corrected to increase efficiency and to render the equipment completely serviceable. It will not cause an immediate breakdown, jeopardize safe operation, or materially reduce the usability of the material or end product.

Airspeed Calibration

2. The boom and ship's pitot-static systems were calibrated using the trailing bomb method to determine the airspeed position error. Calibrated airspeed (V_{cel}) was obtained by correcting indicated airspeed (V_l) using instrument (ΔV_{lc}) and position (ΔV_{pc}) error corrections.

$$V_{col} = V_i + \Delta V_{ic} + \Delta V_{Bc} \tag{1}$$

Aircraft Weight and Balance

- 3. Prior to testing, the aircraft gross weight and center of gravity (cg) location were determined using calibrated scales. The aircraft was weighed with full instrumentation onboard and without fuel. The aircraft weight was 2313 pounds with a longitudinal cg location at fuselage station 114.49. A fuel cell, site gage, and cockpit fuel gage calibration was accomplished. The fuel weight for each test flight was determined prior to engine start by using the calibrated sight gage.
- 4. The Handling Qualities Rating Scale presented in figure D-1 was used to augment pilot comments relative to handling qualities and workload.
- 5. The Vibration Rating Scale presented in figure D-2 was used to augment pilot comments relative to vibrations.

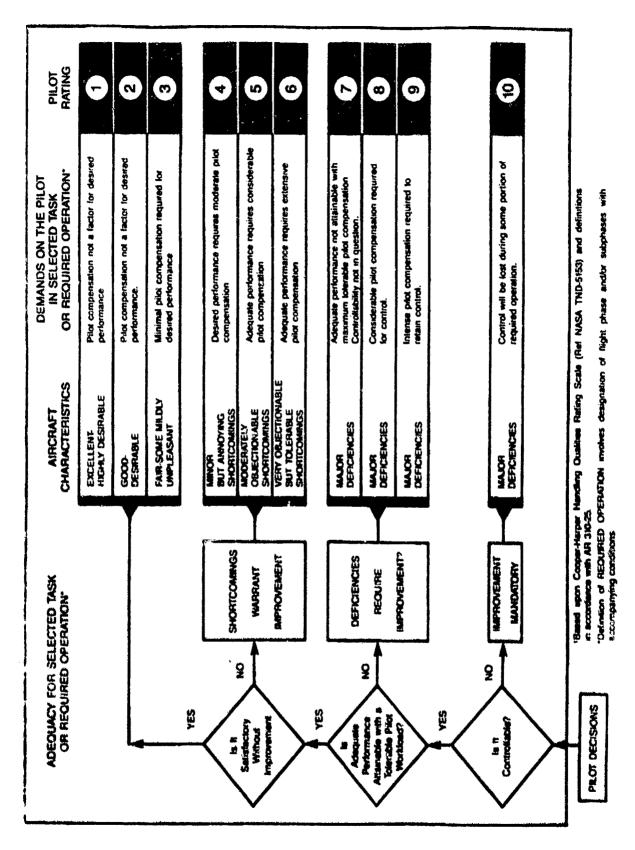
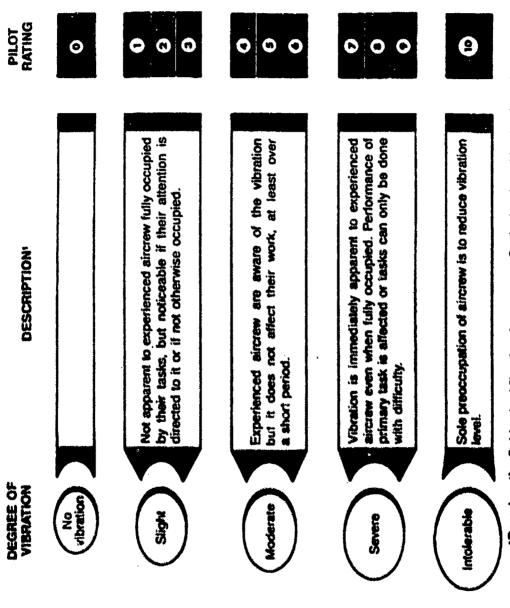


Figure D-1. Handling Qualities Rating Scale



'Based on the Subjective Variation Assessment Scale developed by the Aeroplane and Armament Experimental Establishment, Boscombe Down, England.

Figure D-2. Vibration Rating Scale

HANDLING QUALITIES

Control System Characteristics

6. These tests were conducted on the ground with hydraulic and electrical power provided by ground power units. A hand-held force gauge was used to measure the force required to move the cyclic control in incremental displacements to the limits of travel. Hysteresis was checked by taking measurements in the increasing and decreasing force directions. The force gauge was also used to measure the force required to move the directional and the collective controls in incremental displacements to the limits of travel in both directions.

Static Lateral-directional Stability

7. These tests were accomplished by trimming the aircraft in coordinated flight at the desired conditions. With collective control fixed, the aircraft was then stabilized at incremental sideslip angles up to 20 degrees left and right of trim while maintaining steady heading at the trimmed airspeed.

Maneuvering Stability

8. The variation of longitudinal control position and force with normal acceleration was determined during steady turns. The test consisted of incrementally increasing normal acceleration (load factor) while holding collective position constant. Steady turns, in both directions, were accomplished by stabilizing and trimming in level unaccelerated flight at the desired test airspeed. Load factor was increased by incrementally increasing bank angle. Ball-centered, constant airspeed, and fixed collective control were maintained during the turn. Rotor speed was not adjusted during the turn. Data were gathered within 1000 feet of the specified test altitude.

Dynamic Stability

- 9. These tests consisted of evaluating both the short-term and long-term responses of the aircraft. The tests were performed with the directional stability augmentation system (SAS) ON and OFF. Short-term response testing was accomplished by left and right directional control pulse inputs. The pulse input was obtained by rapidly displacing the control approximately 1 inch, holding for 0.5 second, then rapidly returning to the trim position and holding until aircraft motions were damped or recovery was required. All other controls remained fixed during forward flight tests. Trim conditions for low-speed dynamic stability tests were established as described under Low-speed Flight Characteristics, paragraph 13. Only the collective control remained fixed during low-speed dynamic stability tests.
- 10. Spiral stability was evaluated by stabilizing and trimming the aircraft in level unaccelerated flight. With lateral and collective fixed, a 5 degree bank angle left and right was established using directional control only. Once a bank angle was established, the directional controls were returned to the trimmed position and fixed while the resultant aircraft response was observed.

11. Long-term stick-fixed longitudinal stability characteristics were evaluated by displacing the aircraft from trim airspeed approximately 10 knots. The technique consisted of reducing airspeed below the trim value using cyclic control, then returning the cyclic control to the original trim position and observing the resulting aircraft response.

Controllability

12. Controllability tests were accomplished by applying left and right directional step inputs of up to 1 inch. The step input was made by rapidly displacing the control from trim, against the observer's foot. The input was rigidly held until a steady rate was obtained or recovery was necessary. A build-up of increasing step displacement was conducted. Collective control was held fixed. Hover and low-speed tests were conducted in winds of 5 knots or less at skid height of 10 feet.

Low-speed Flight Characteristics

- 13. Testing was accompushed using the ground pace vehicle method in winds of 5 knots or less. Tests were flown in not less than 5 knot increments from hover to 30 KTAS. All tests were conducted by stabilizing at a skid height of approximately 10 feet. The pace vehicle then established the desired speed using a calibrated fifth wheel for a reference ground speed. The test aircraft was flown in formation with the pace vehicle utilizing ground reference and horizontal situation indicator for heading stabilization. Data were recorded when the relative motion between the aircraft and pace vehicle was zero and the radar altimeter indicated no vertical displacement from the desired skid height.
- 14. Low-speed flight characteristics effects on yaw rates were accomplished by stabilizing on the 270 and 090 degree relative azimuths as described in paragraph 27. A left or right yaw up to 20 degrees/second was established; then, both collective and pedal controls were fixed while in the 120 to 240 degree relative azimuth region. Cyclic was used as necessary to maintain pace speed. Recovery from the yaw rate was initiated at the region boundary. Recovery was completed prior to passing the 360 degree relative azimuth.

Trim Changes With Power Effects

15. These tests were conducted by stabilizing the aircraft in a maximum power climb at the desired trim airspeed and sideslip with the SAS OFF. Collective control was gradually reduced while airspeed and sideslip were maintained until the rate of descent reached 1000 feet per minute.

Mission Maneuvers

16. Mission maneuvers were conducted in accordance with the OH-SS helicopter ATM (ref. 11, app. A).

APPENDIX E. TEST DATA

Figure	rigure Number		
Control System Characteristics	E-1 through E-3		
Static Lateral-Directional Stability	E-4 through E-9		
Maneuvering Stability	E-10		
Dynamic Stability	E-11 through E-151		
Controllability	E-152 through E-157		
Low-Speed Flight	E-158 through E-208		
Trim Changes with Power Effects	E-209 through E-216		
Mission Maneuvers	E-217 through E-254		
Pitot-Static Calibration	E-255		

FIGURE E-1 LIMITS OF CYCLIC CONTROL TRAVEL JOH-58C USA S/N 70-15349

NOTES:

ROTORS STATIC
CONTROL POSITION MEASURED AT CENTER OF GRIP
HYDRAULIC AND ELECTRICAL POWER PROVIDED BY
EXTERNAL POWER SOURCES
COLLECTIVE CONTROL FULL DOWN 2. 3.

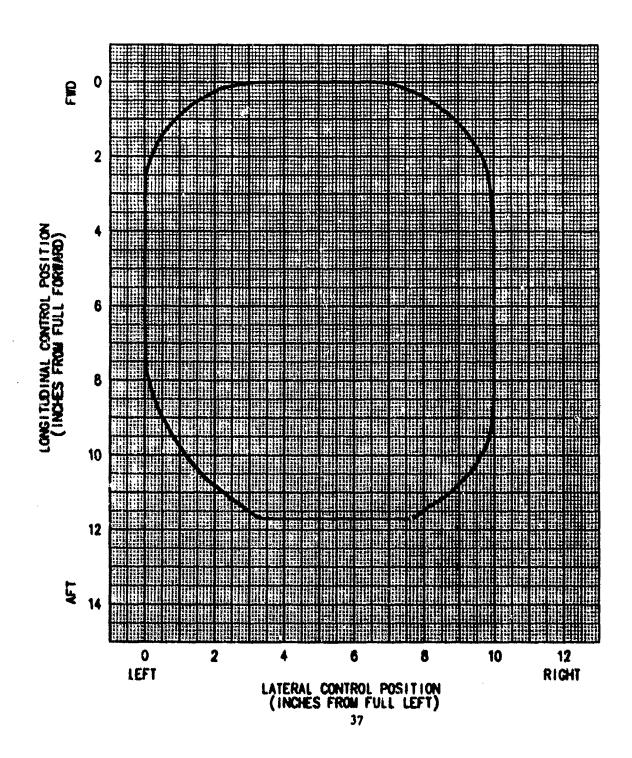


FIGURE E-2 LONGITUDINAL CONTROL SYSTEM CHARACTERISTICS JOH-58C USA S/N 70-15349

NOTES:

1. ROTORS STATIC
2. FORCES AND POSITIONS MEASURED AT CENTER OF CONTROL GRIP

3. HYDRAULIC AND ELECTRICAL POWER PROVIDED BY

EXTERNAL POWER SOURCES

4. HYDRAULIC SYSTEM ON

5. STABILITY AUGMENTATION SYSTEM ON

6. LATERAL CONTROL POSITION = 5.6 INCHES

FROM FULL LEFT

7. FORCE TRIM ON, ADJUSTABLE CYCLIC FRICTION OFF 8. TOTAL LONGITUDINAL CONTROL TRAVEL = 11.7 INCHES

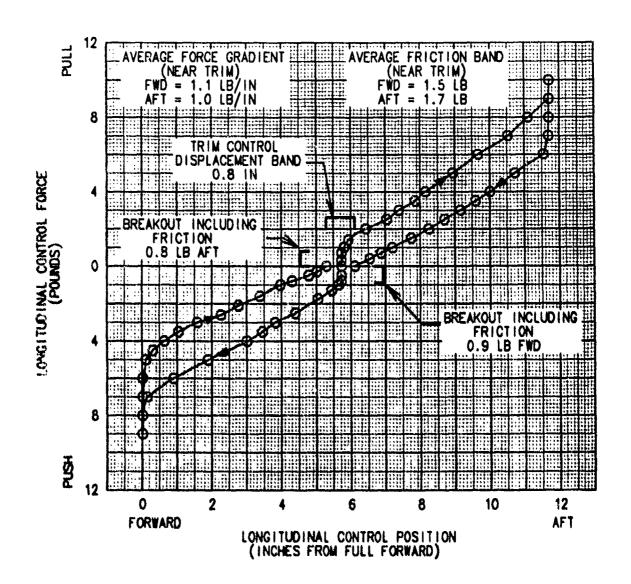


FIGURE E-3 LATERAL CONTROL SYSTEM CHARACTERISTICS JOH-58C S/N 70-15349

NOTES:

- 1. ROTORS STATIC 2. FORCES AND POSITIONS MEASURED AT CENTER OF CONTROL GRIP
- 3. HYDRAULIC AND ELECTRICAL POWER PROVIDED BY EXTERNAL POWER SOURCES

- HYDRAULIC SYSTEM ON
 STABILITY AUGMENTATION SYSTEM ON
 LONGITUDINAL CONTROL POSITION = 4.5 INCHES FROM FULL FORWARD
- 7. FORCE TRIM ON, ADJUSTABLE CYCLIC FRICTION OFF 8. TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES

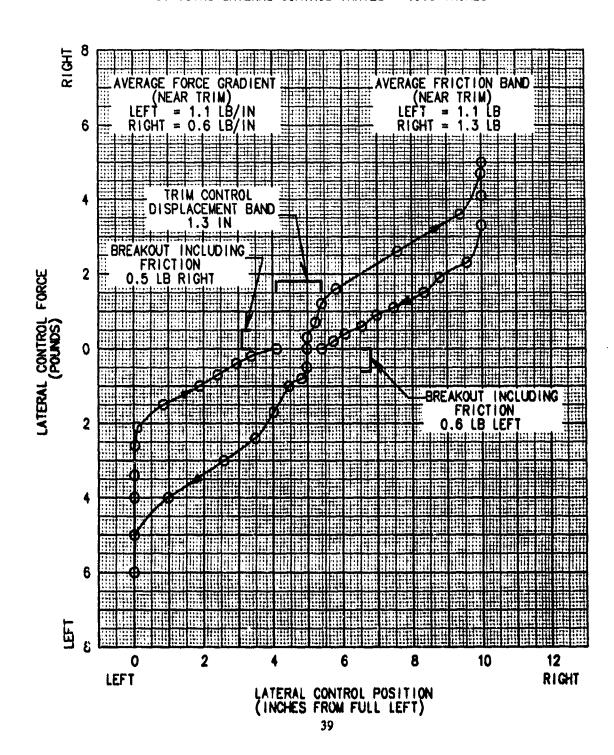


FIGURE E-4
STATIC LATERAL-DIRECTIONAL STABILITY
JOH-58C S/N 70-15349

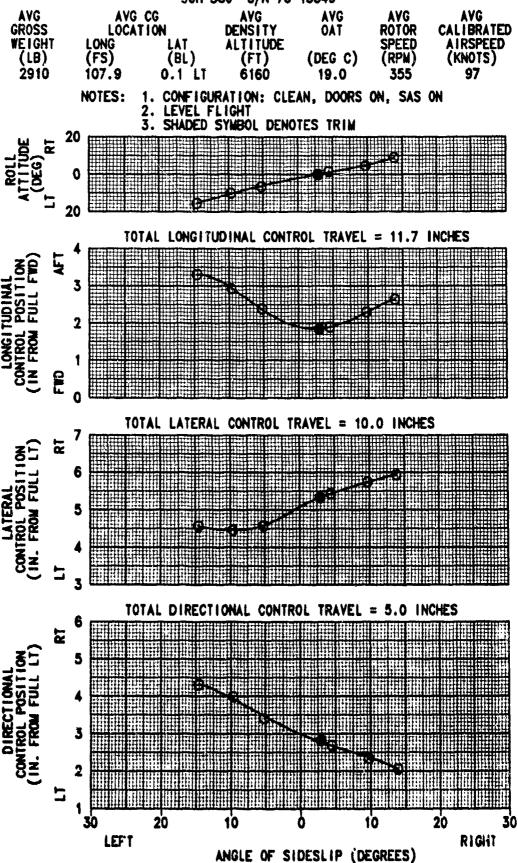


FIGURE E-5
STATIC LATERAL-DIRECTIONAL STABILITY
JOH-58C S/N 70-15349

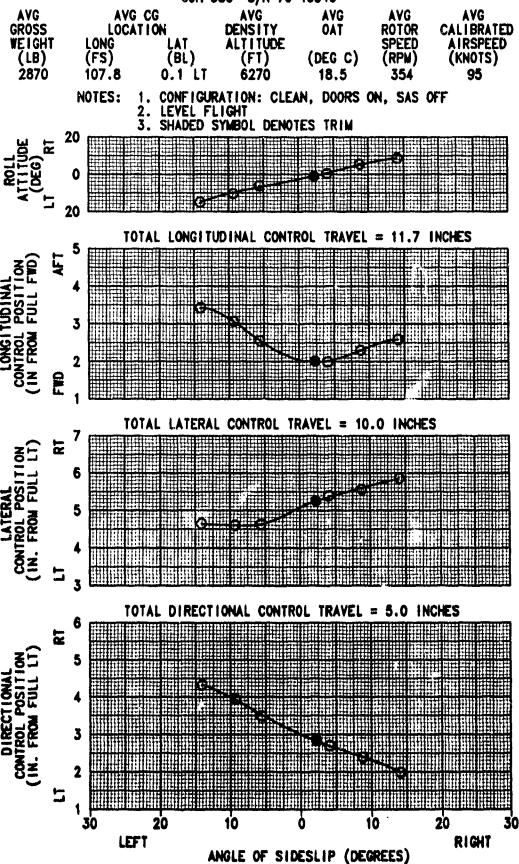


FIGURE E-6 STATIC LATERAL-DIRECTIONAL STABILITY JOH-58C S/N 70-15349

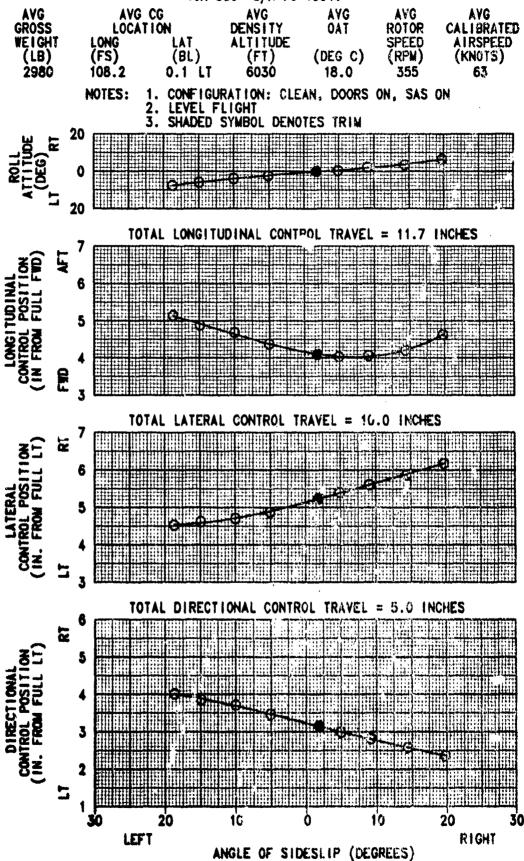


FIGURE E-7
STATIC LATERAL-DIRECTIONAL STABILITY
JOH-58C S/N 70-15349

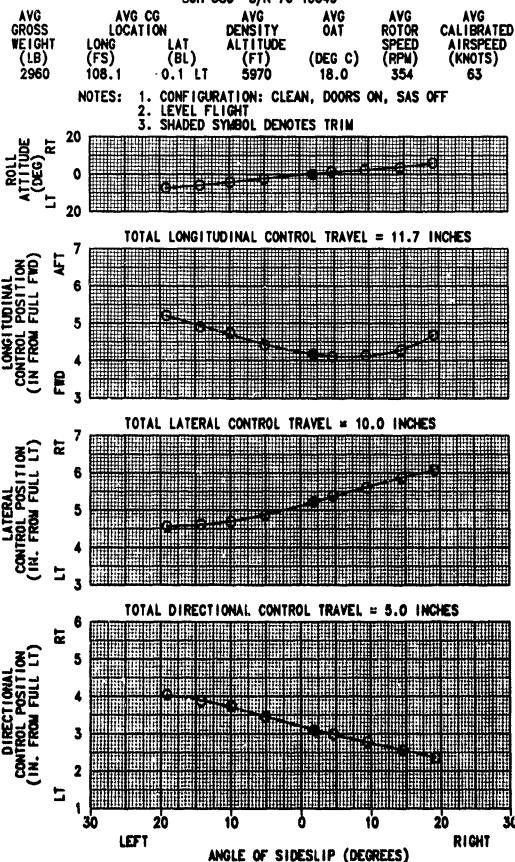
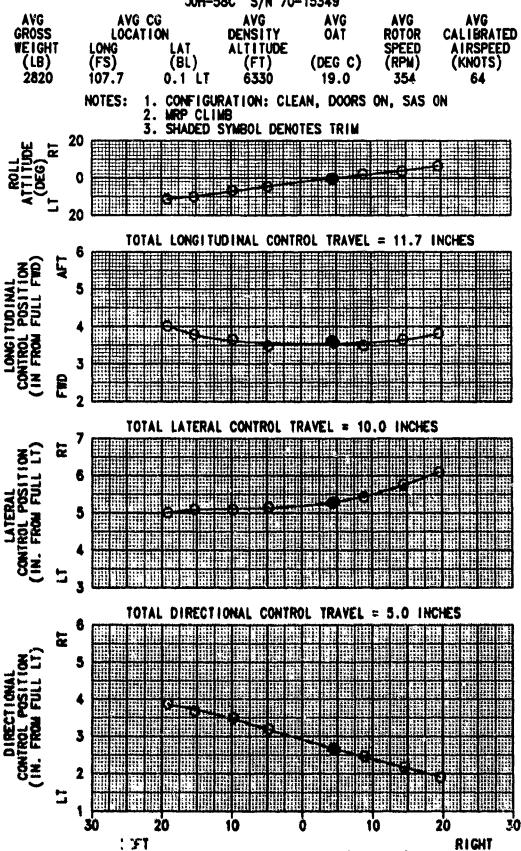


FIGURE E-8
STATIC LATERAL-DIRECTIONAL STABILITY IN CLIMBING FLIGHT
JOH-58C S/N 70-15349



ANGLE OF SIDESLIP (DEGREES)

FIGURE E-9
STATIC LATERAL-DIRECTIONAL STABILITY IN AUTOROTATIONAL FLIGHT
JOH-58C S/N 70-15349

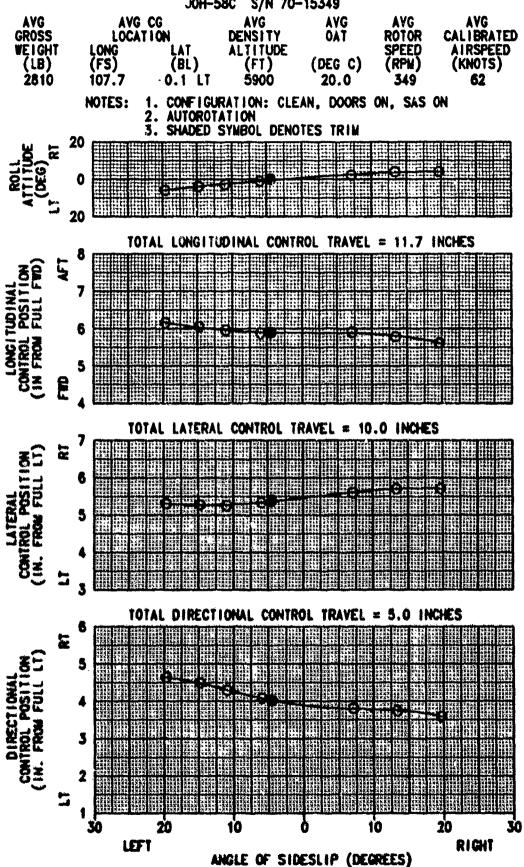
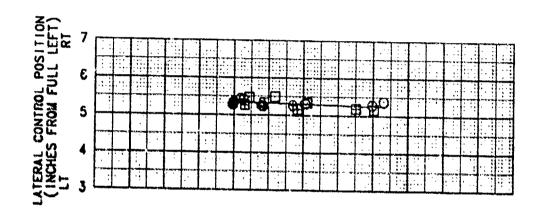
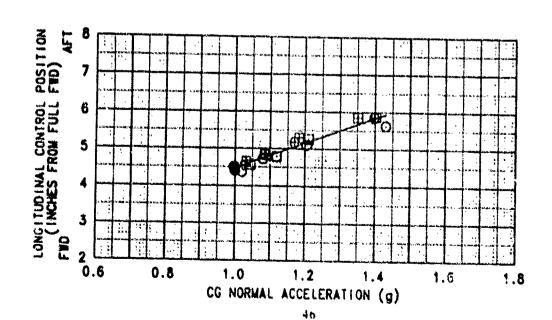


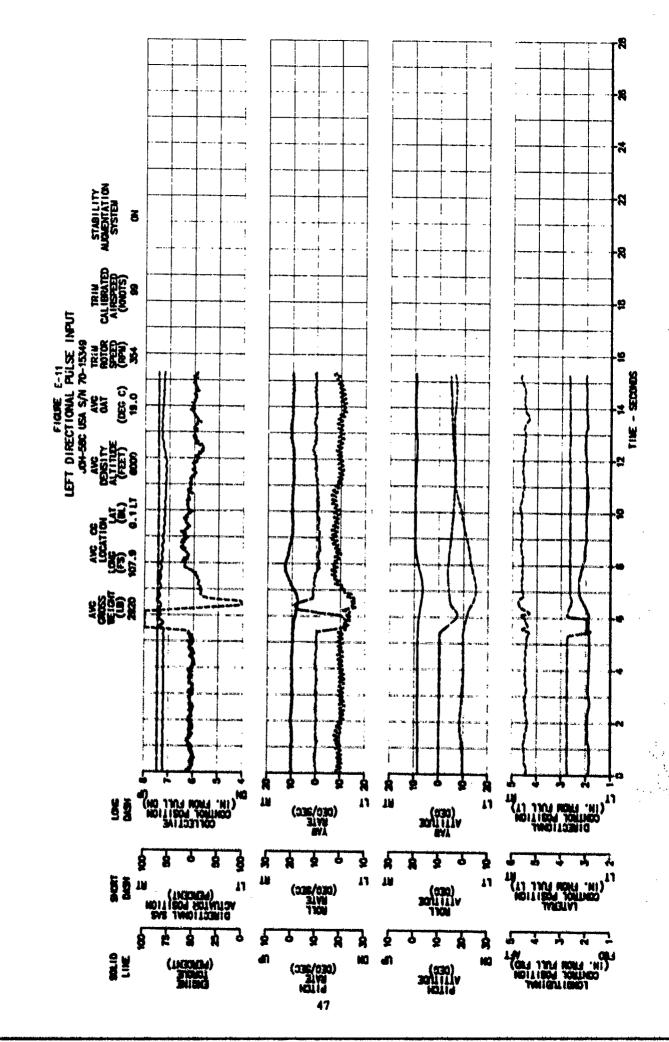
FIGURE E-10 MANEUVERING STABILITY JOH-58C S/N 70-15349

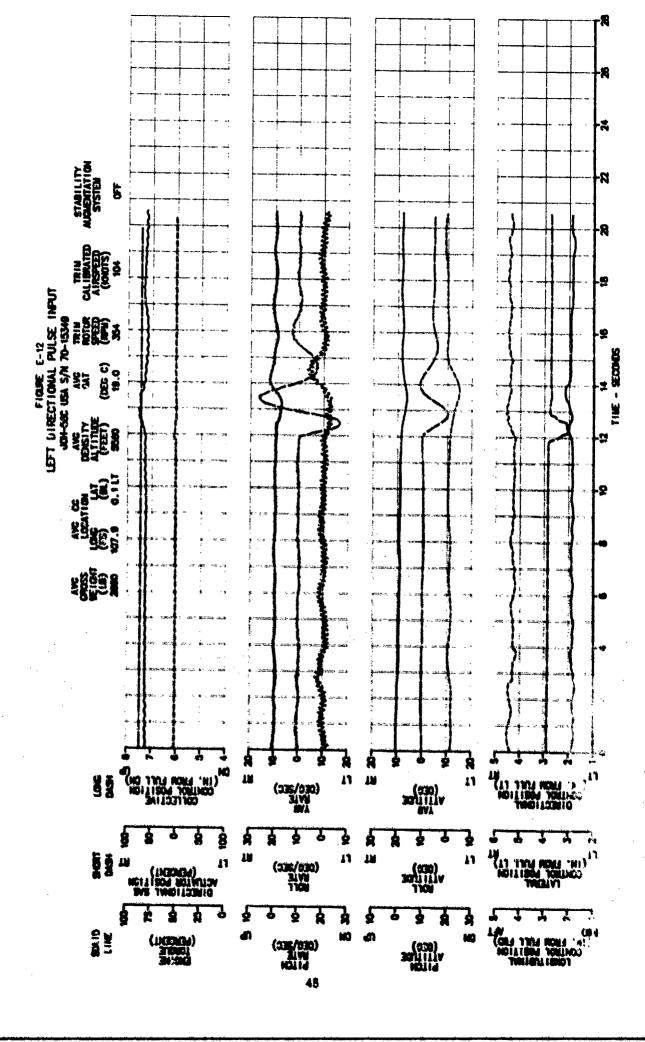
SYM	AVG GROSS WEIGHT (LB)	AVG LOCAT LONG (FS)		AVG DENSITY ALTITUDE (FT)	AVG OAT (DEG C)	AVG ROTOR SPEED (RPM)	AVG CALIBRATED AIRSPEED (KNOIS)	STABILITY AUGMENTATION SYSTEM
0	2990	107.7	0.0	6690	21.0	355	64	ON
	2930	107.5	0.0	6610	21.5	355	63	OFF

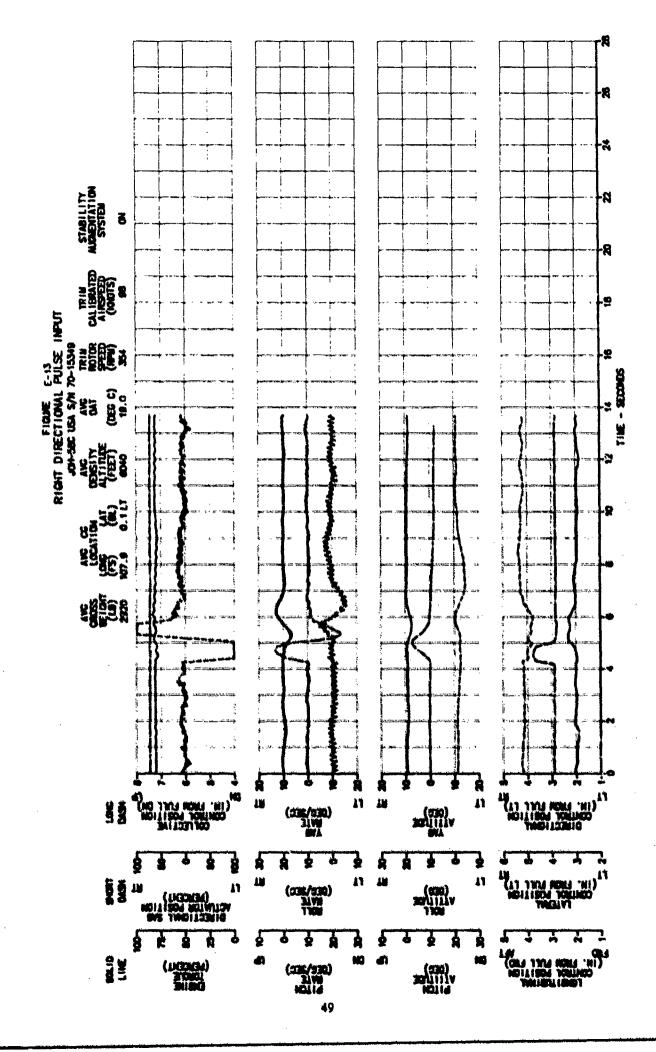
NOTE: 1. CLEAN CONFIGURATION, DOORS ON
2. SHADED SYMBOLS DENOTE TRIM,
OPEN SYMBOLS DENOTE LEFT TURN,
CROSSED SYMBOLS DENOTE RIGHT TURN

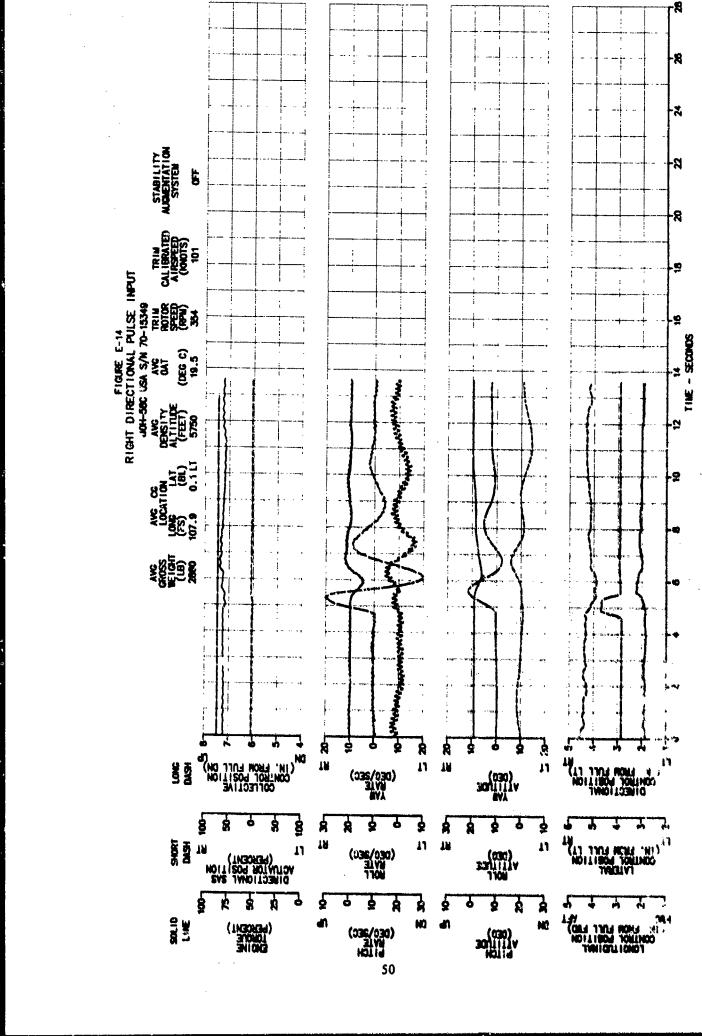


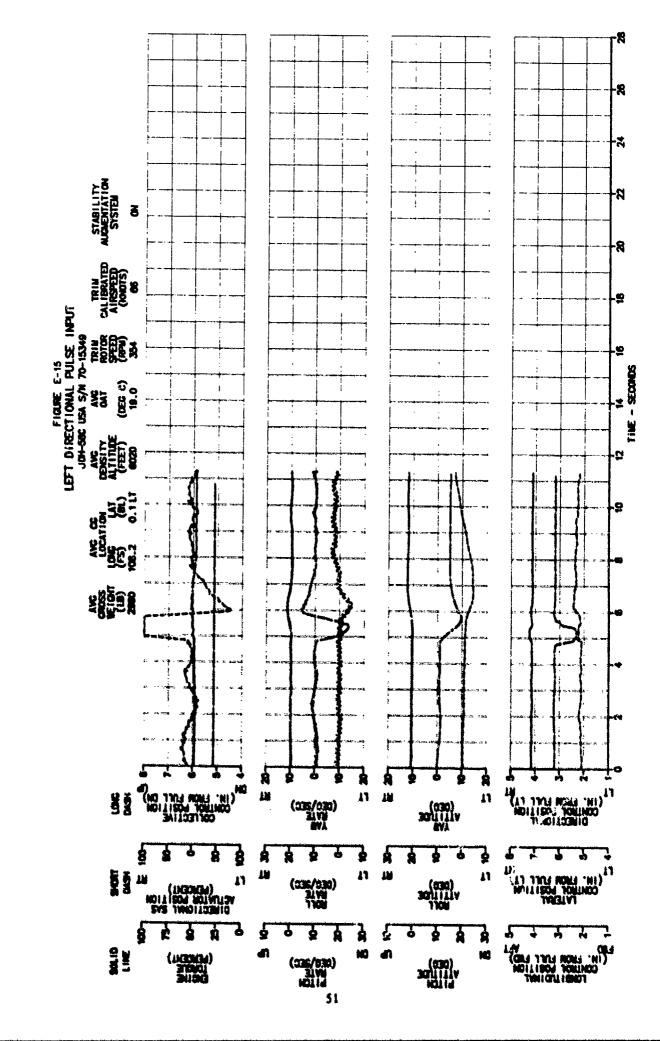




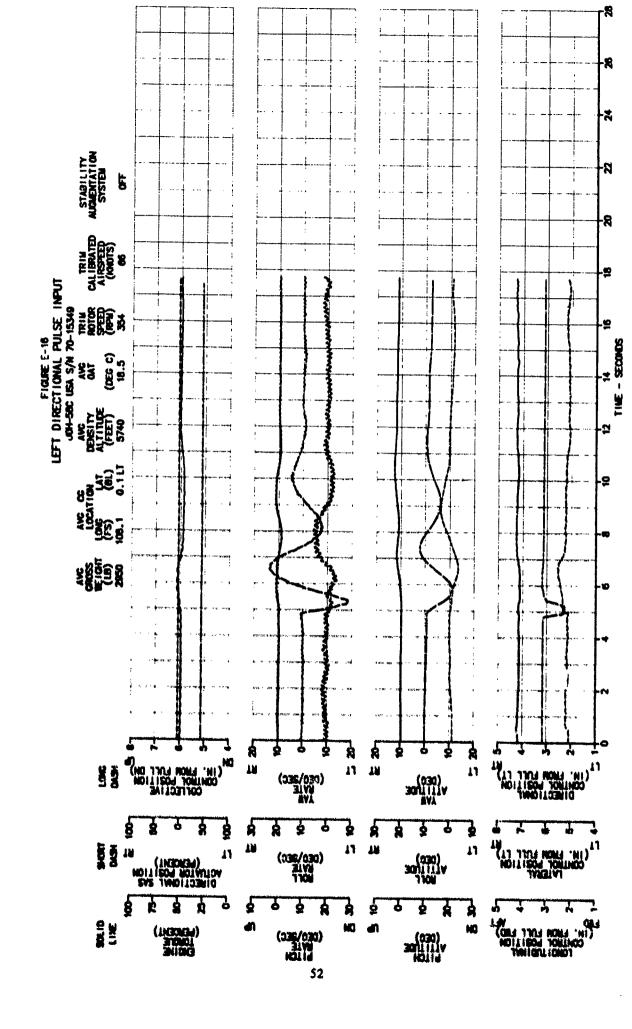


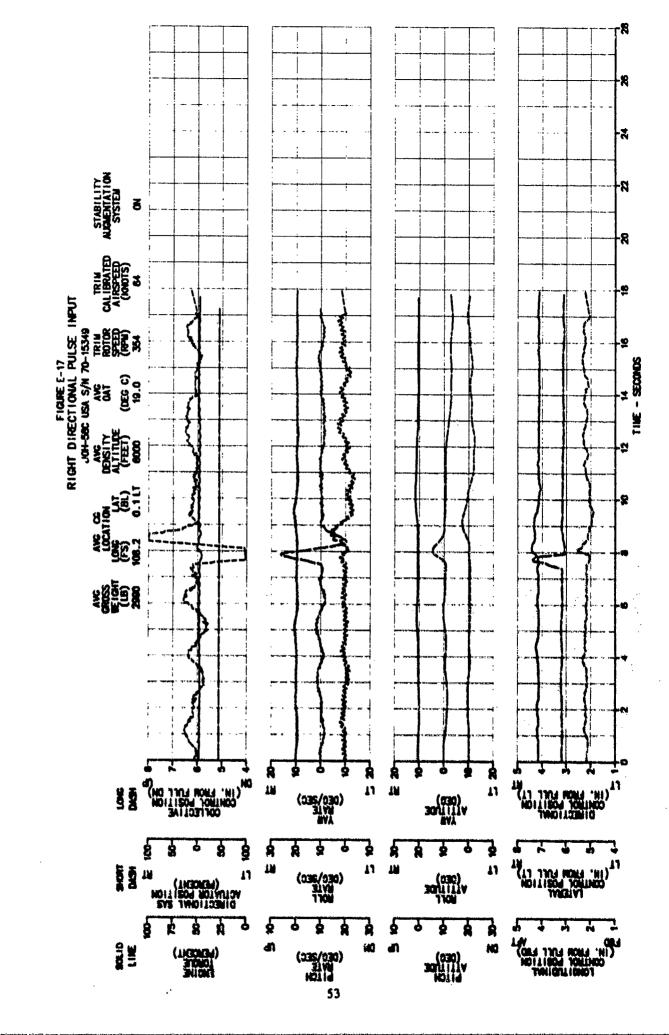


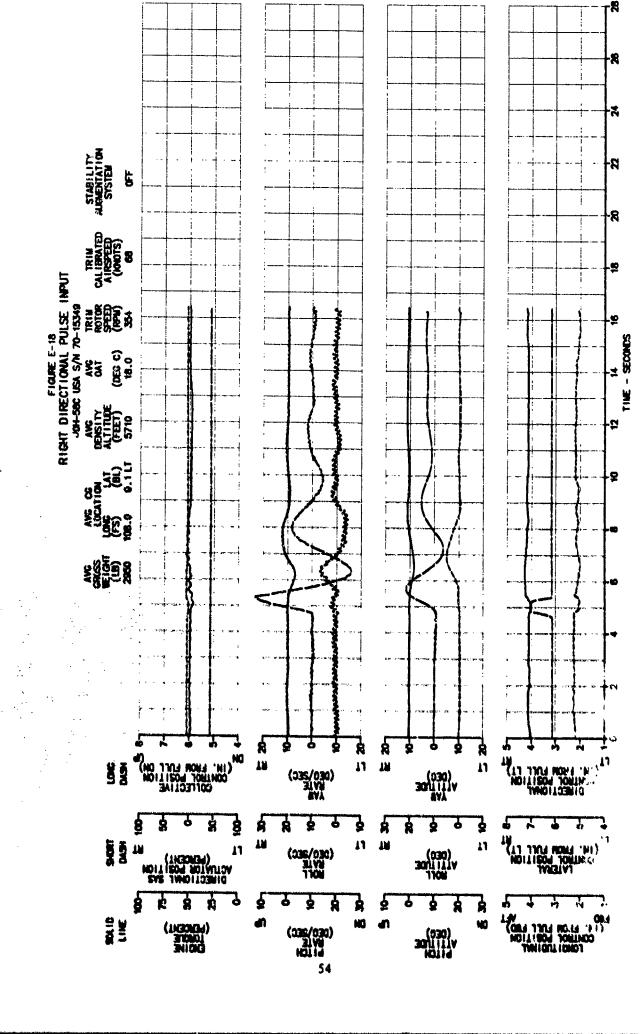


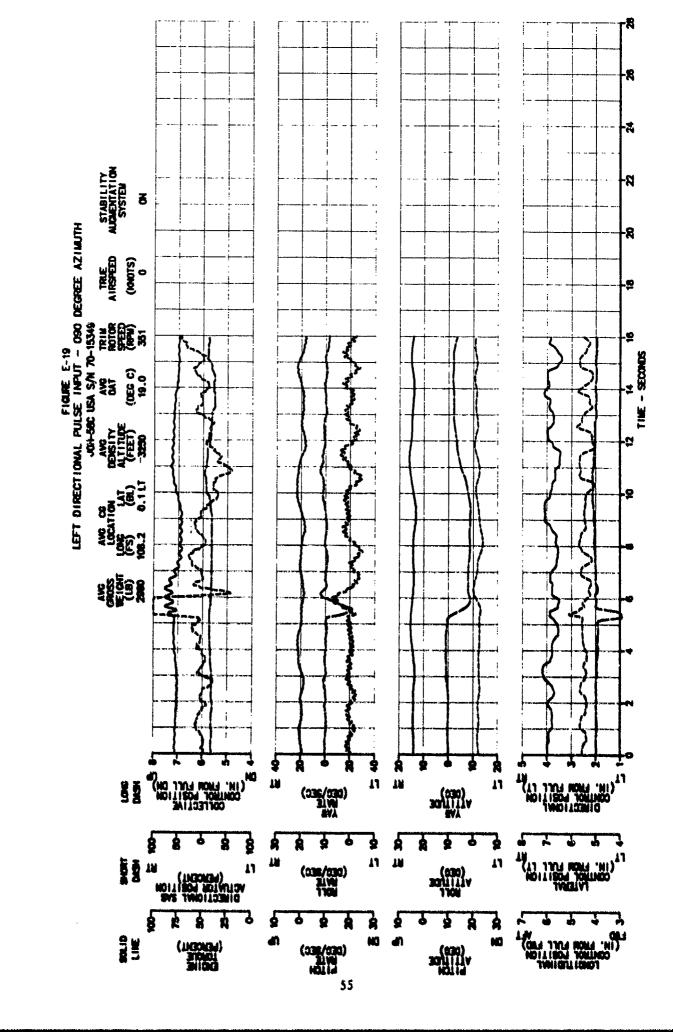


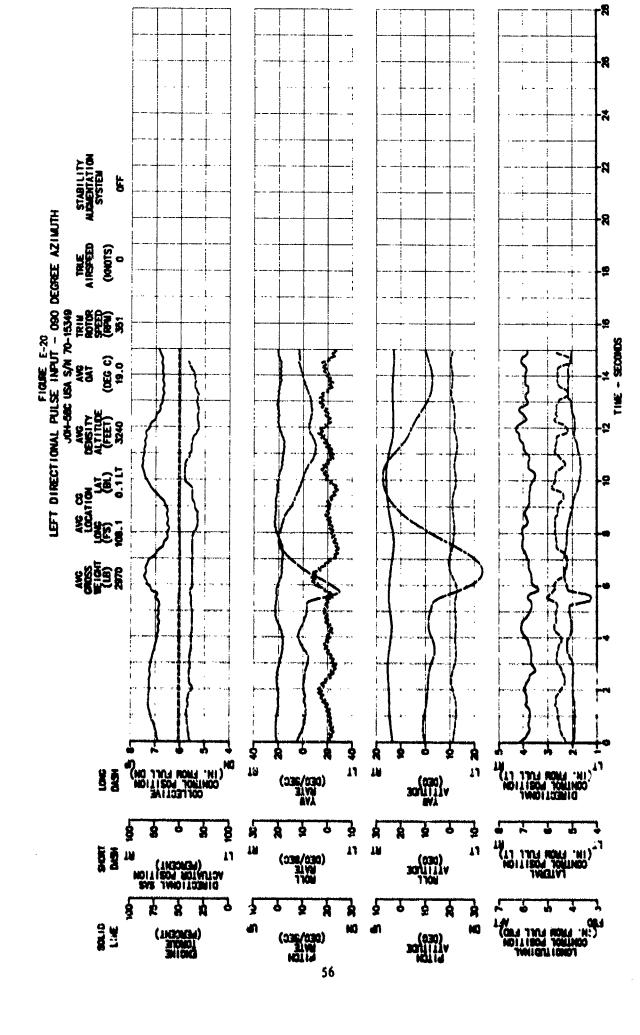
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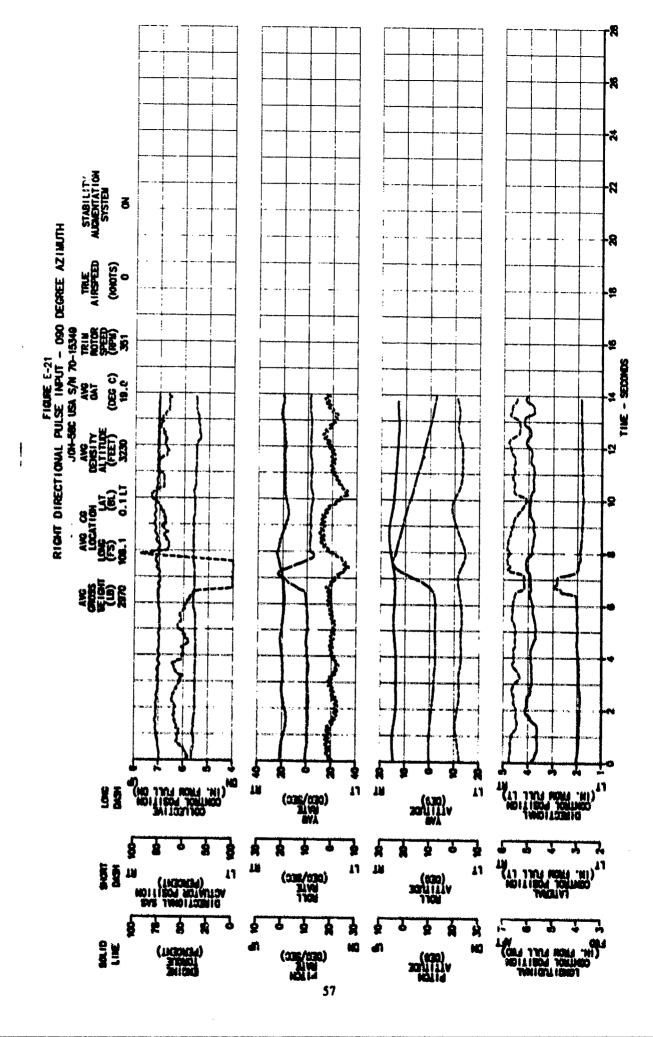


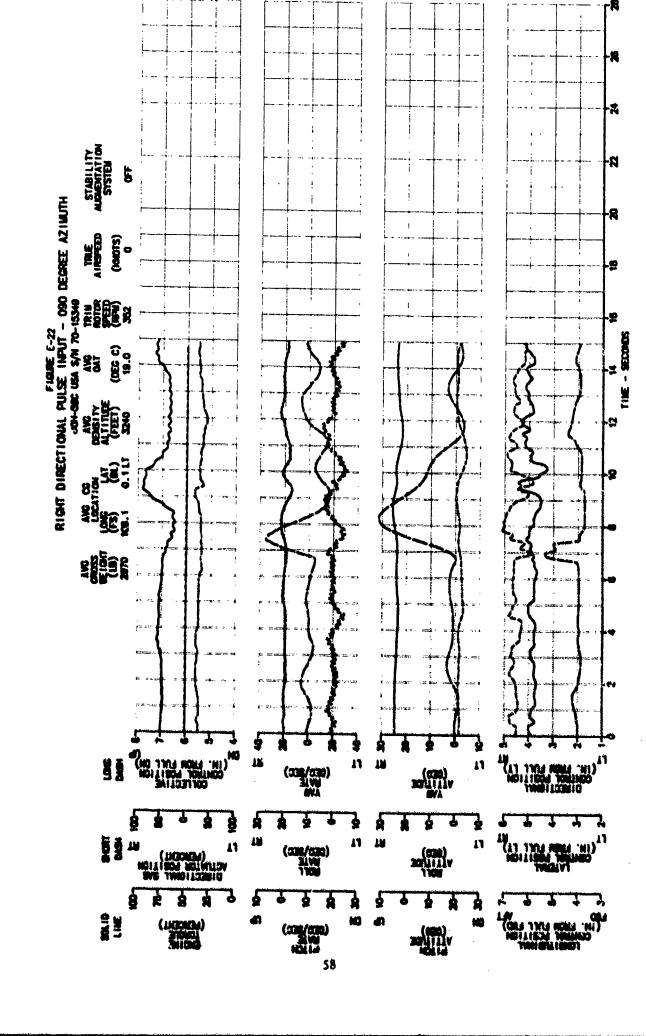


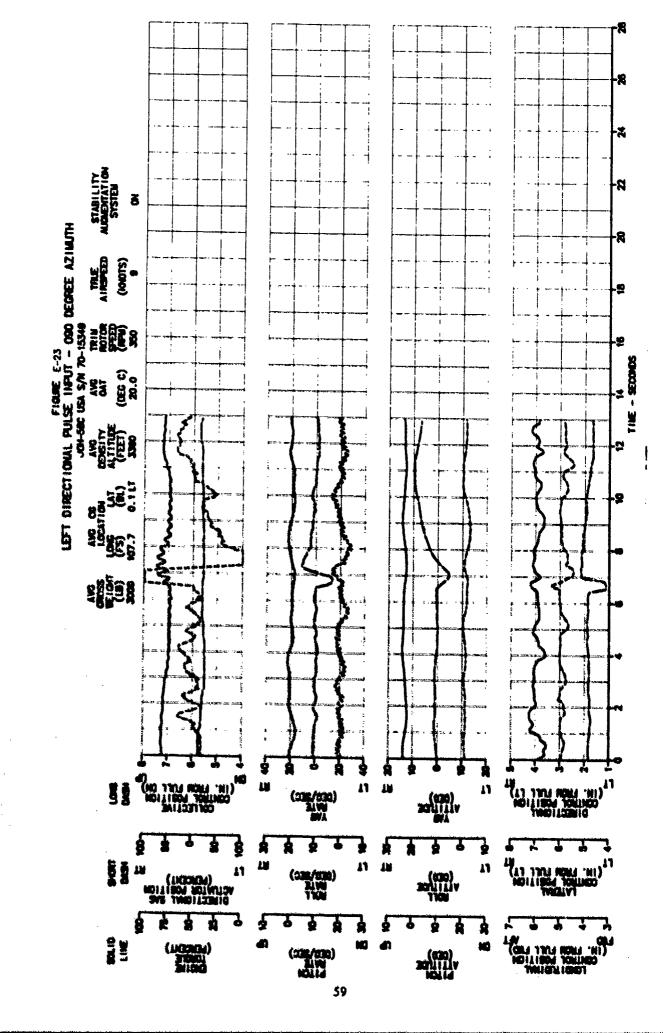


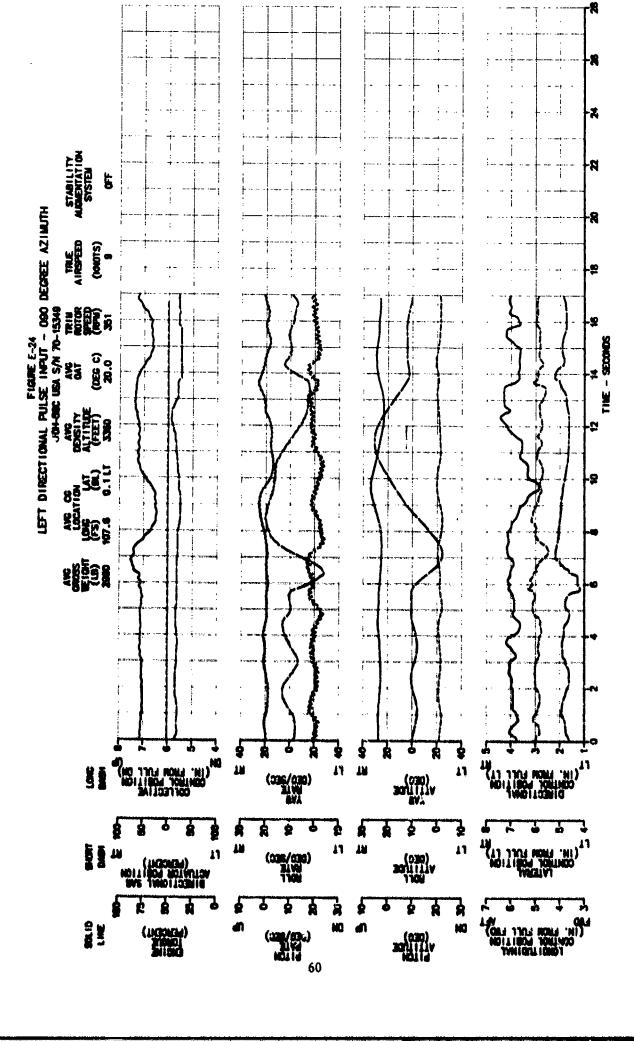


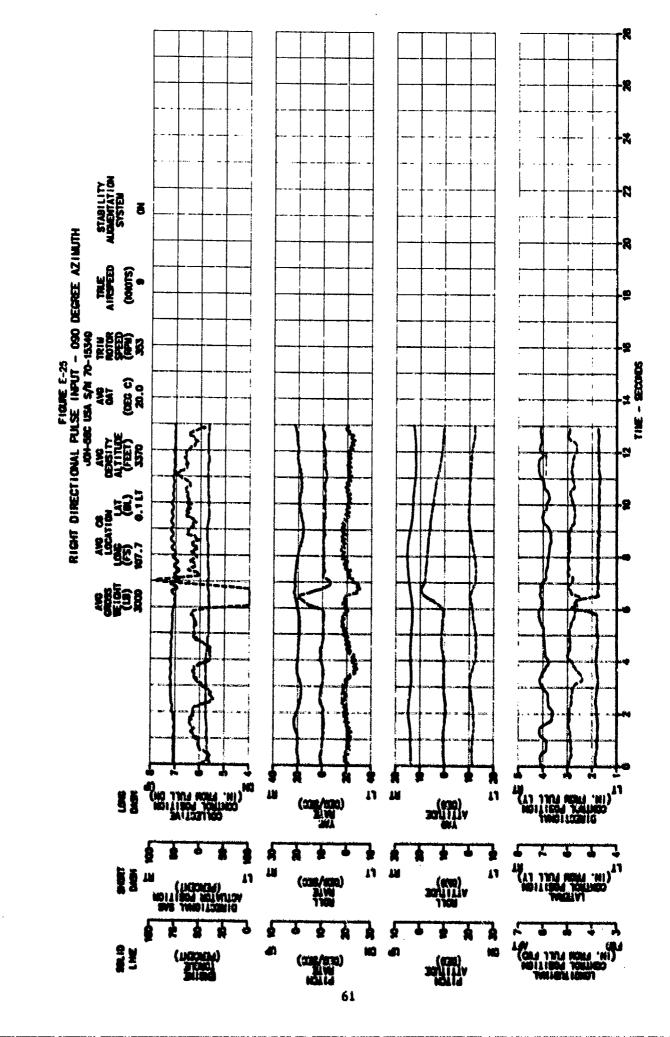


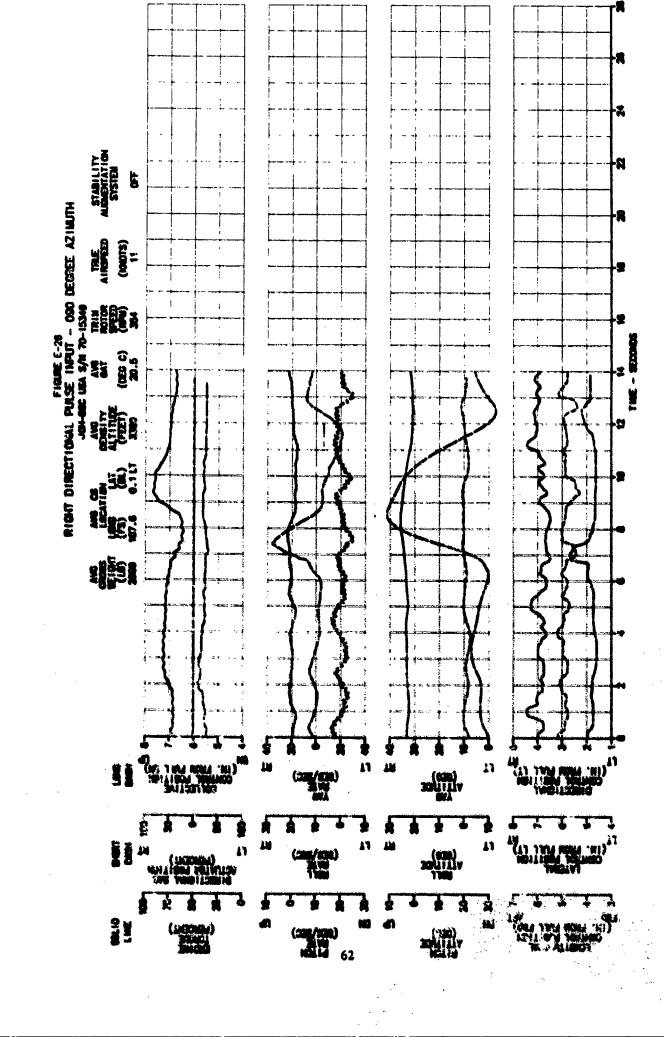


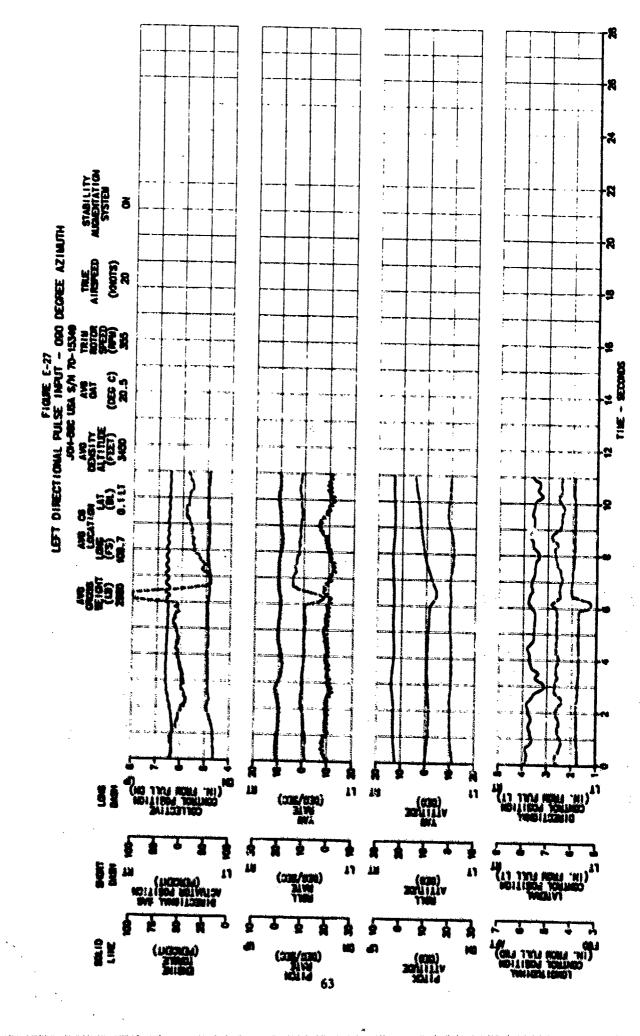


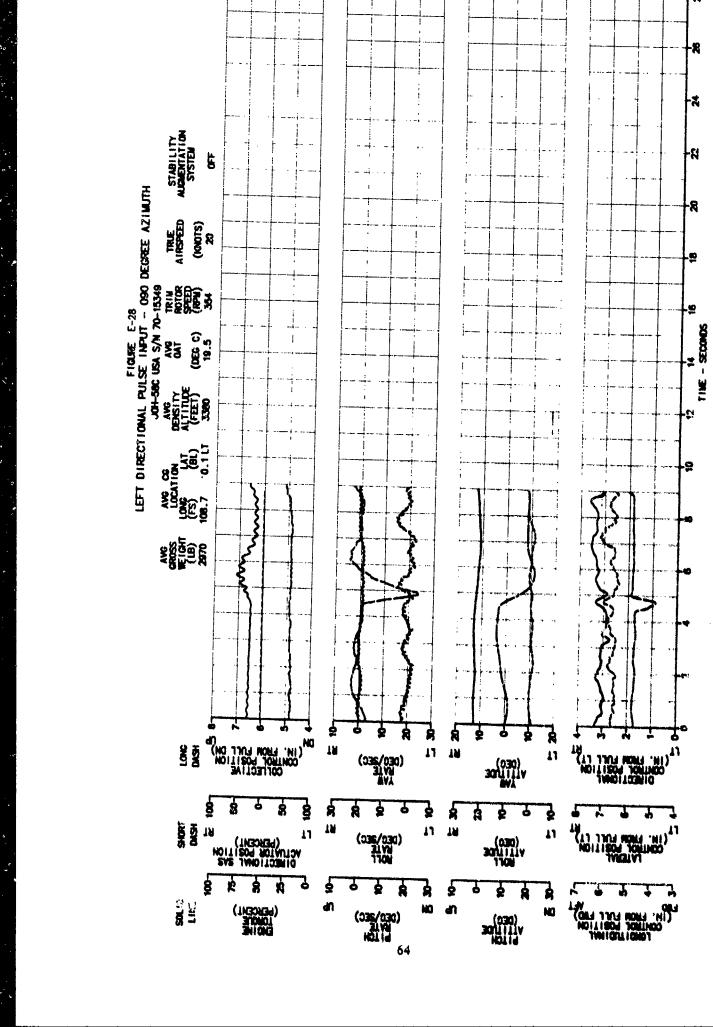


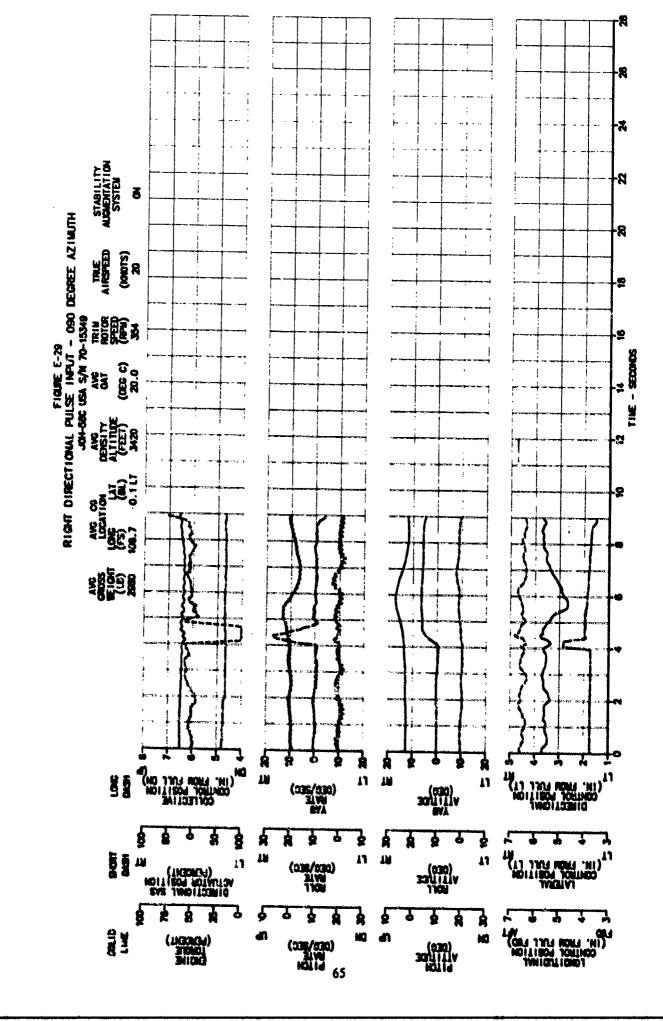


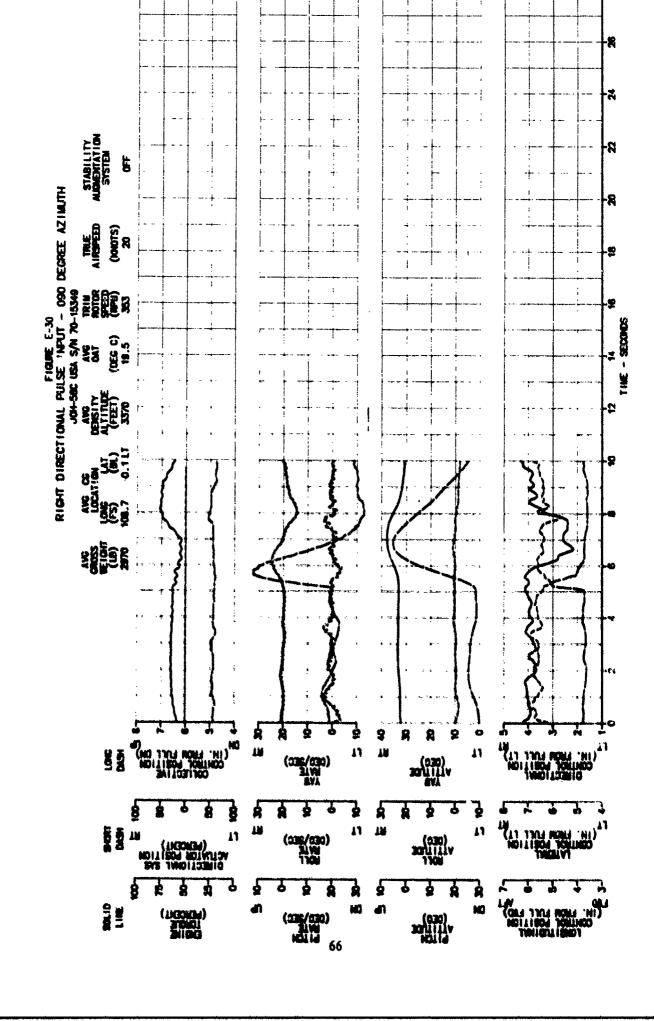


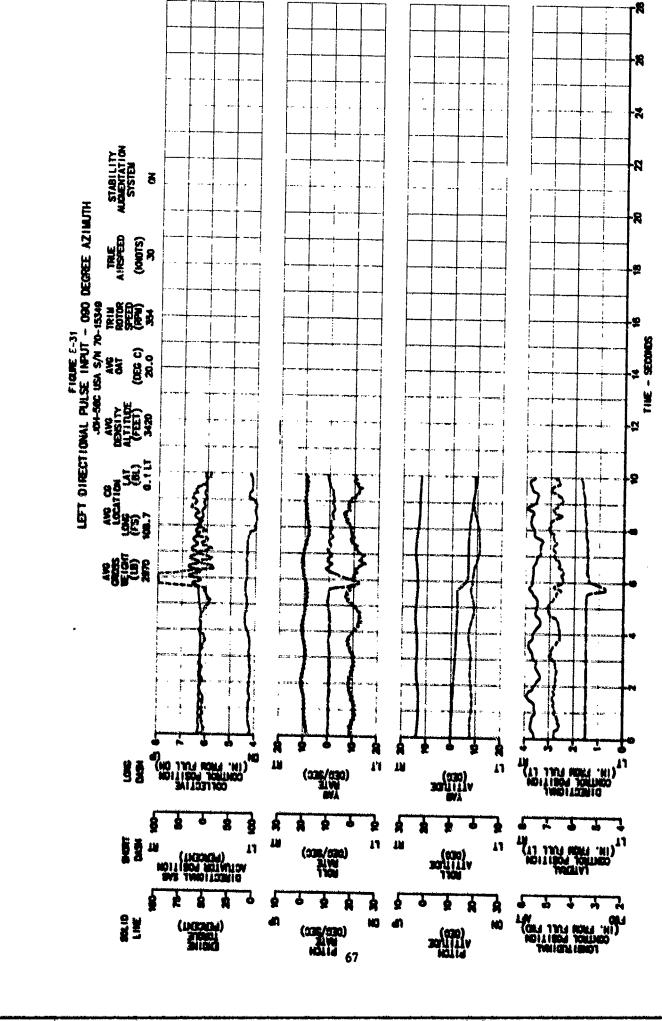


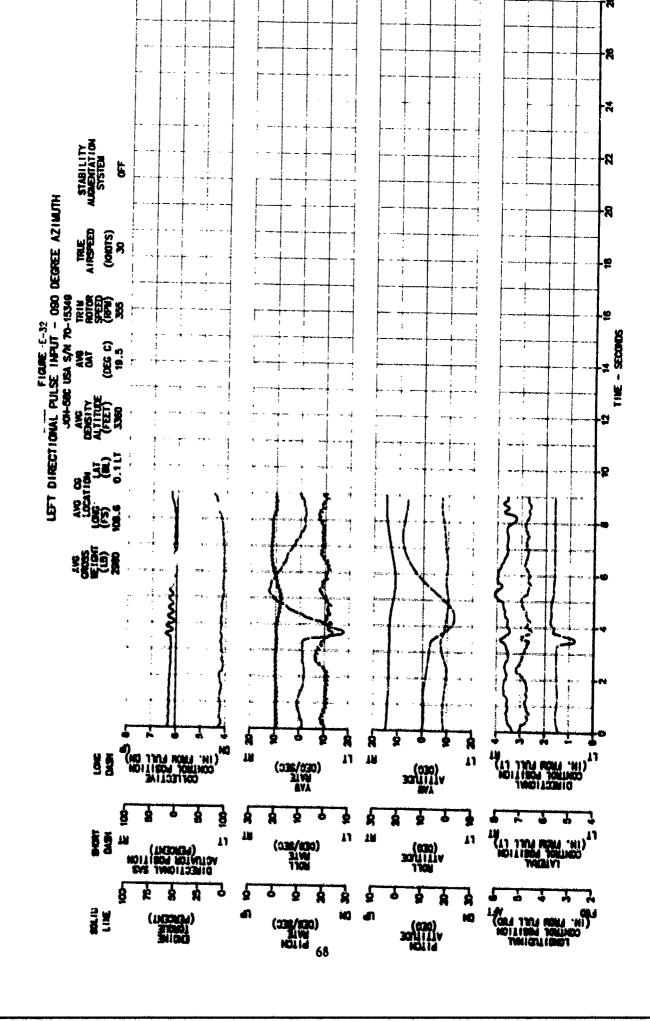


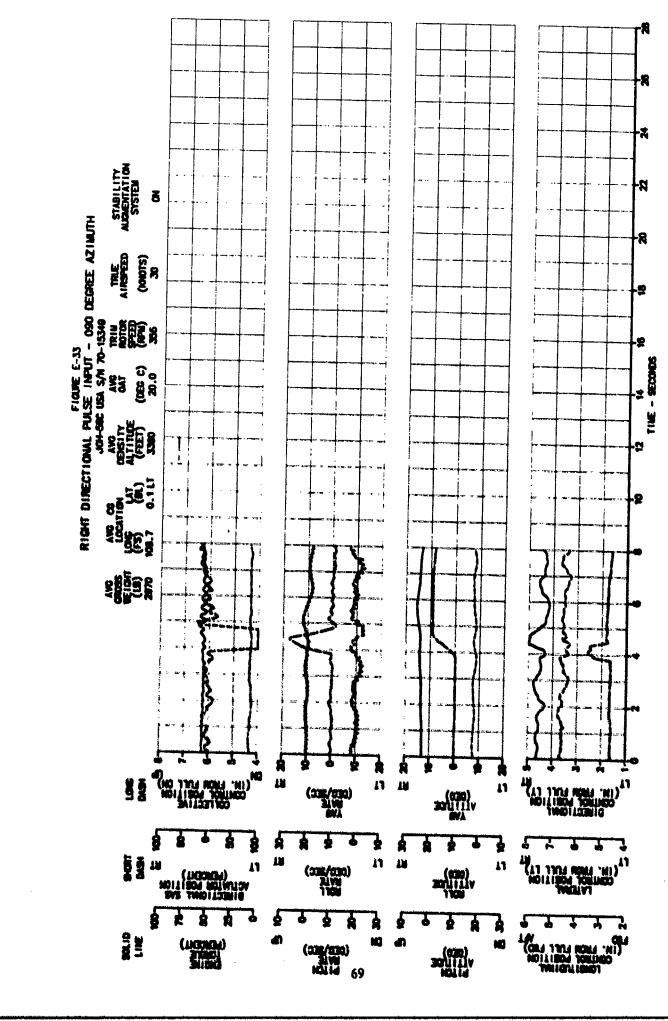


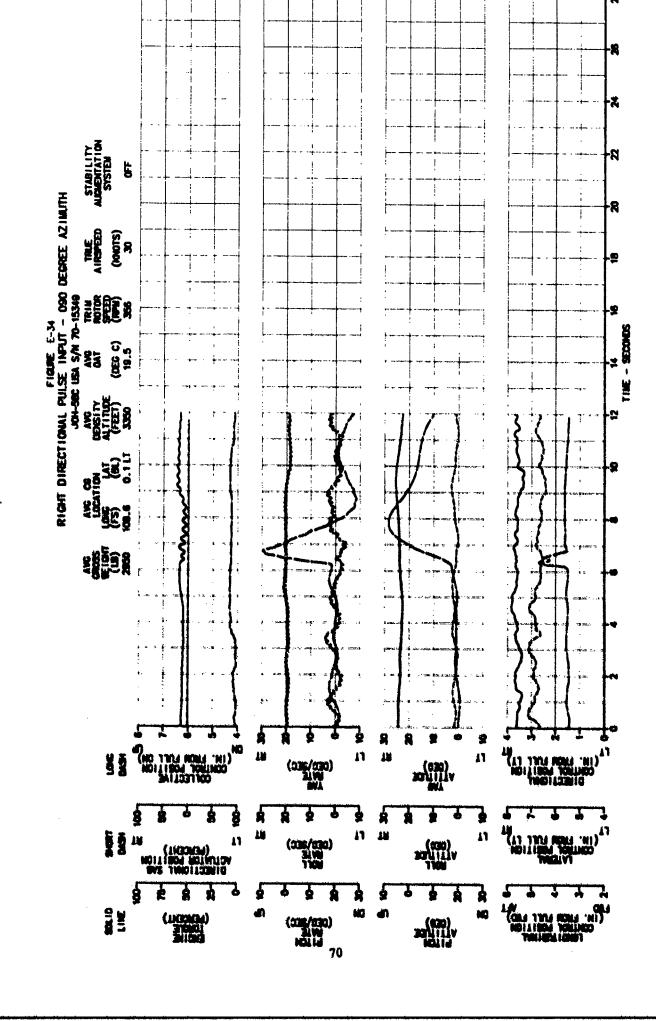


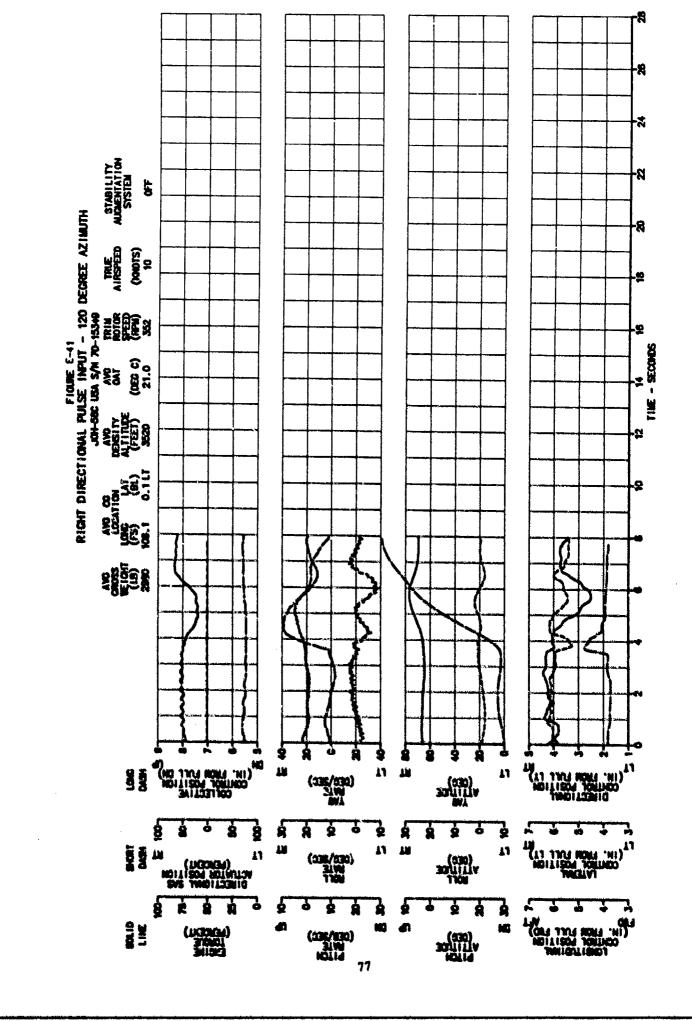


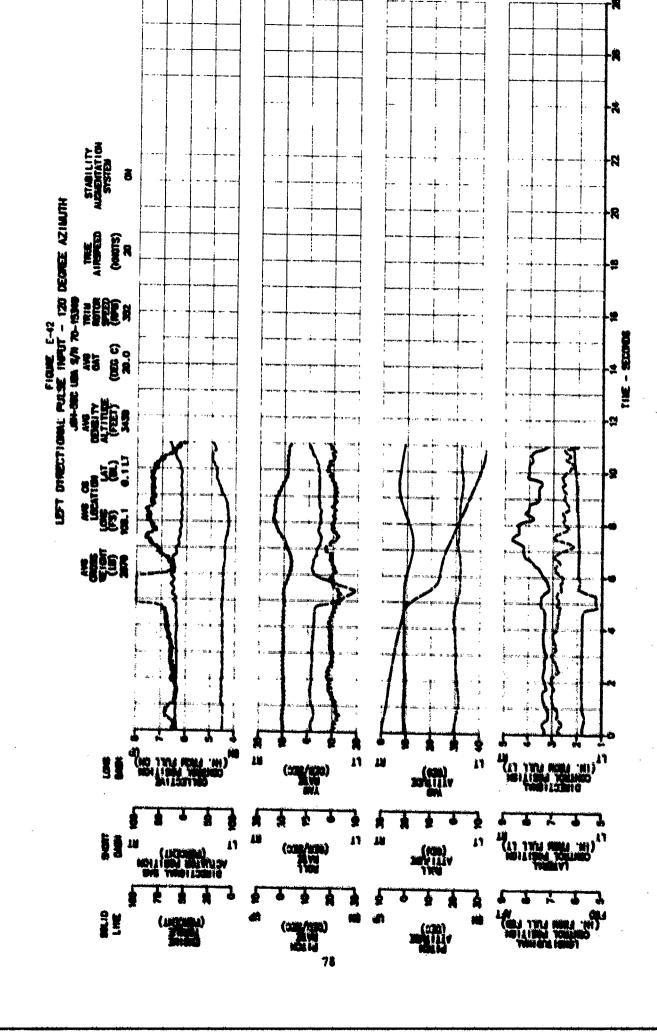


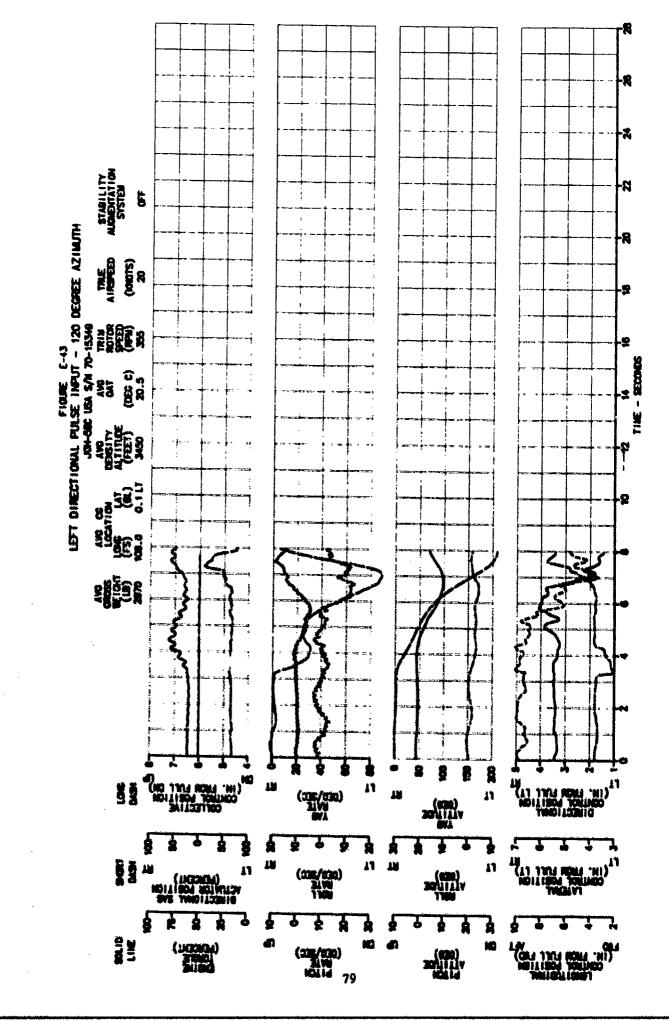


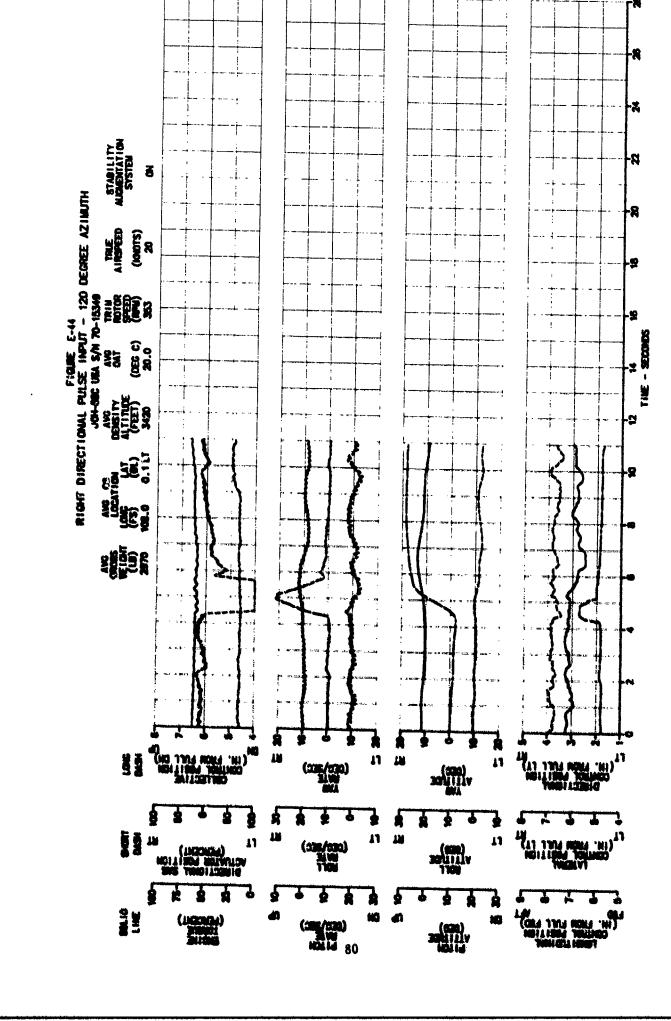


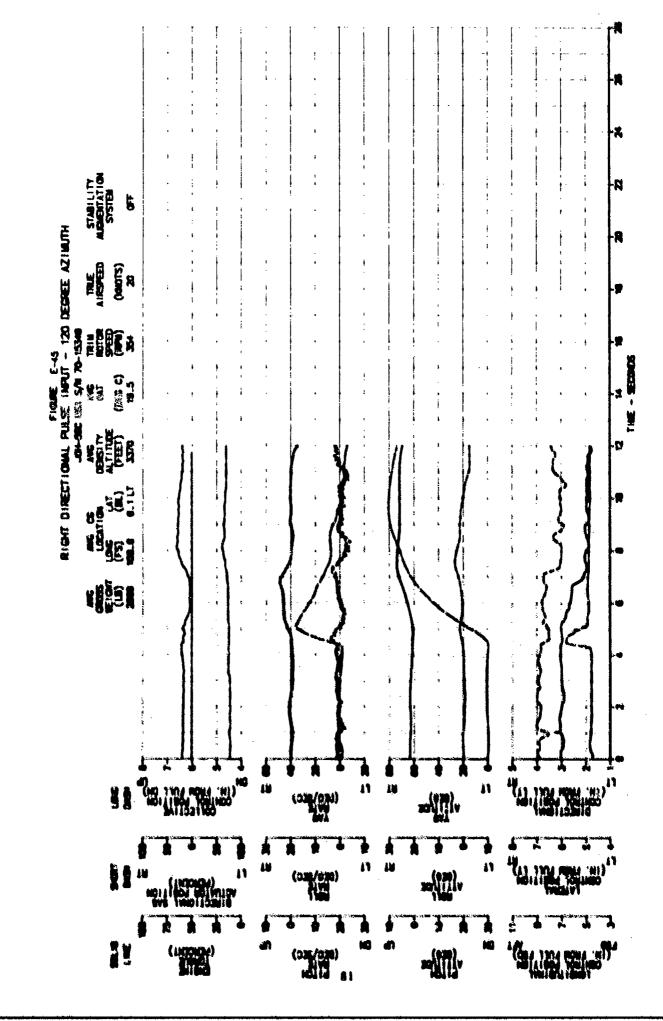


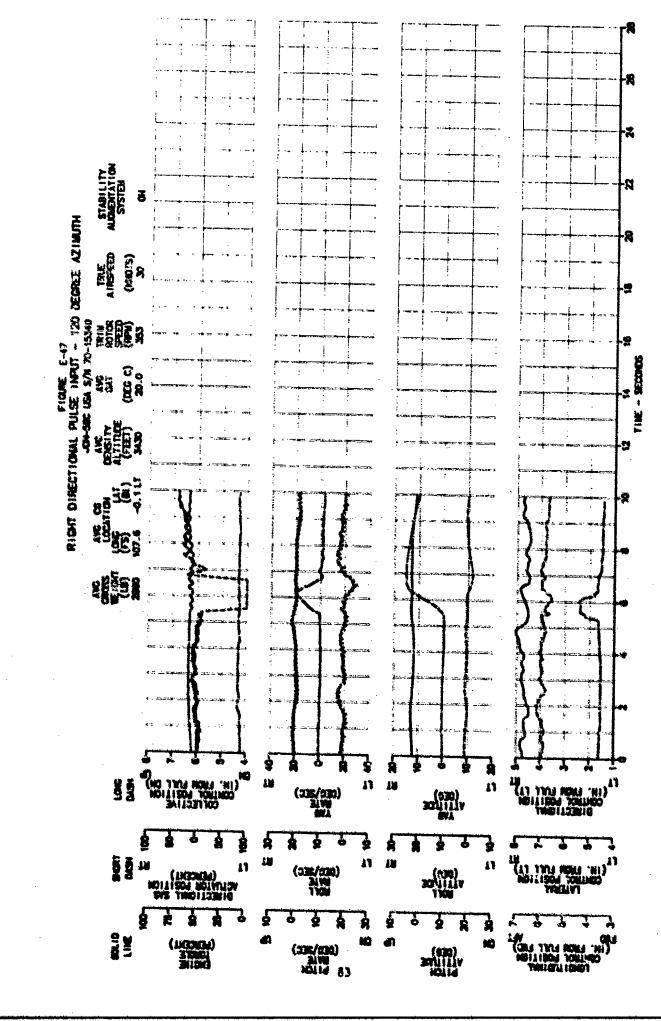


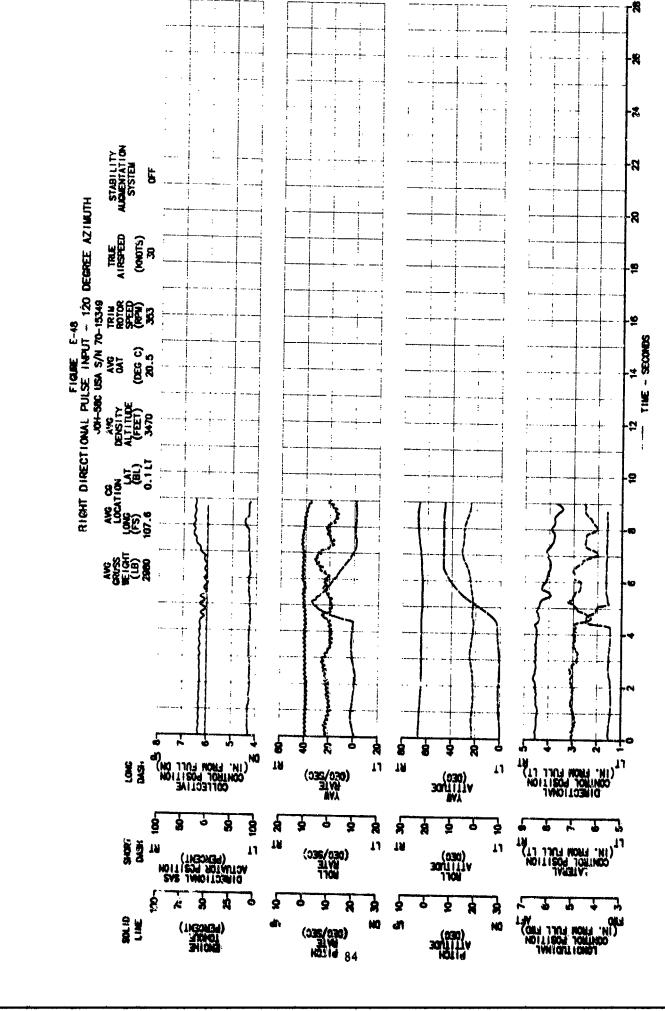


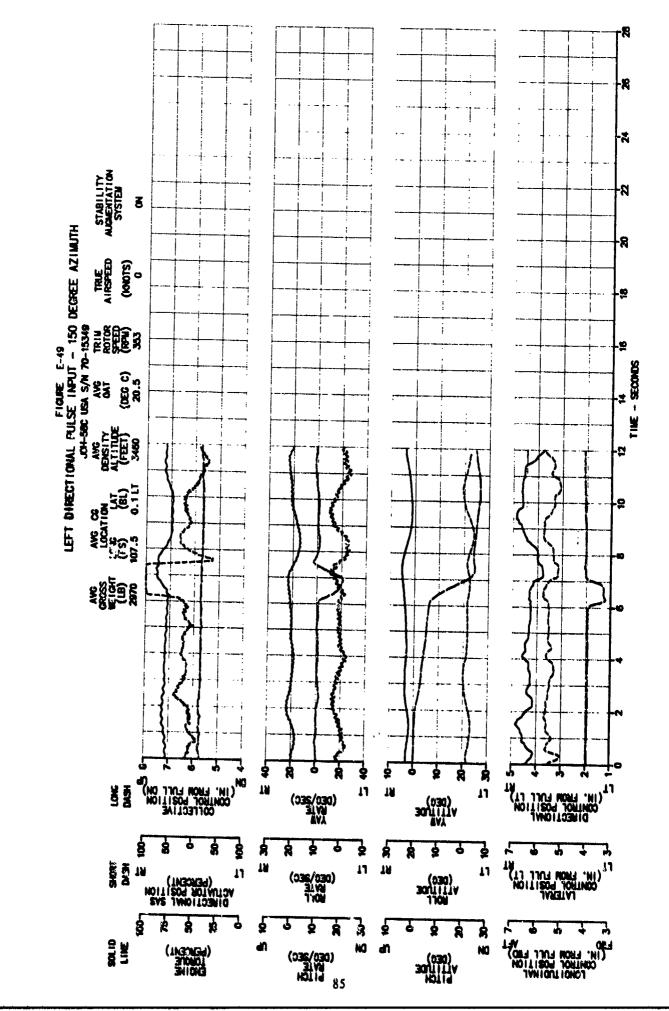


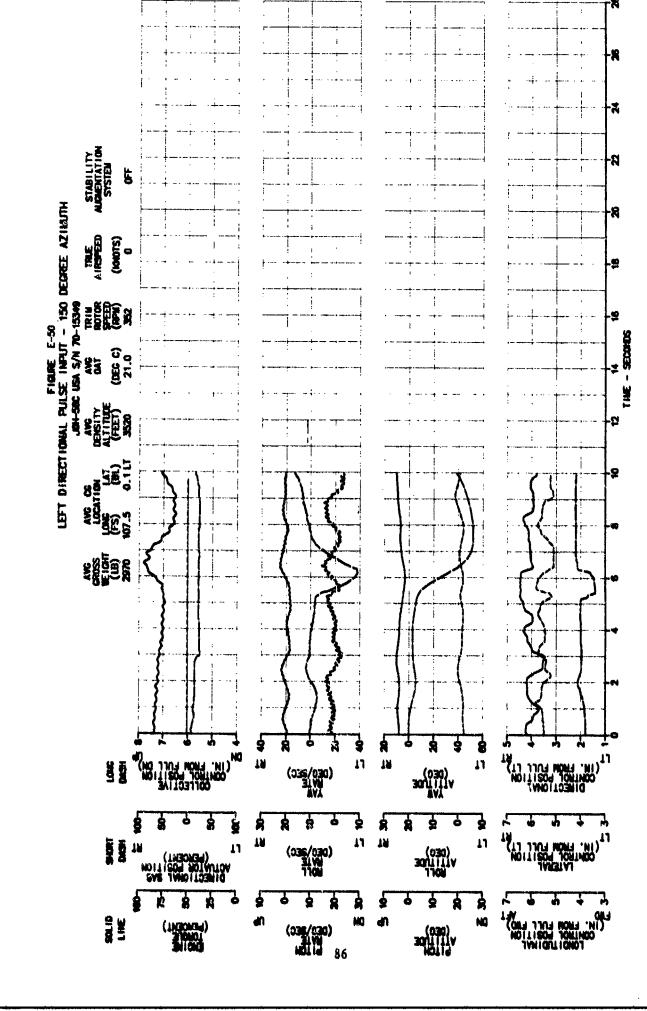


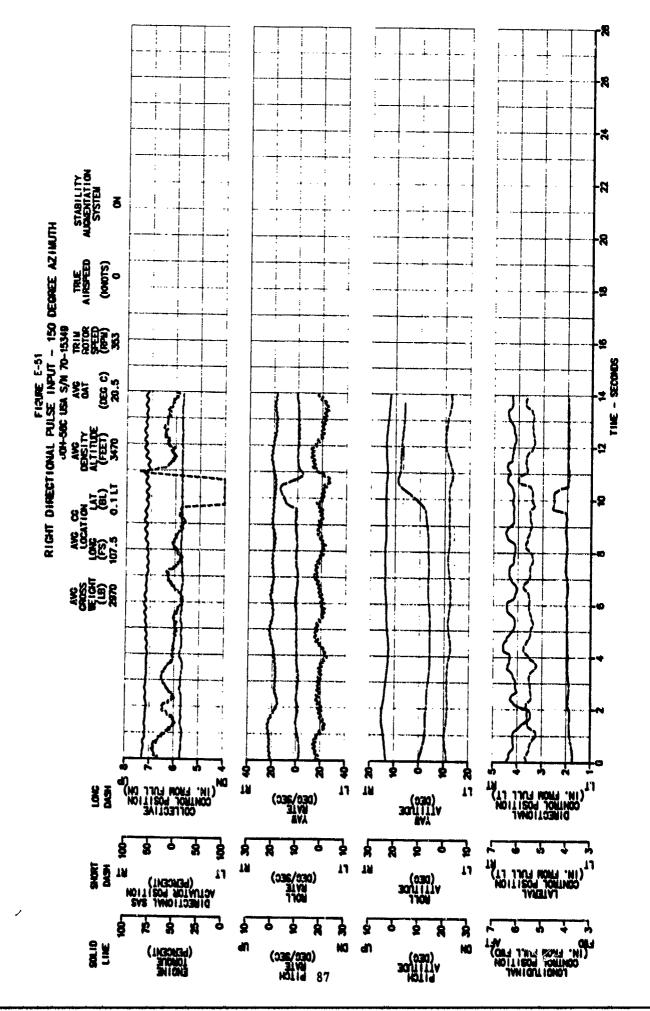


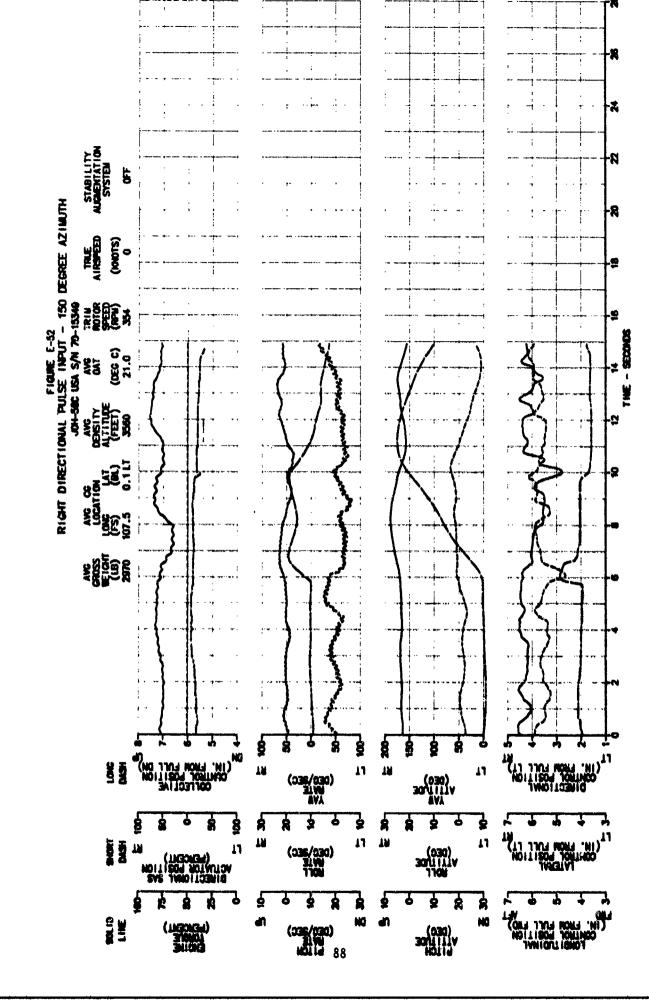


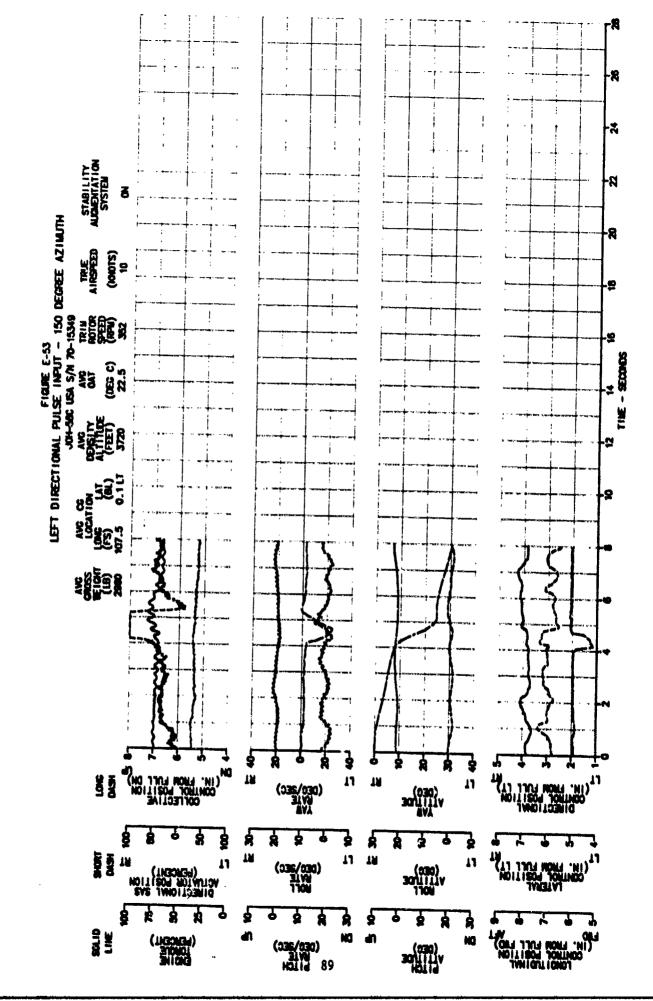


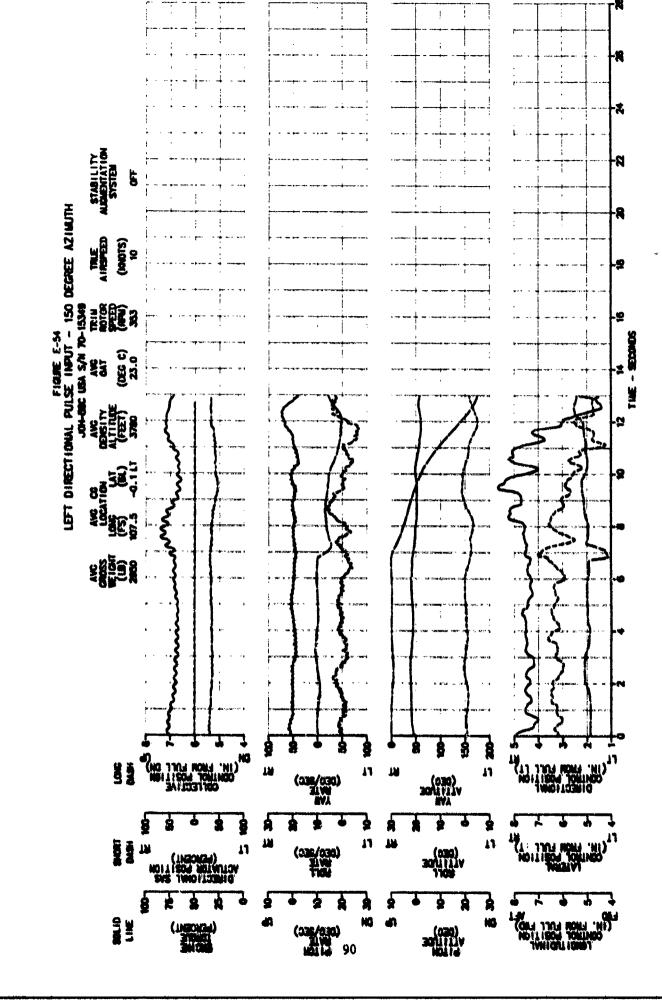


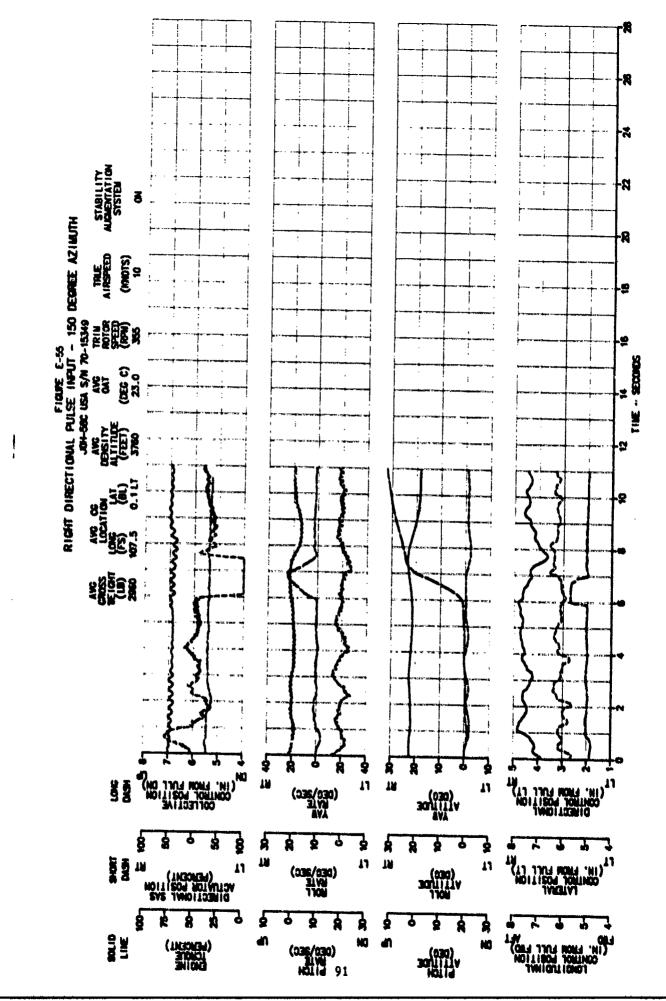


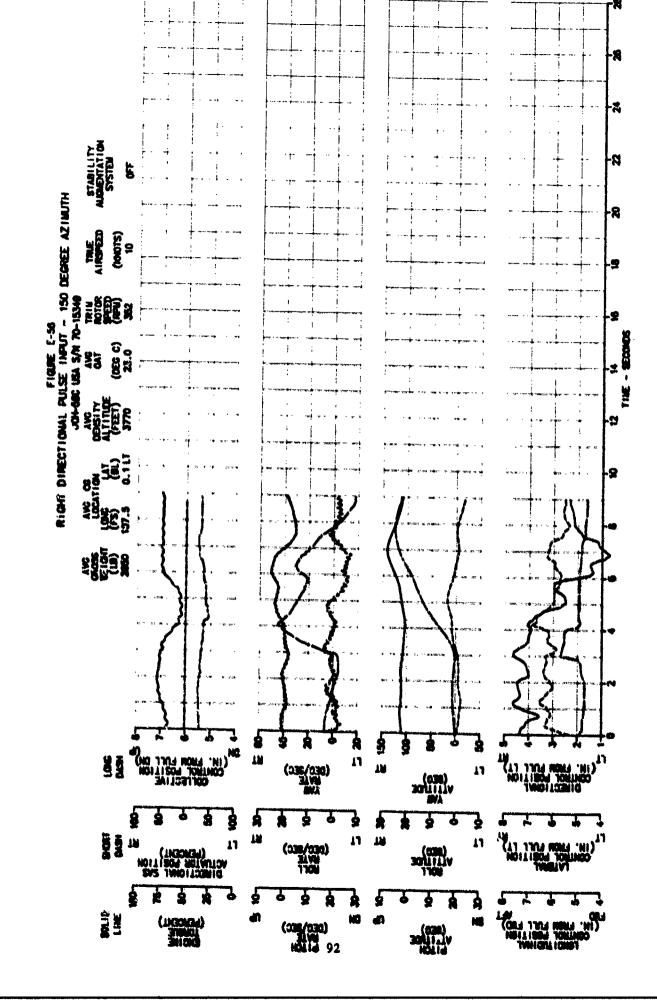


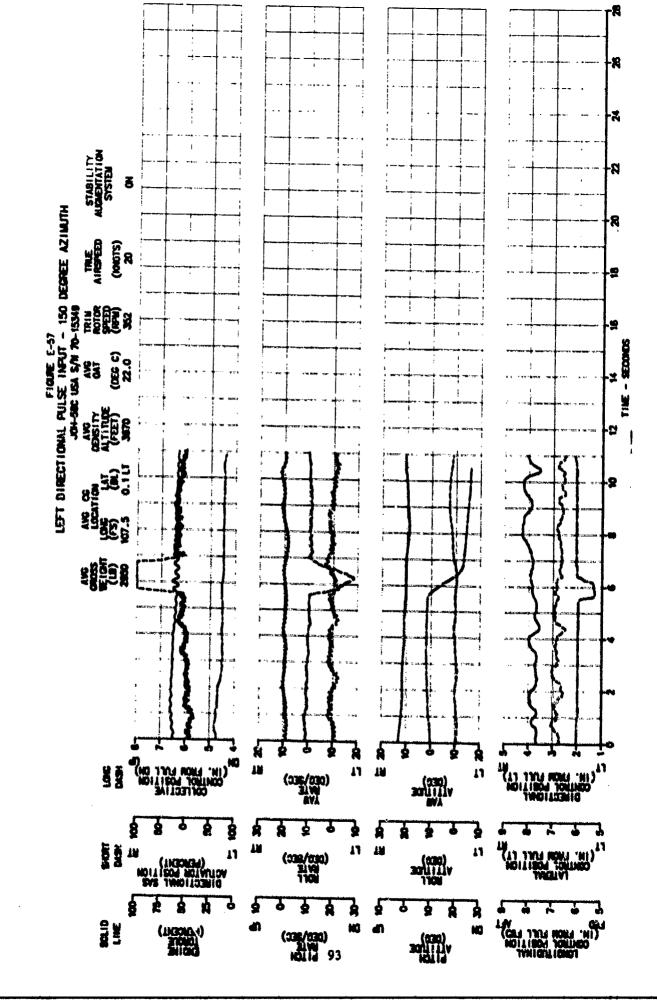


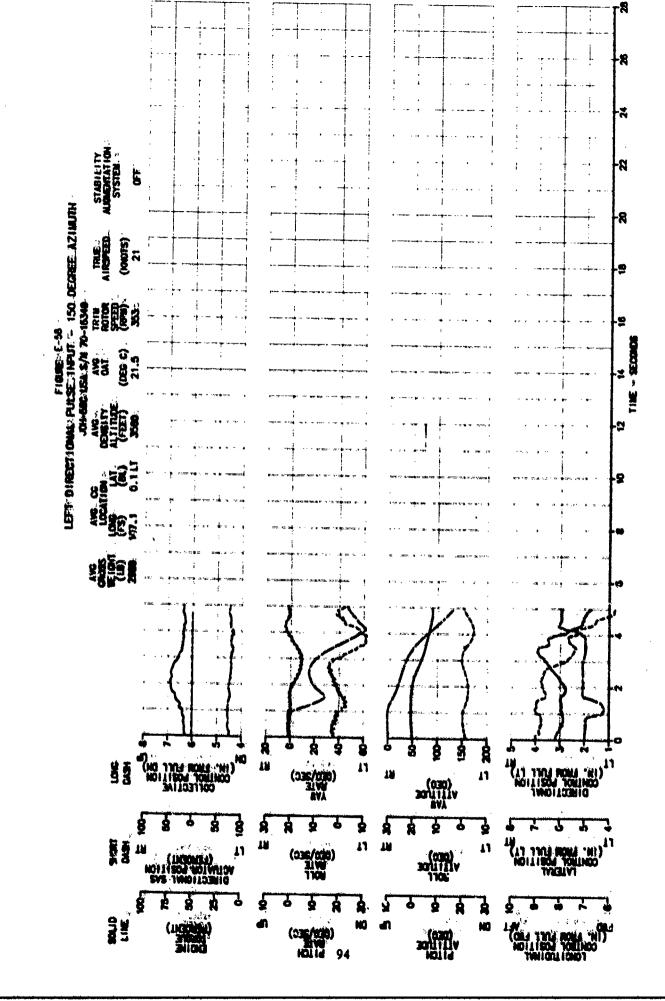


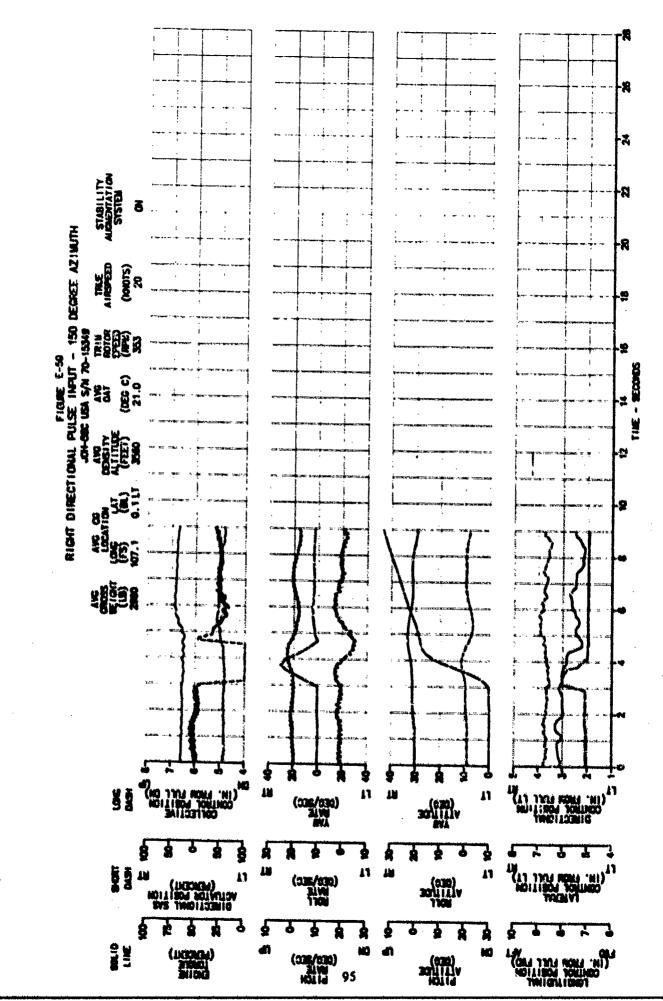


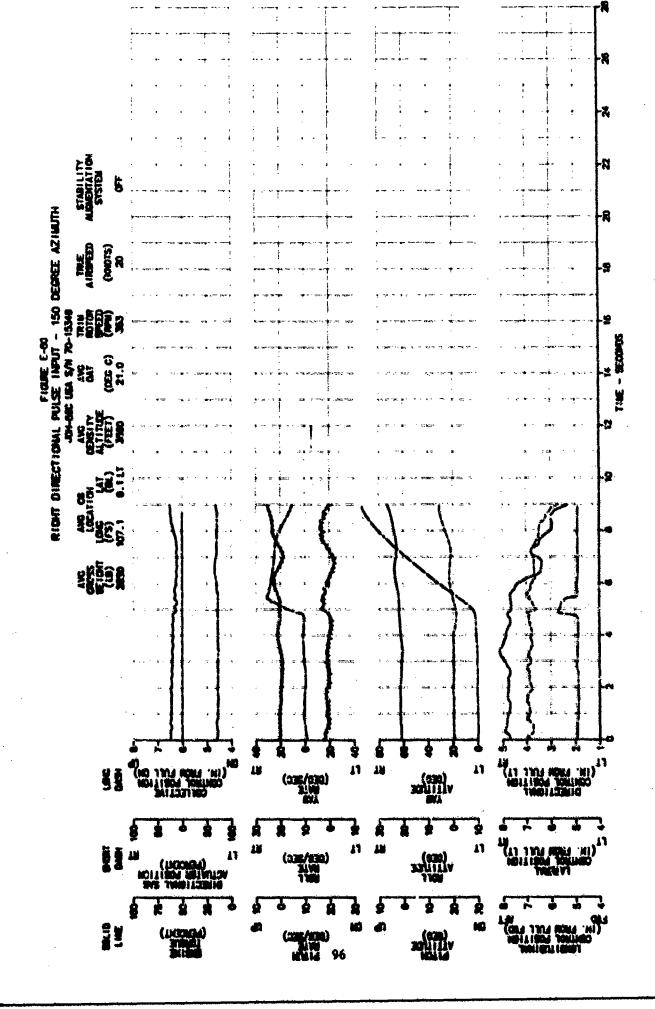


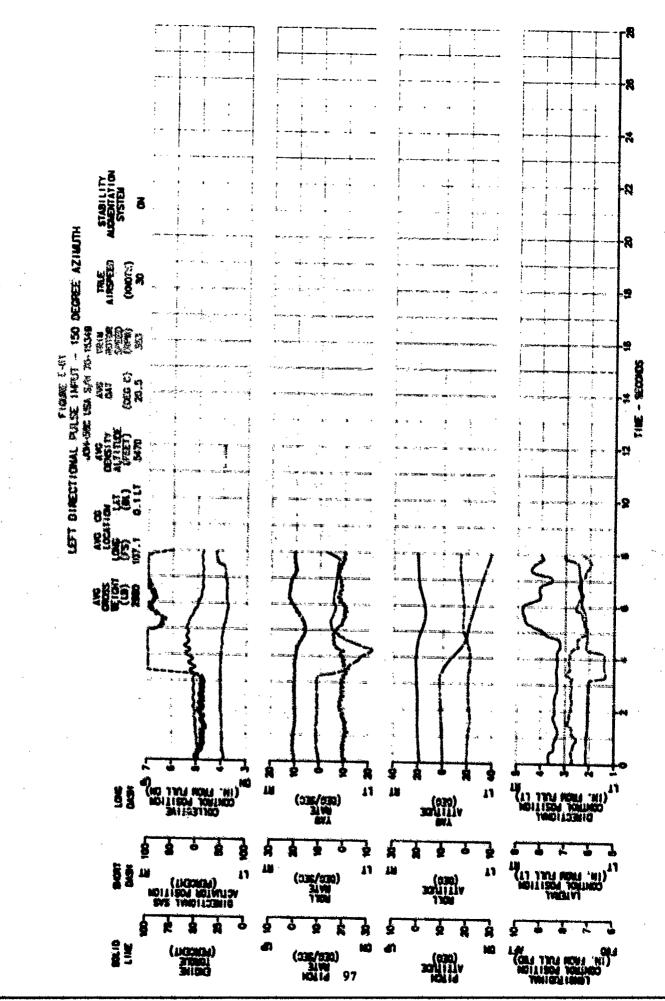


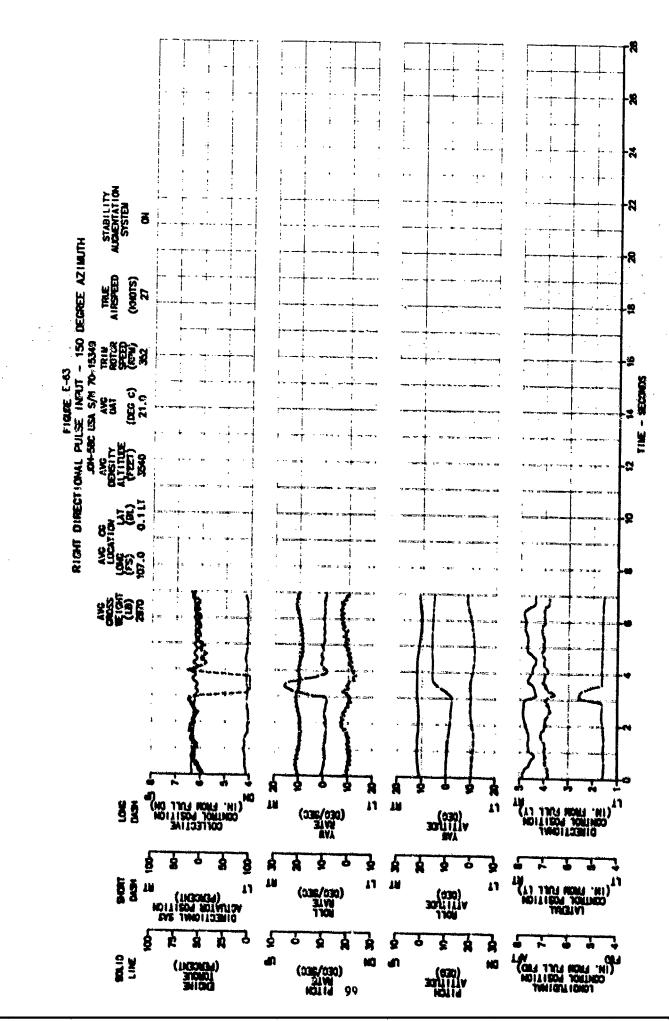


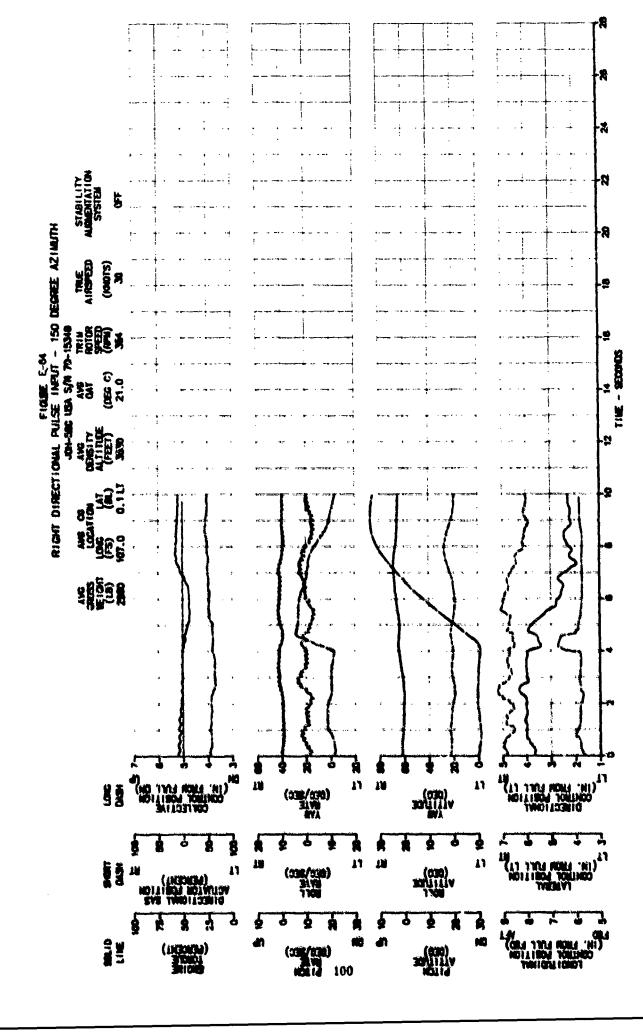


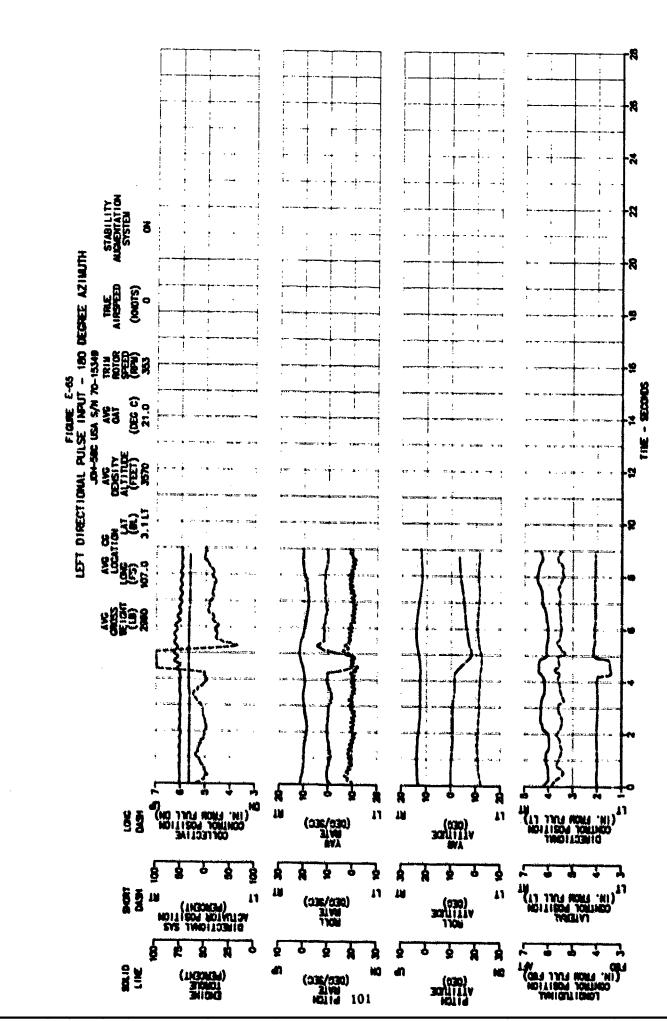


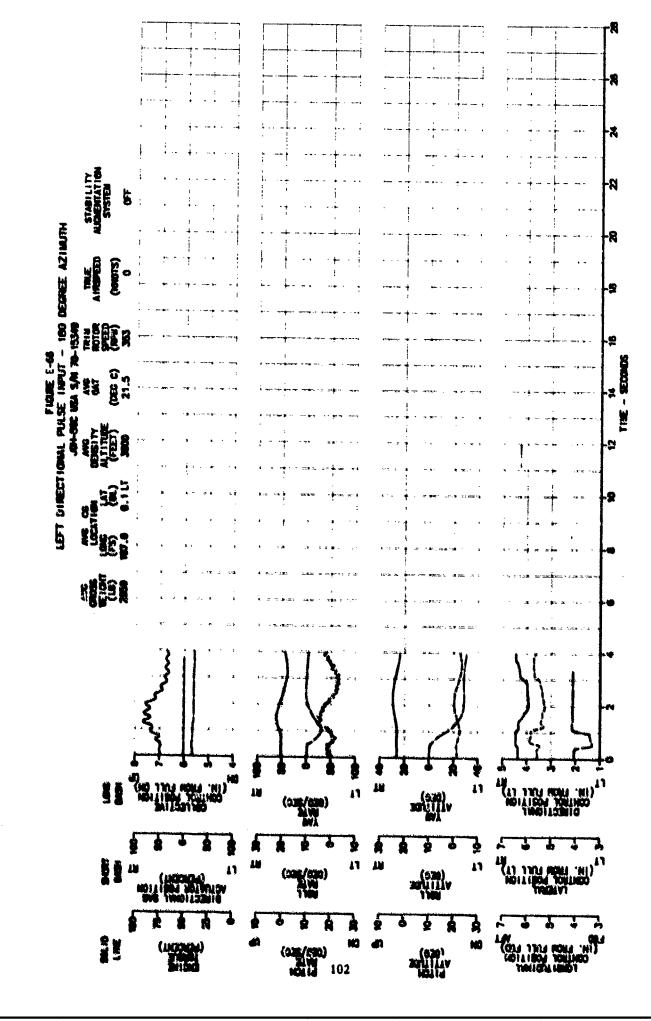


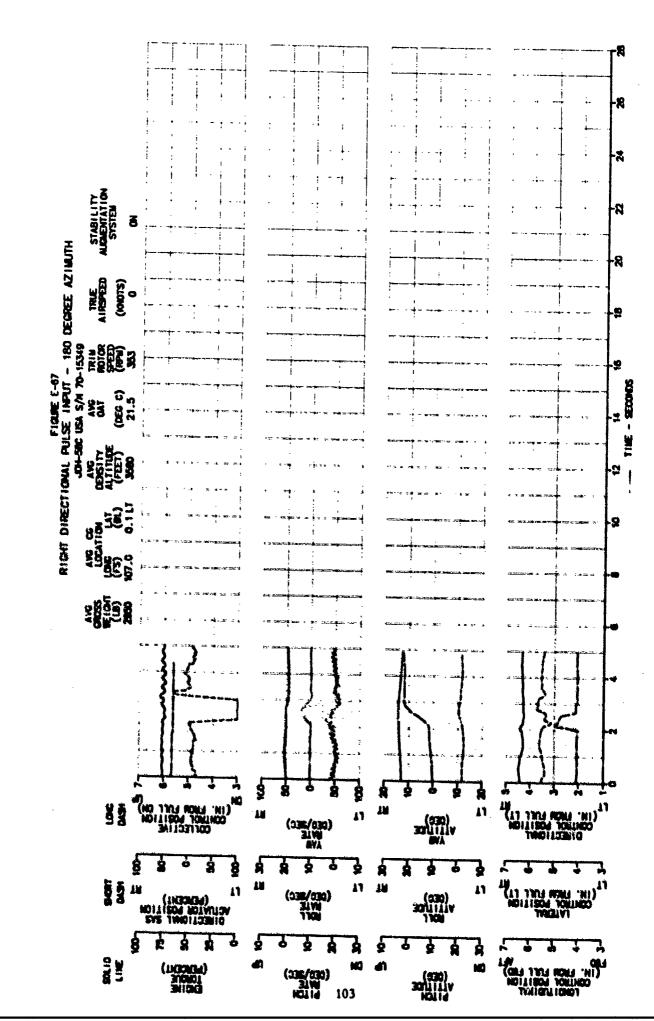


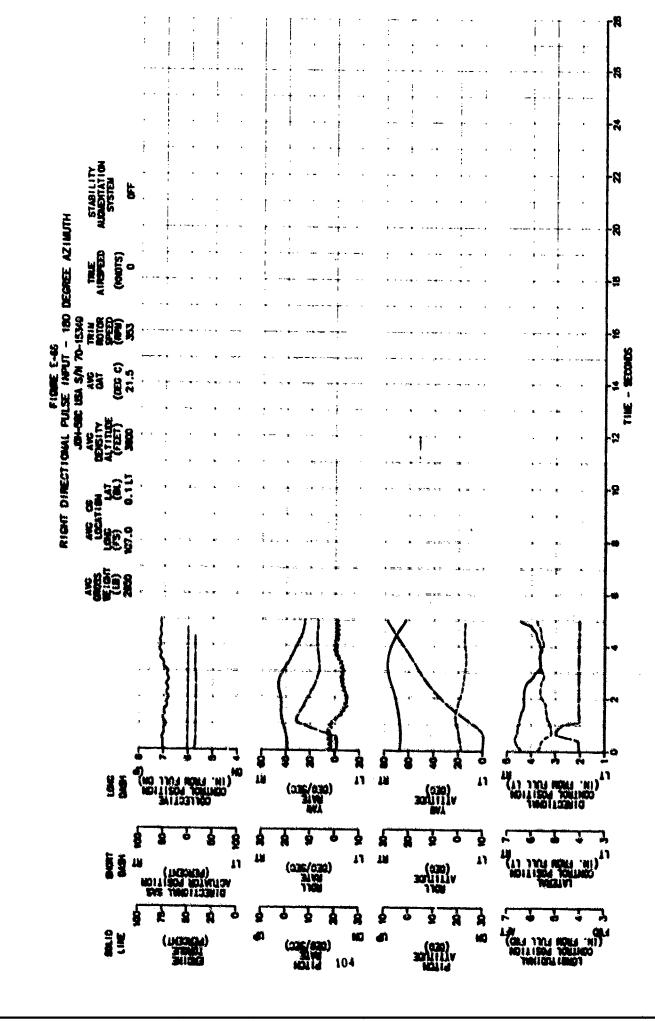


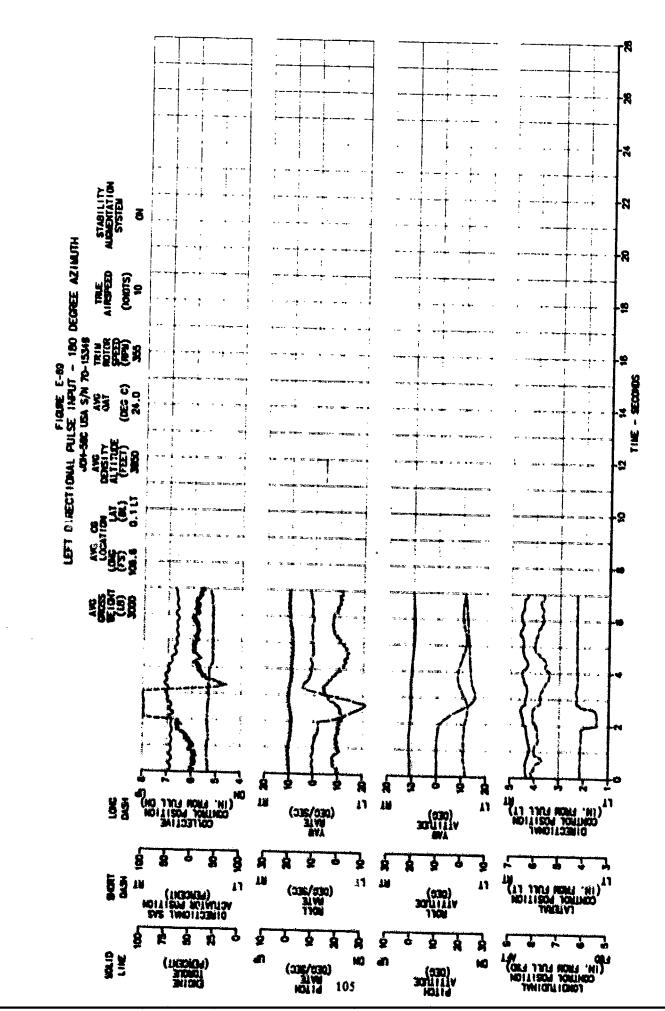


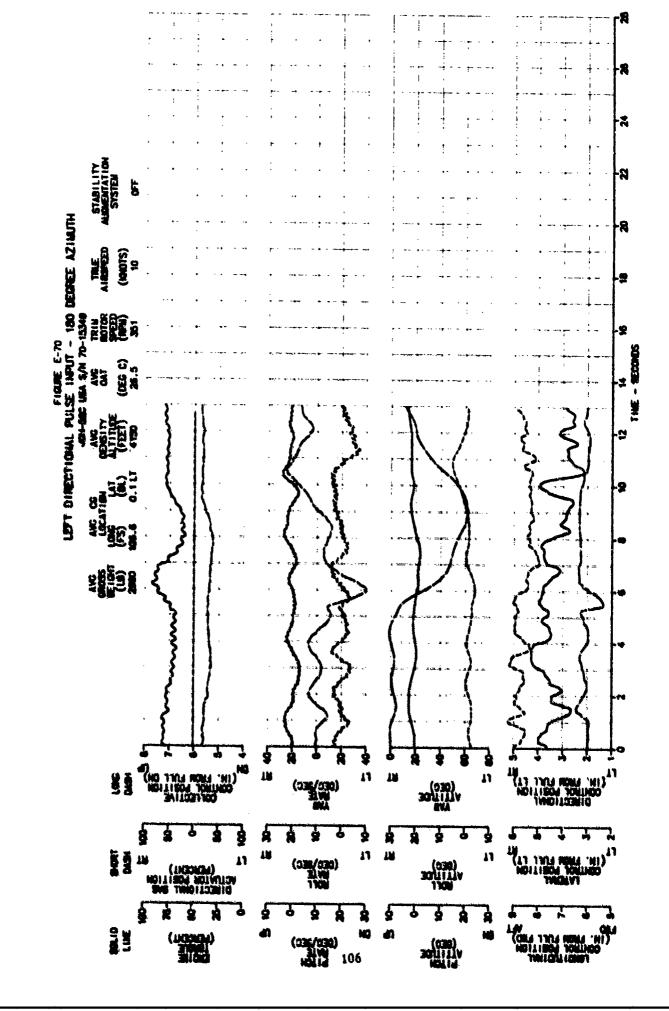


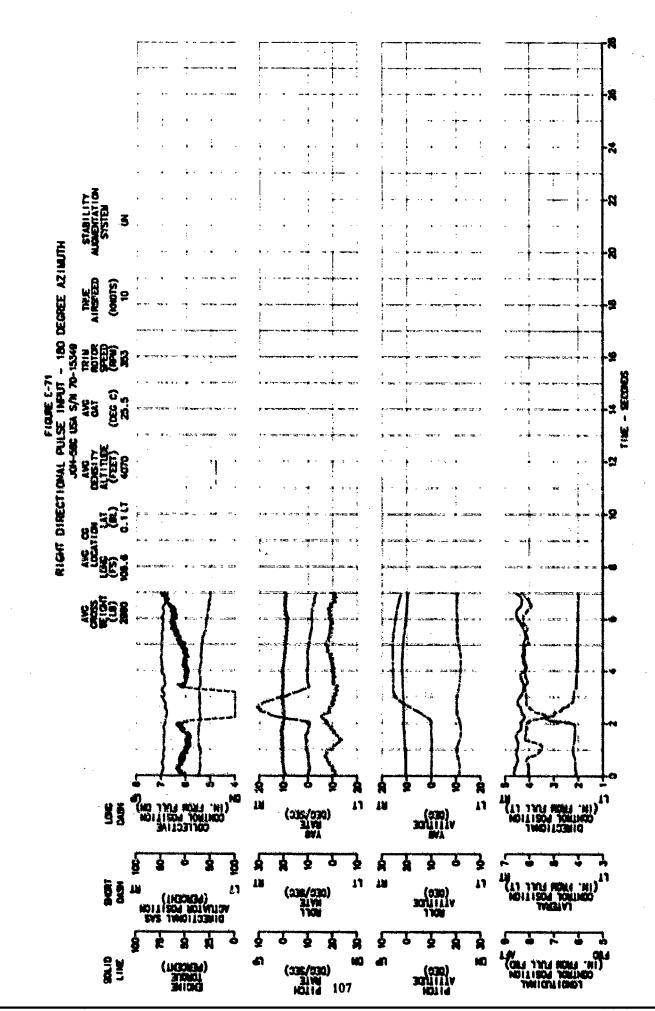


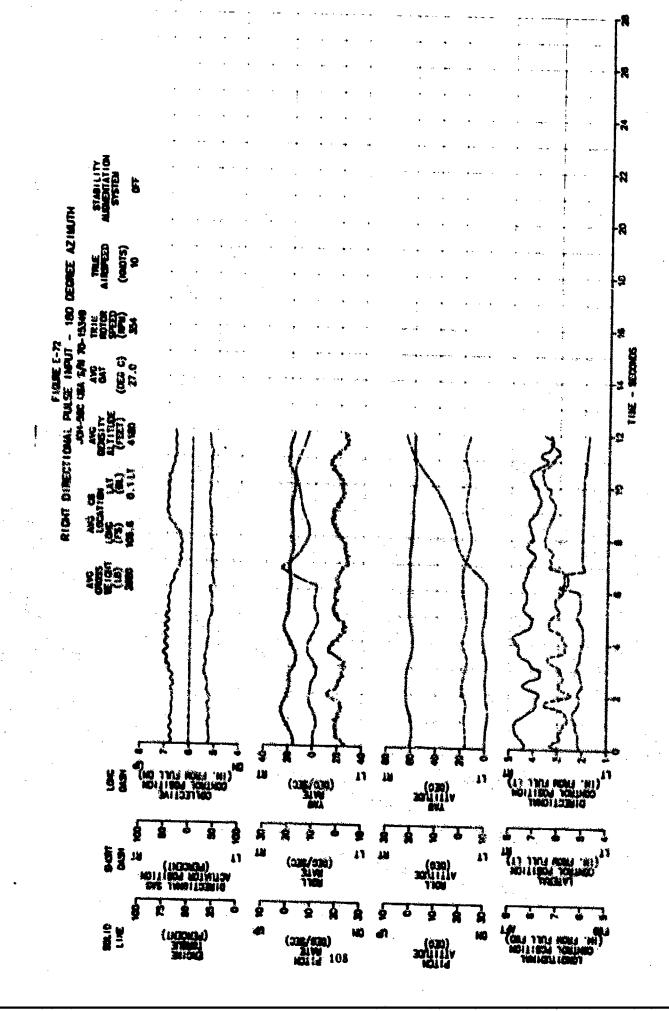


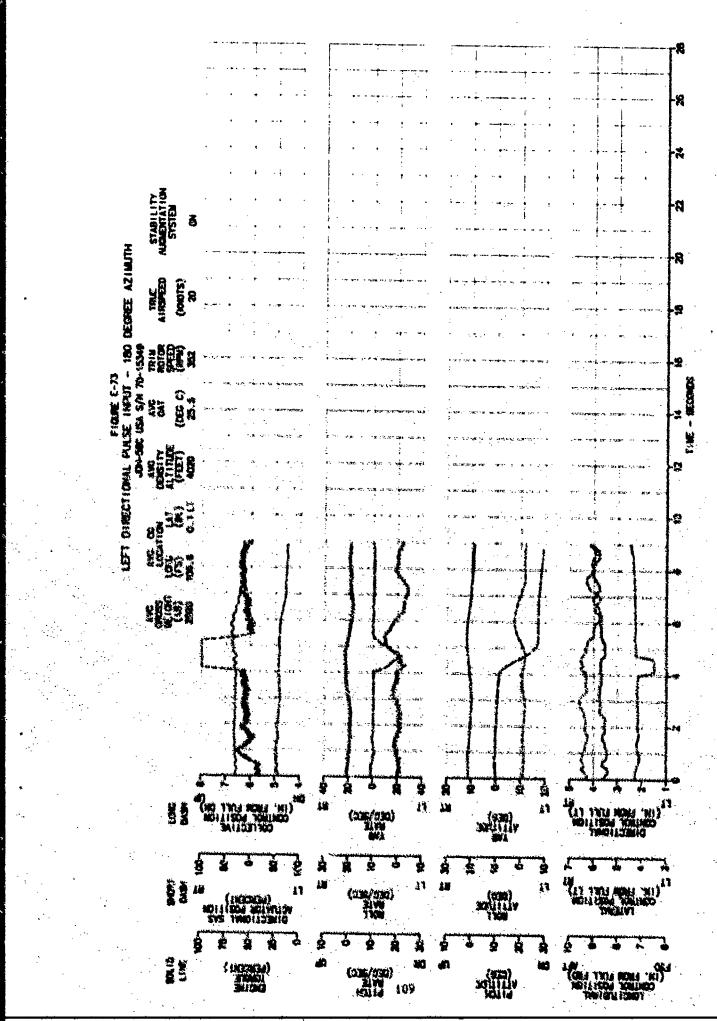


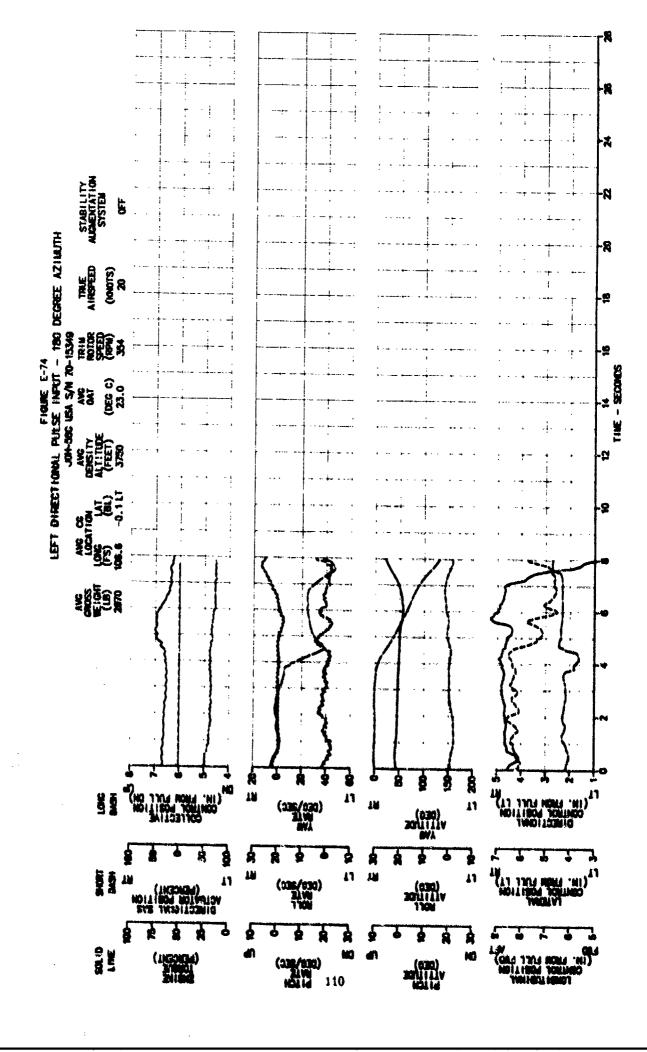


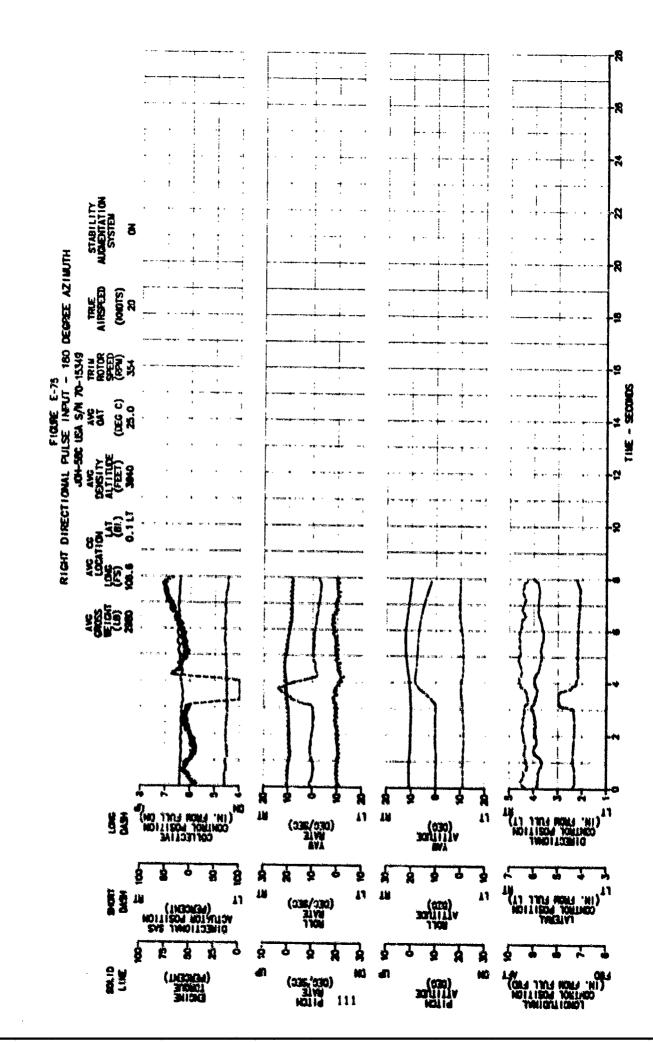


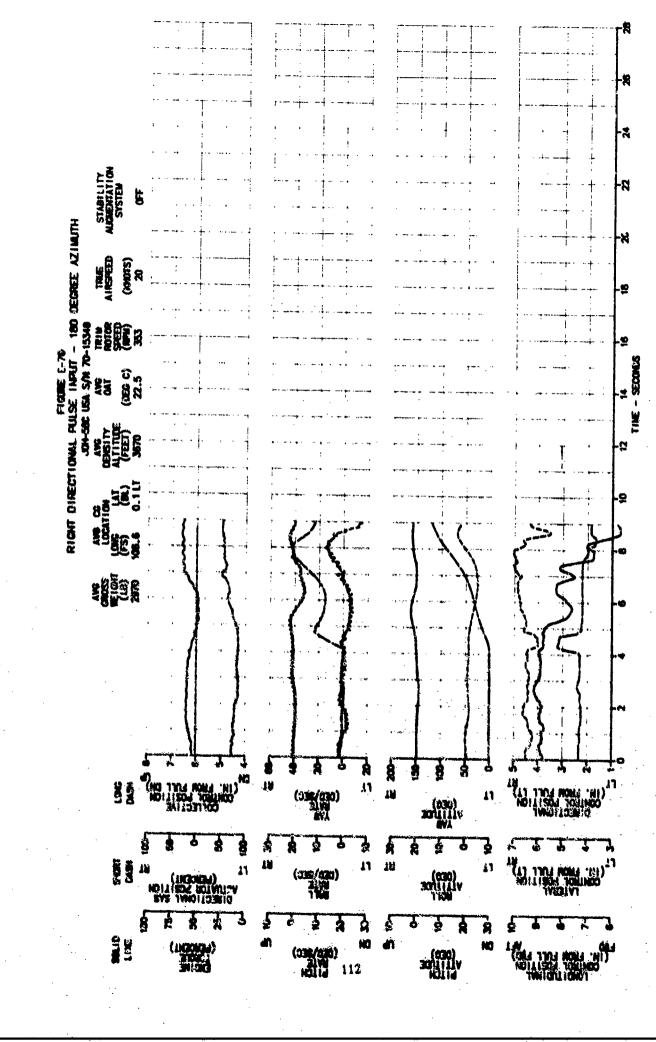


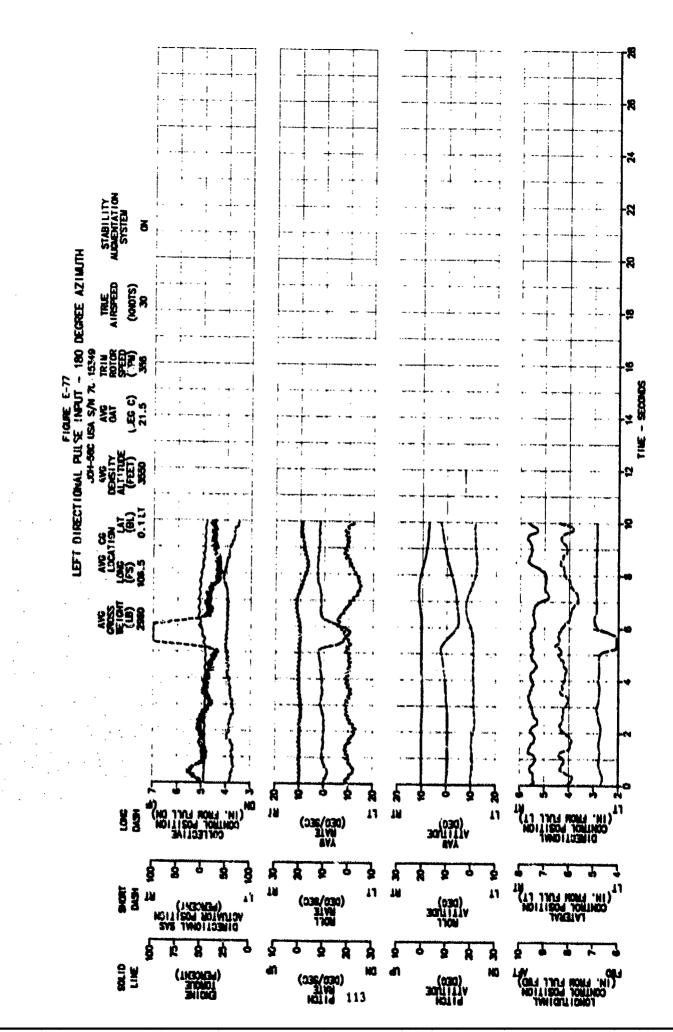


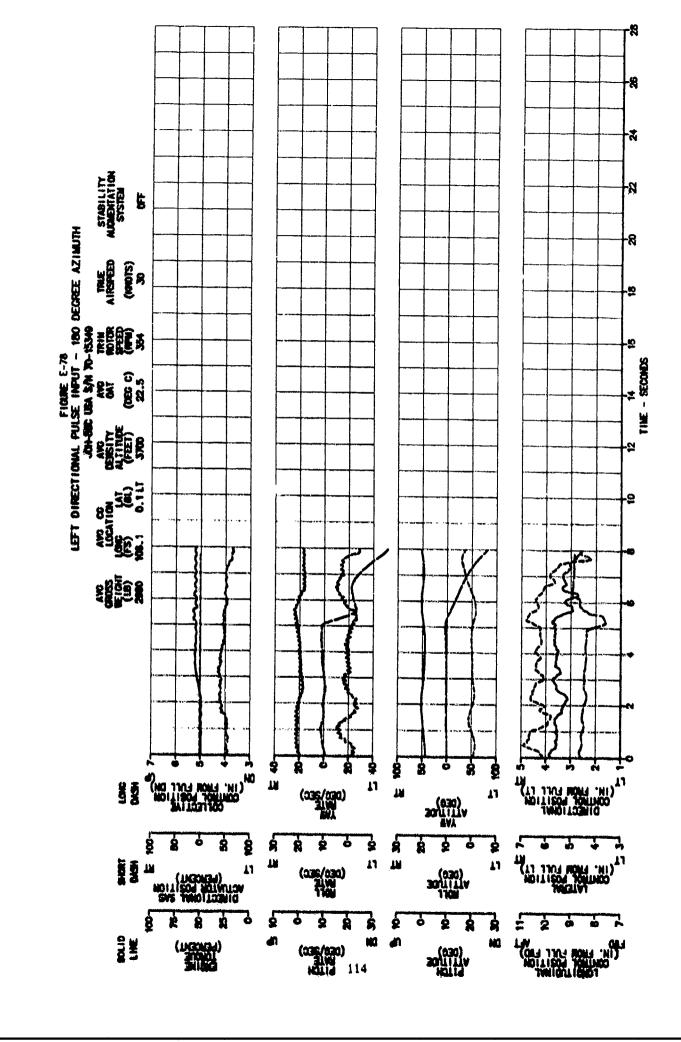


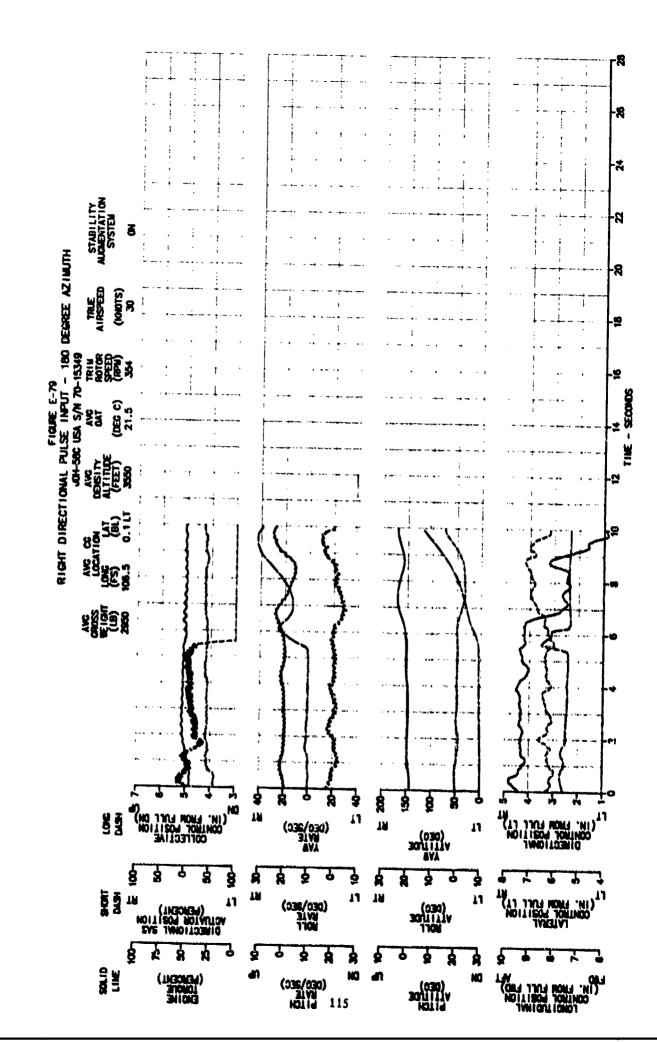


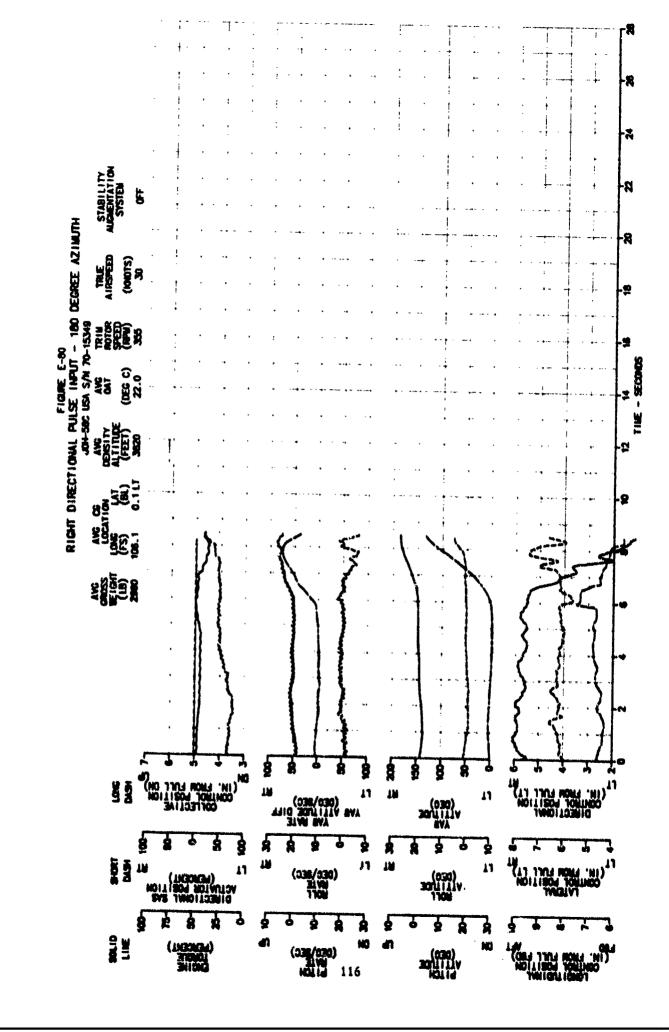


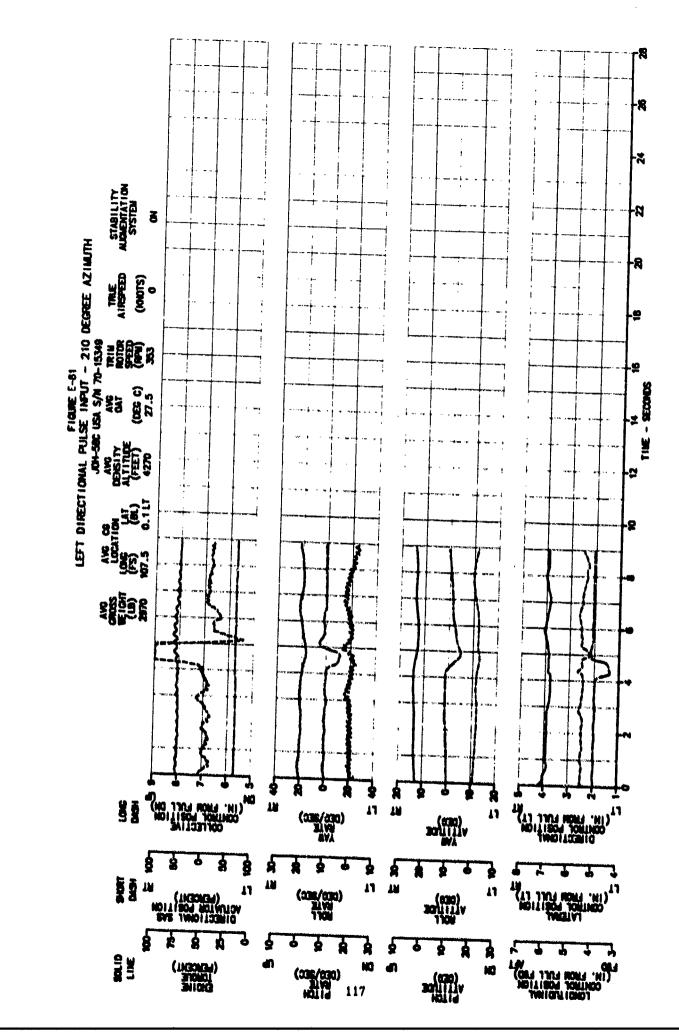


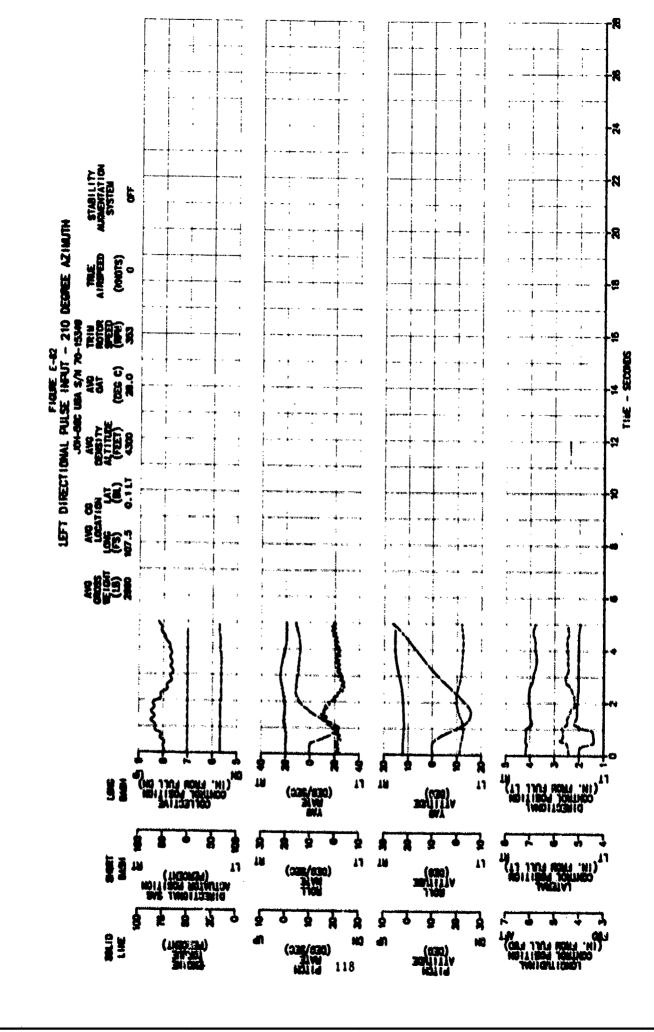


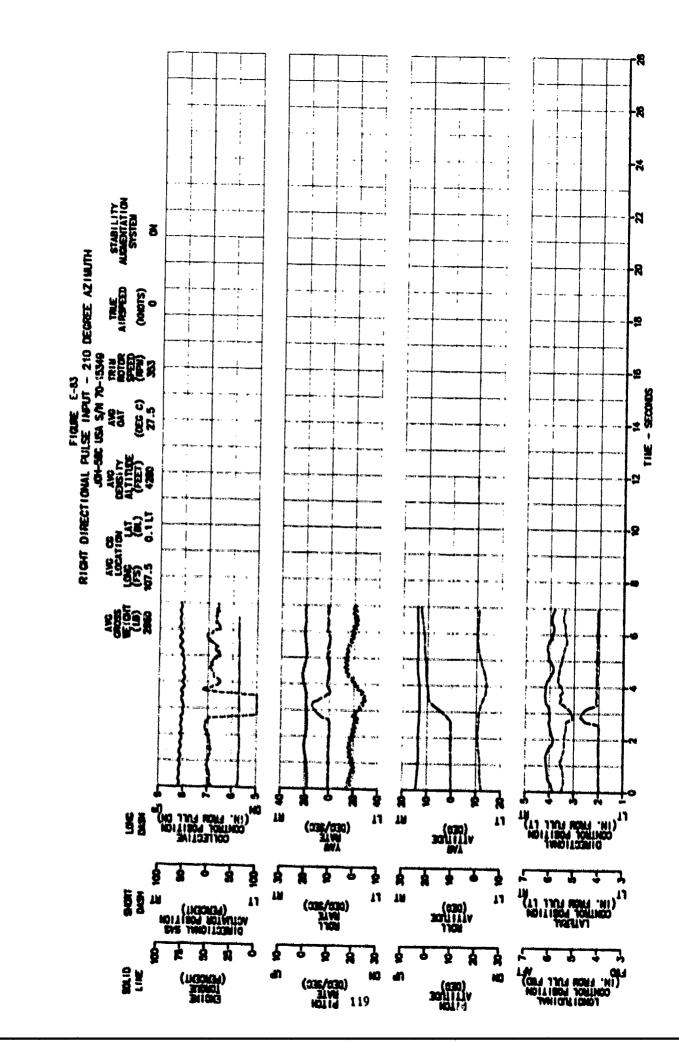


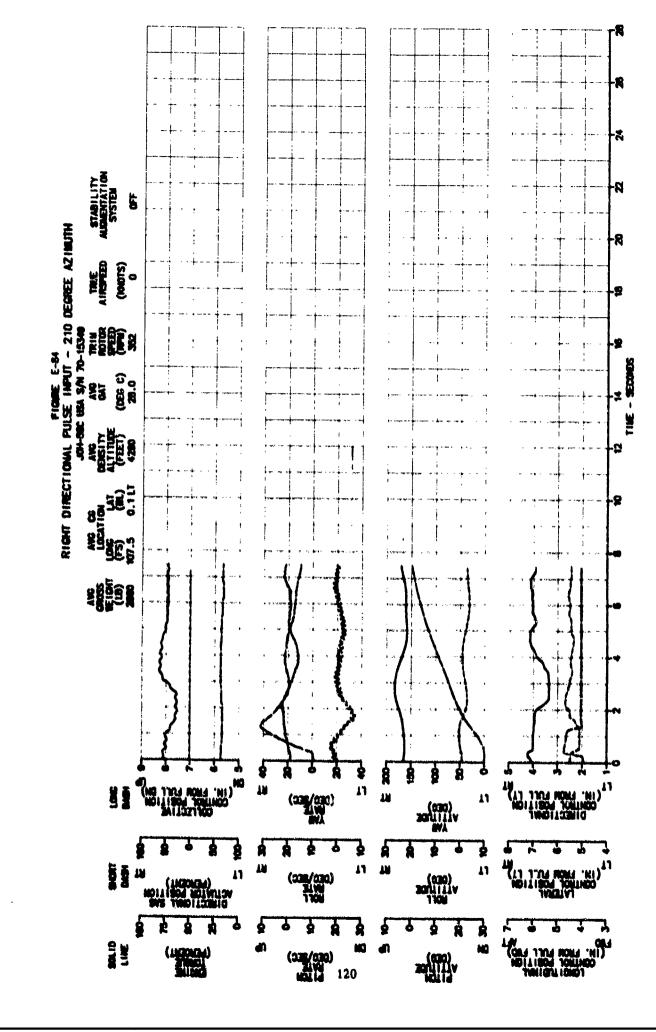


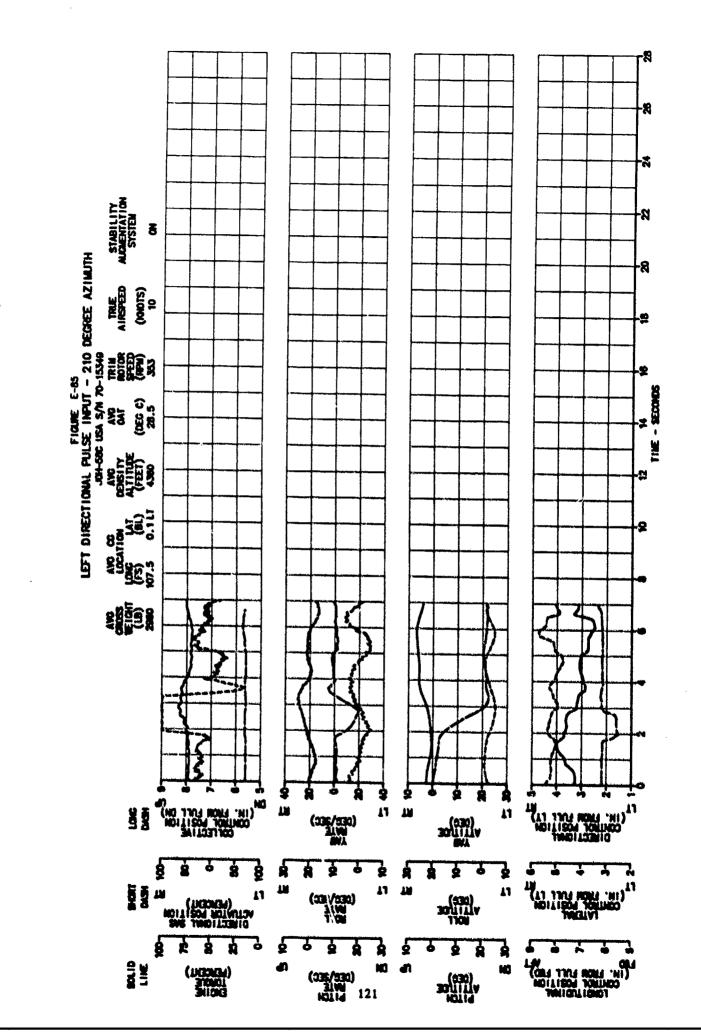


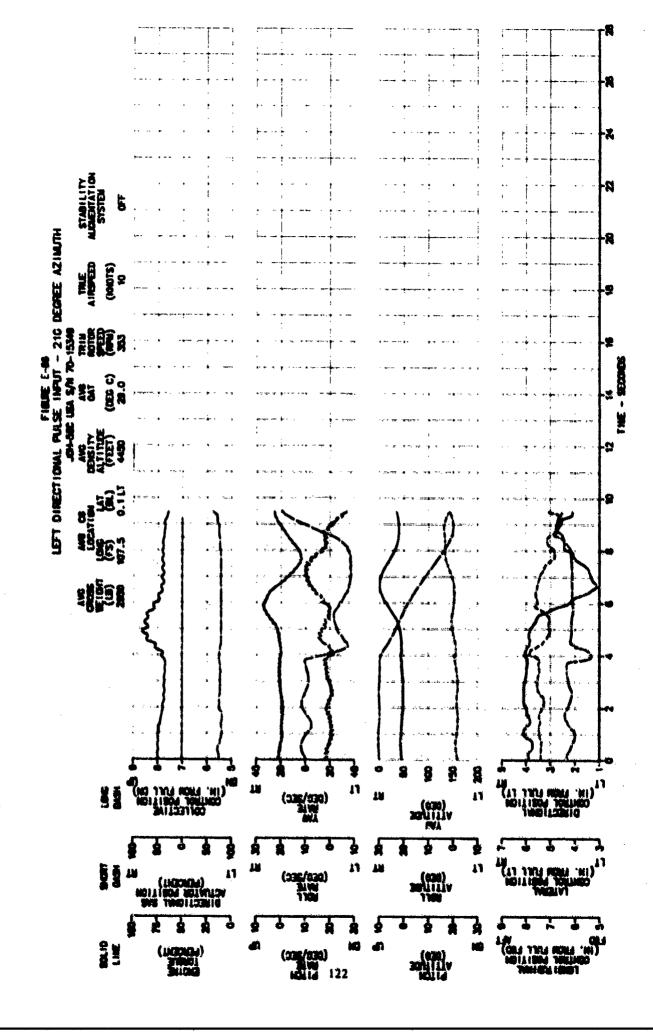


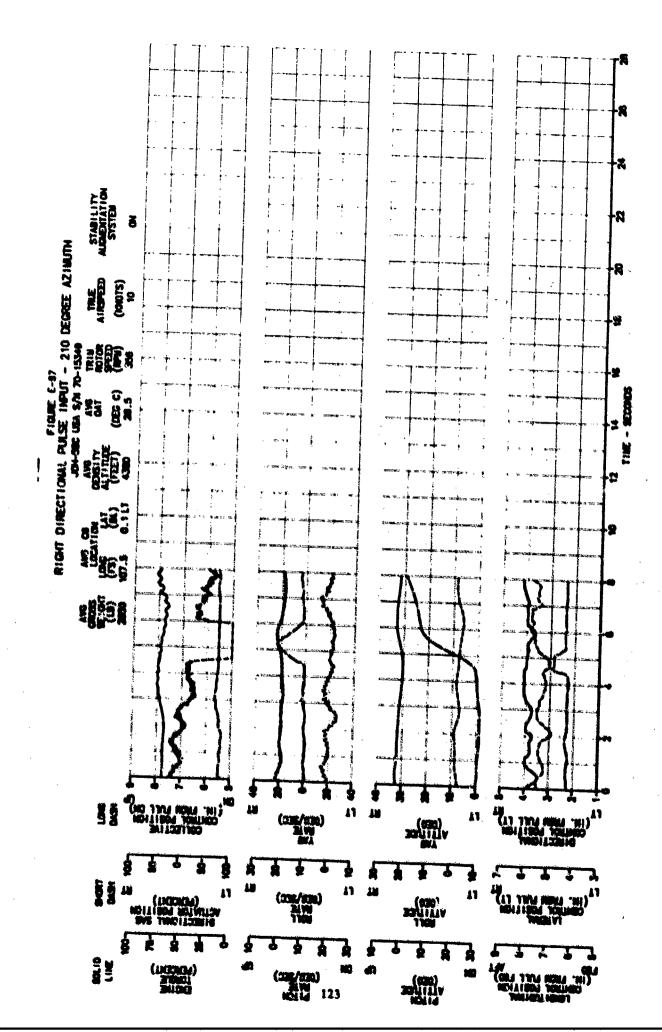


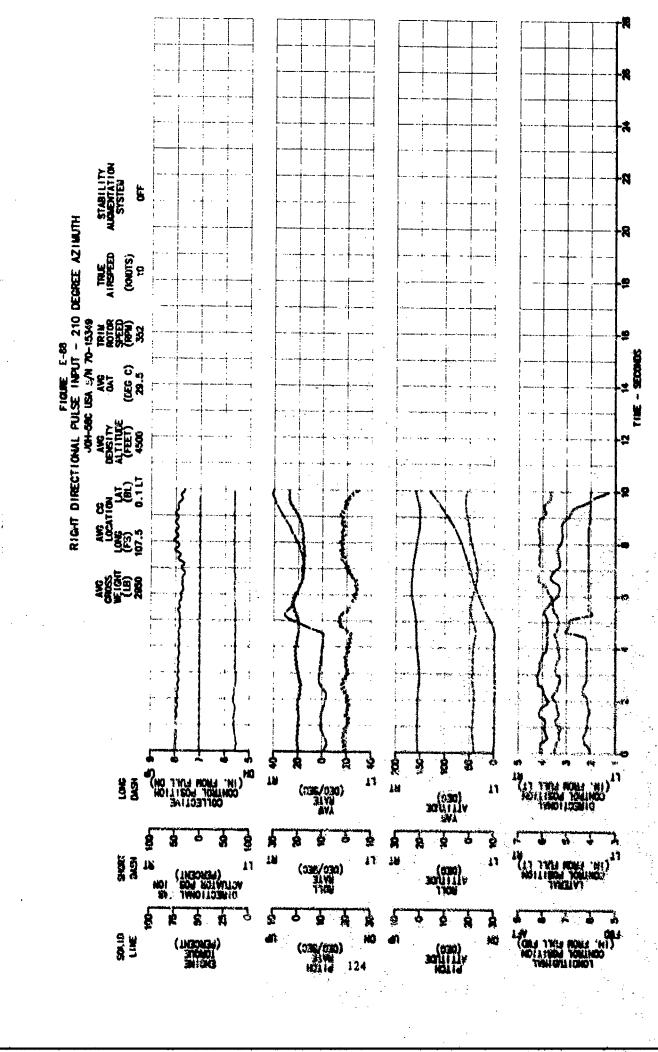


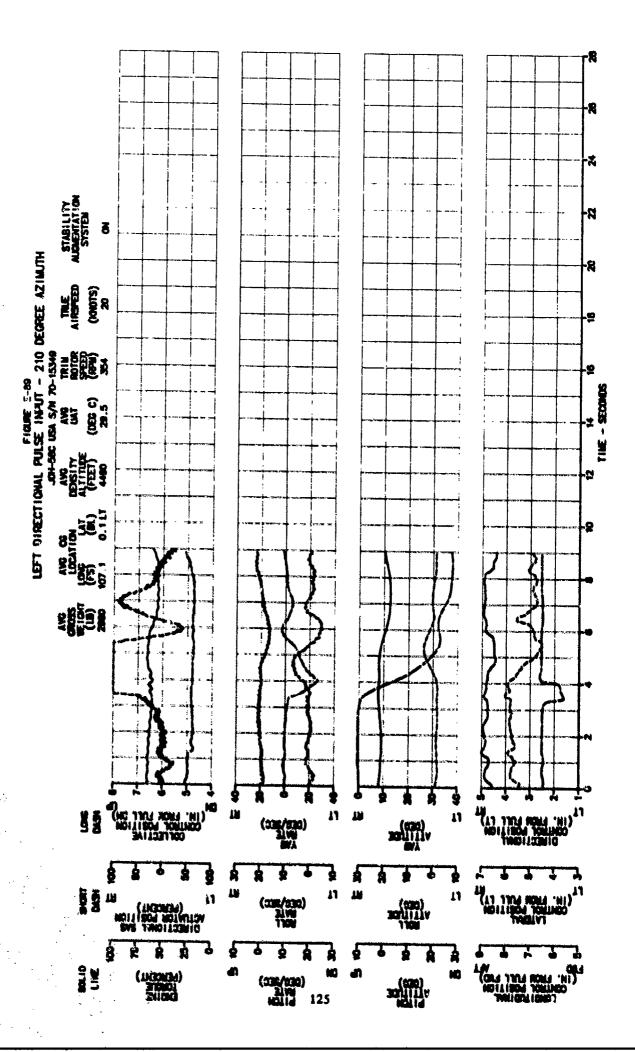


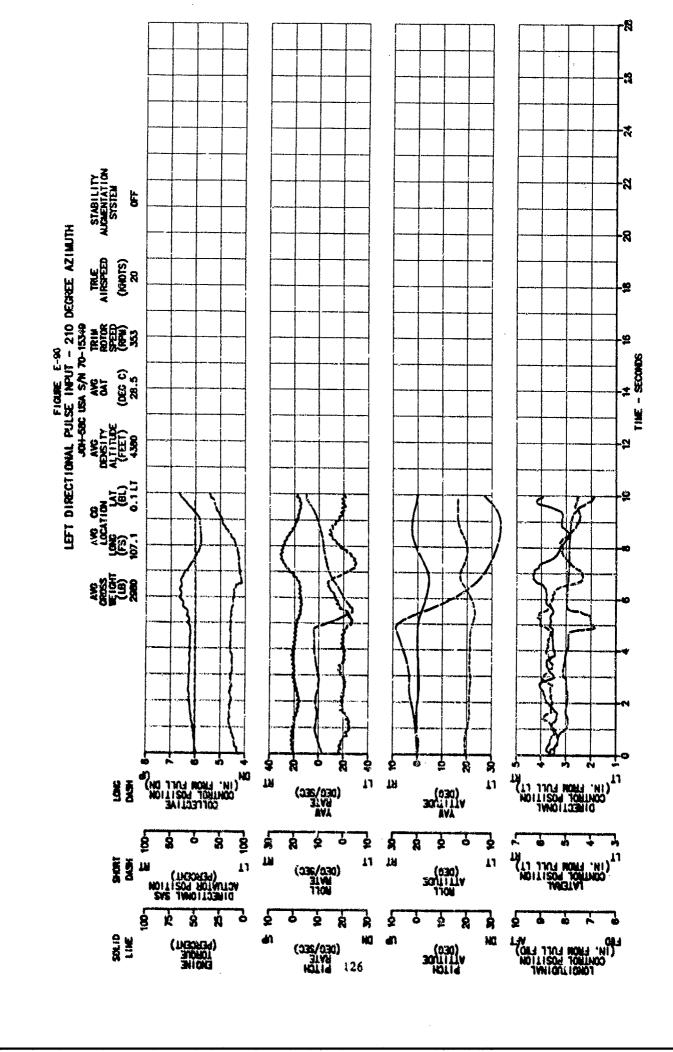


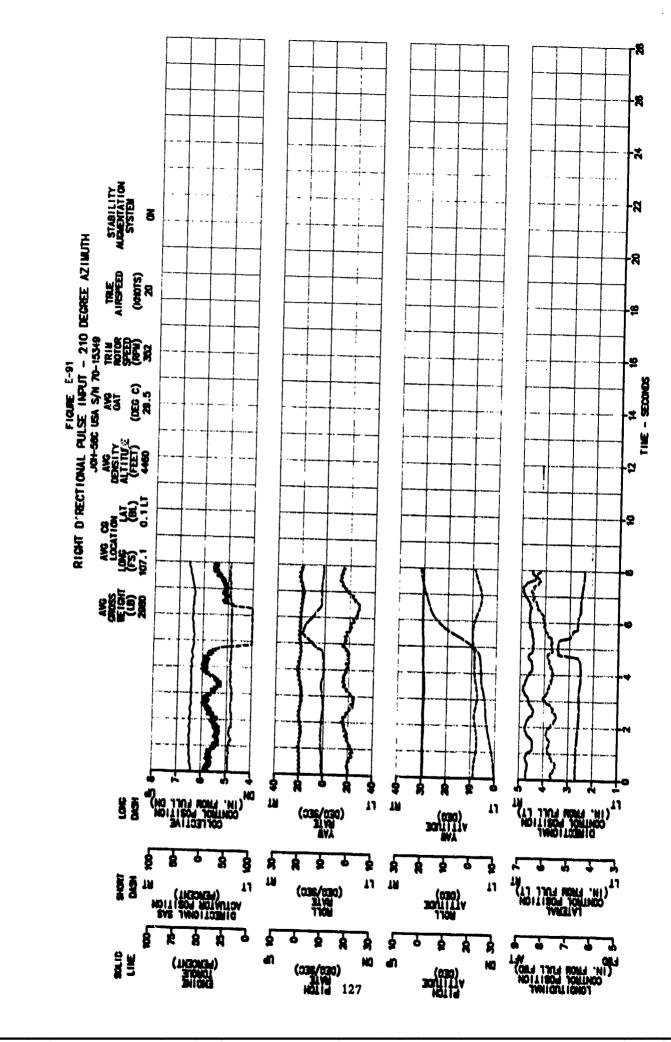


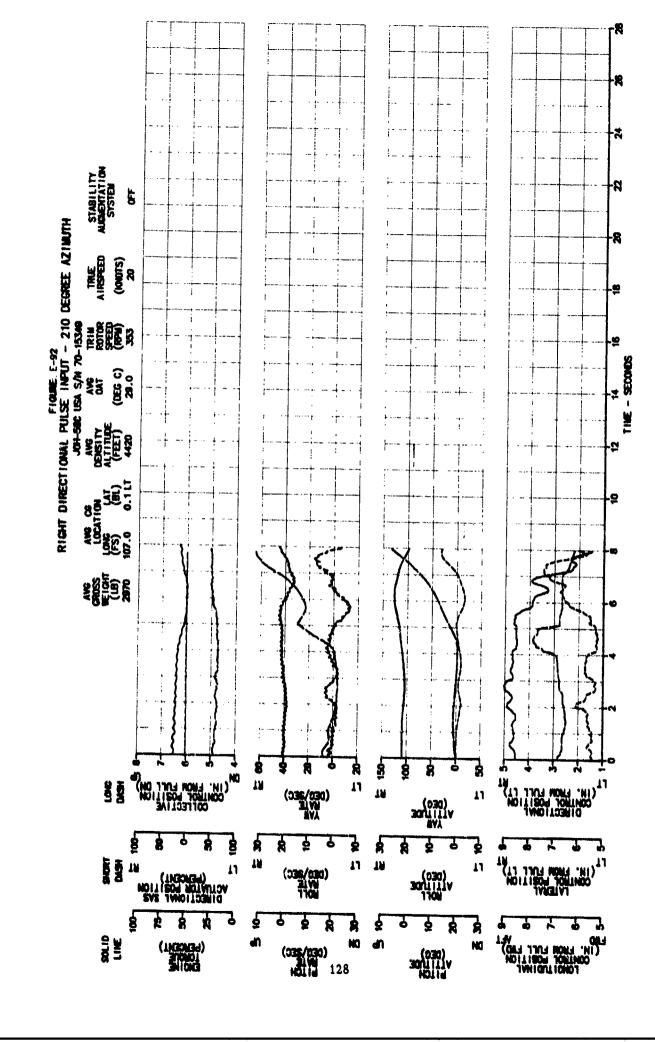


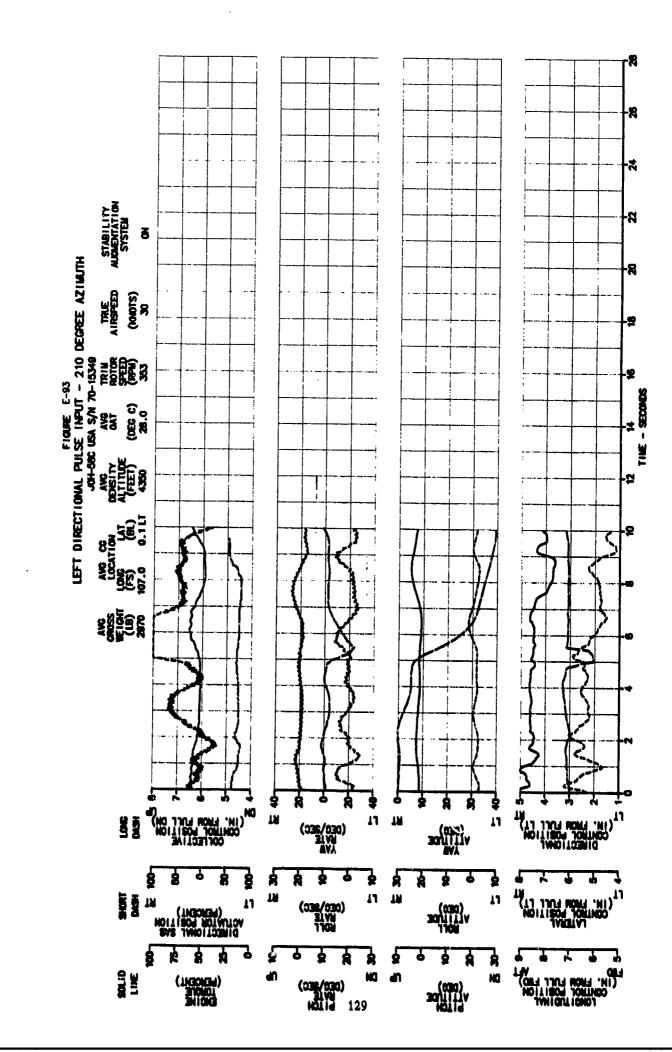


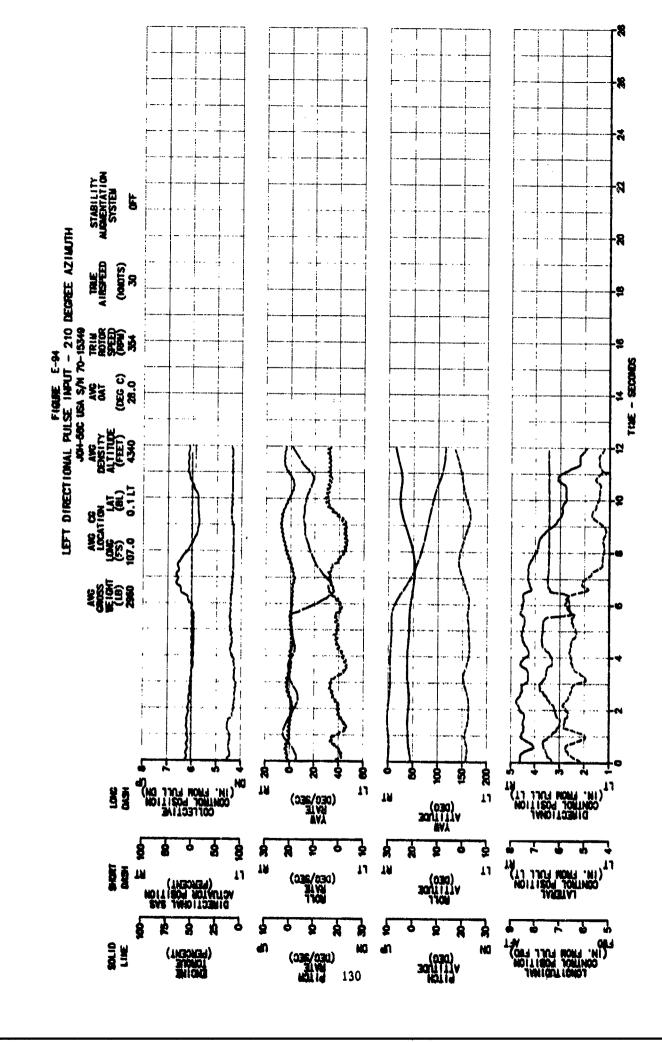


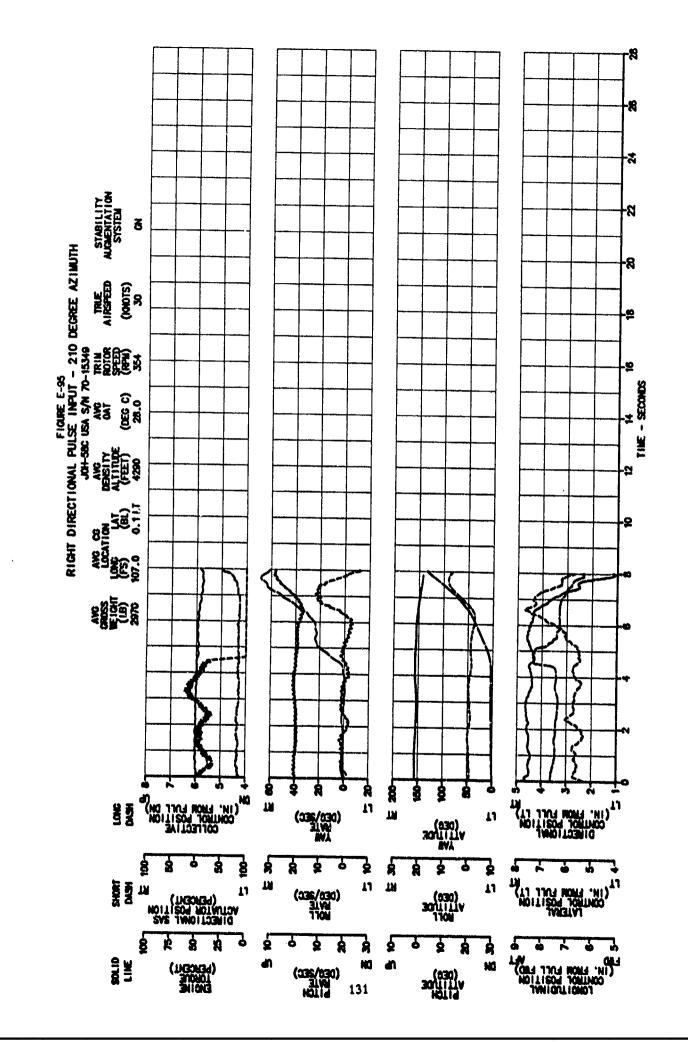


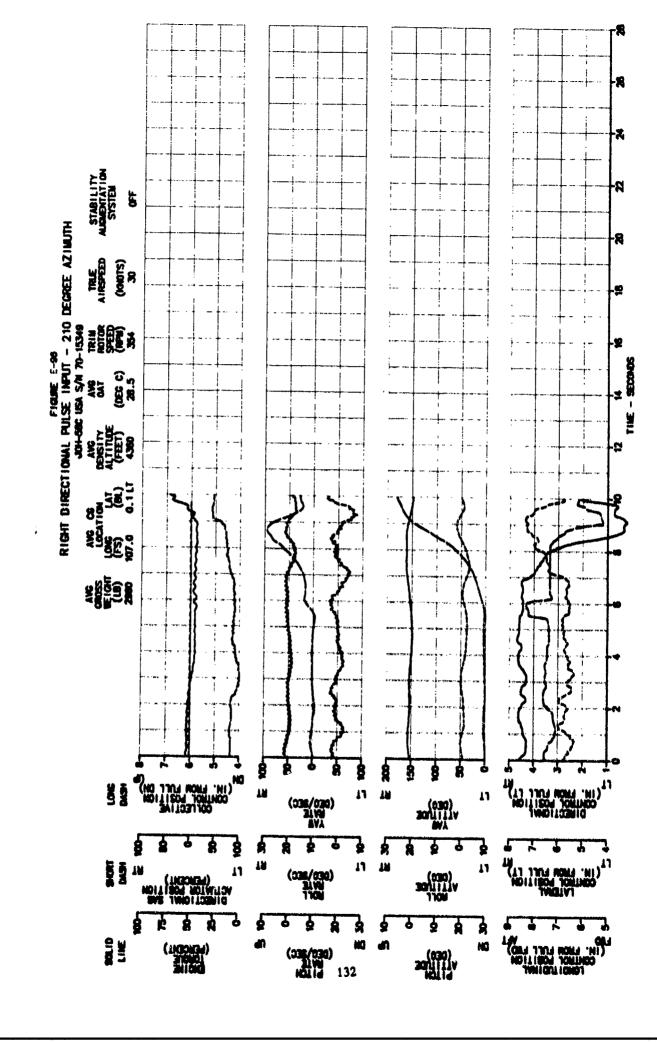


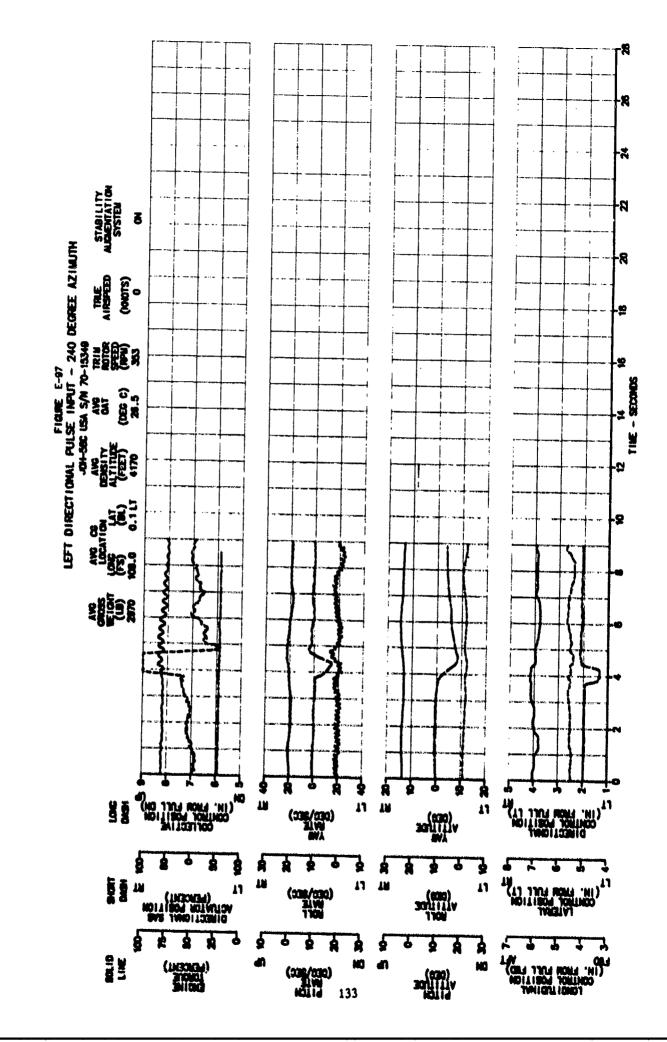


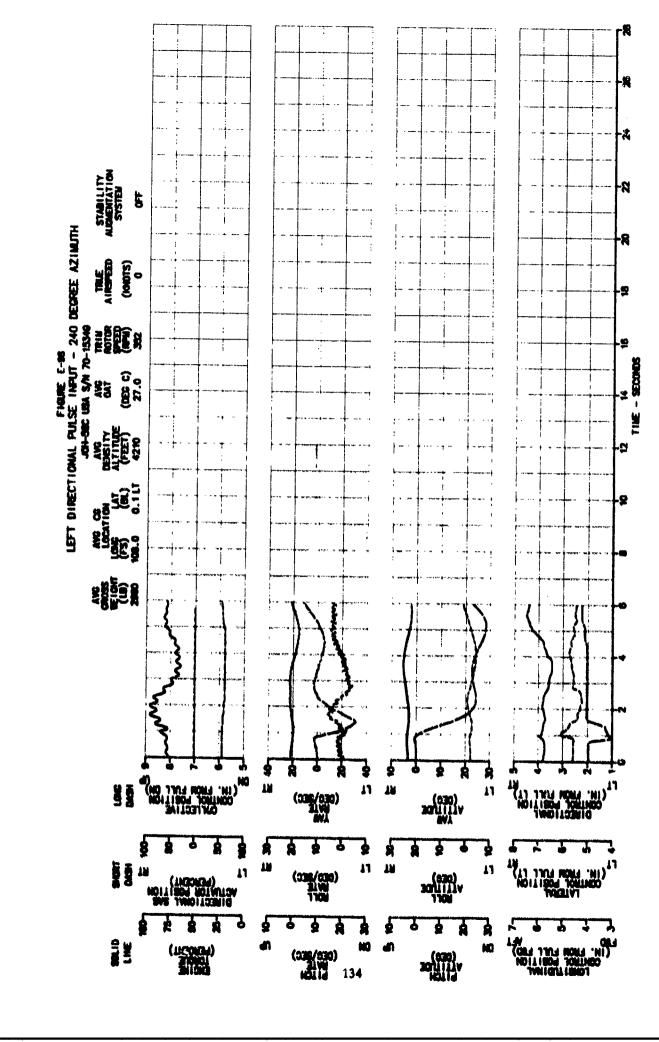


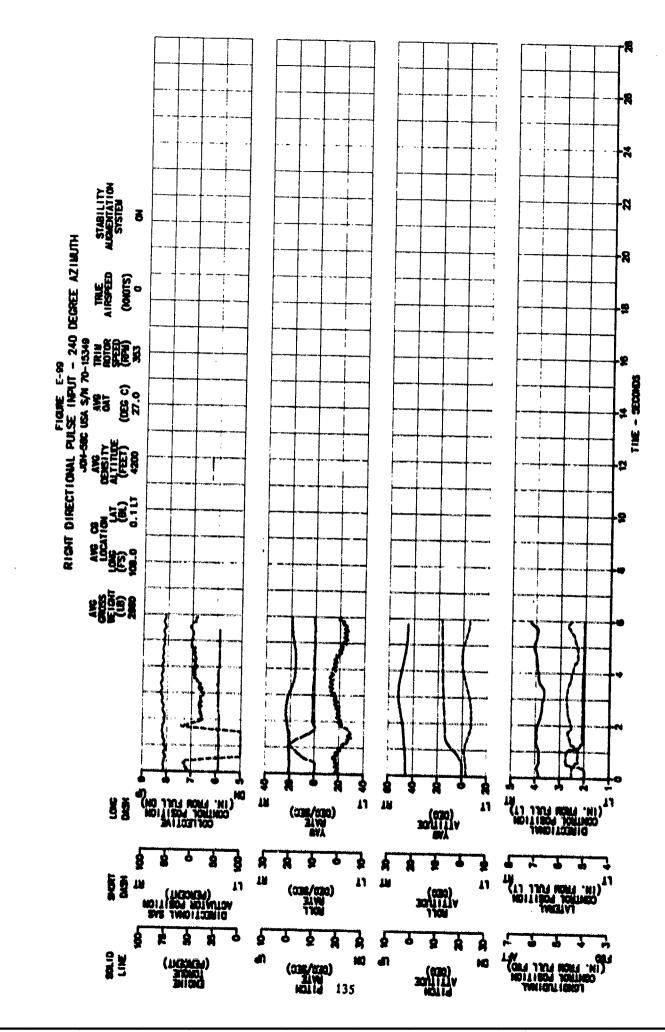


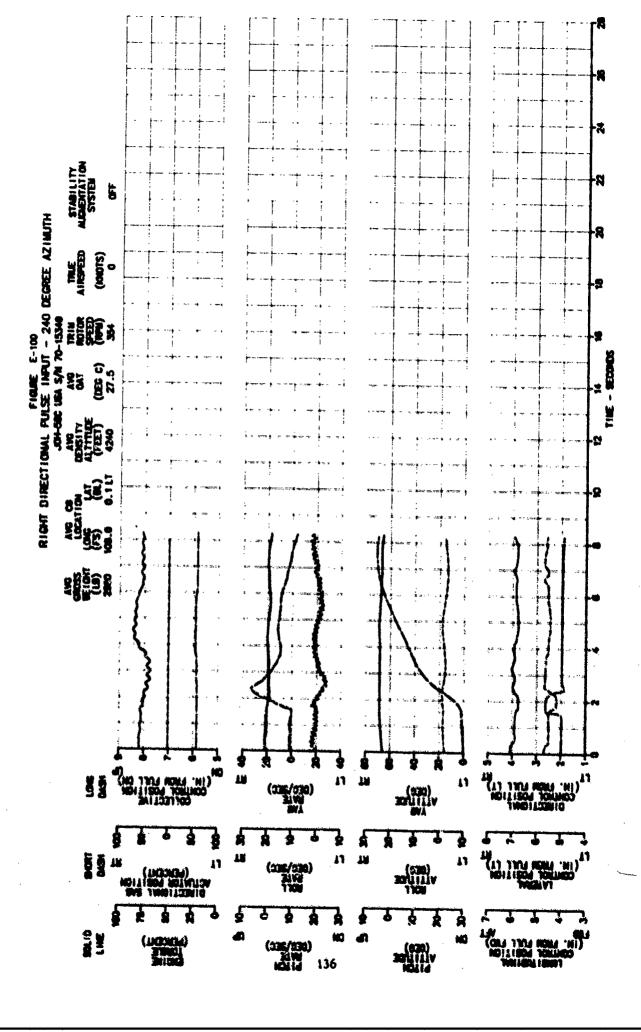


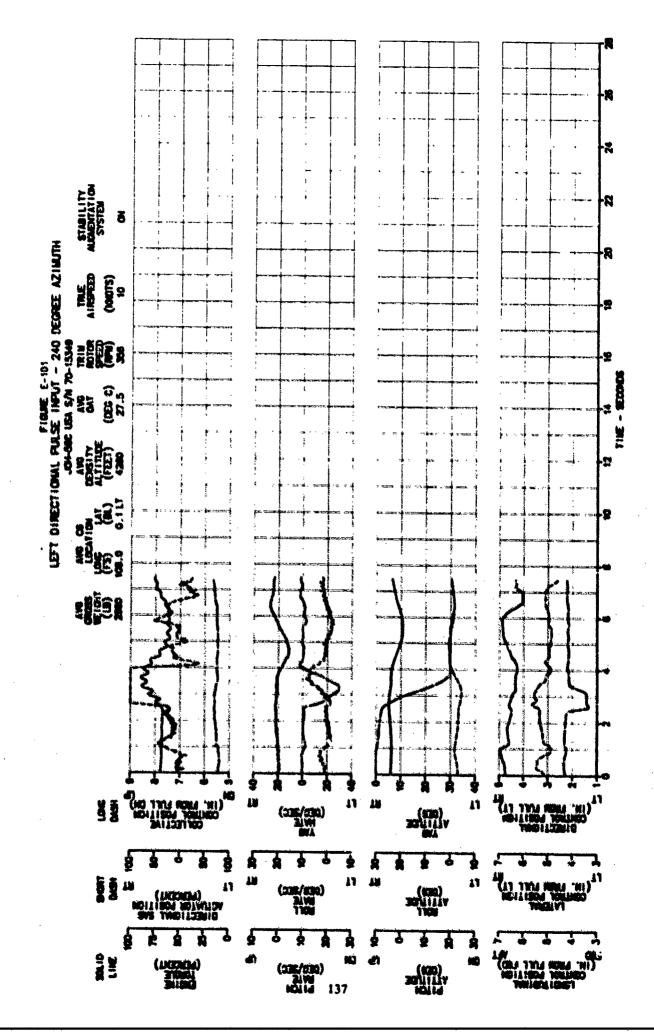


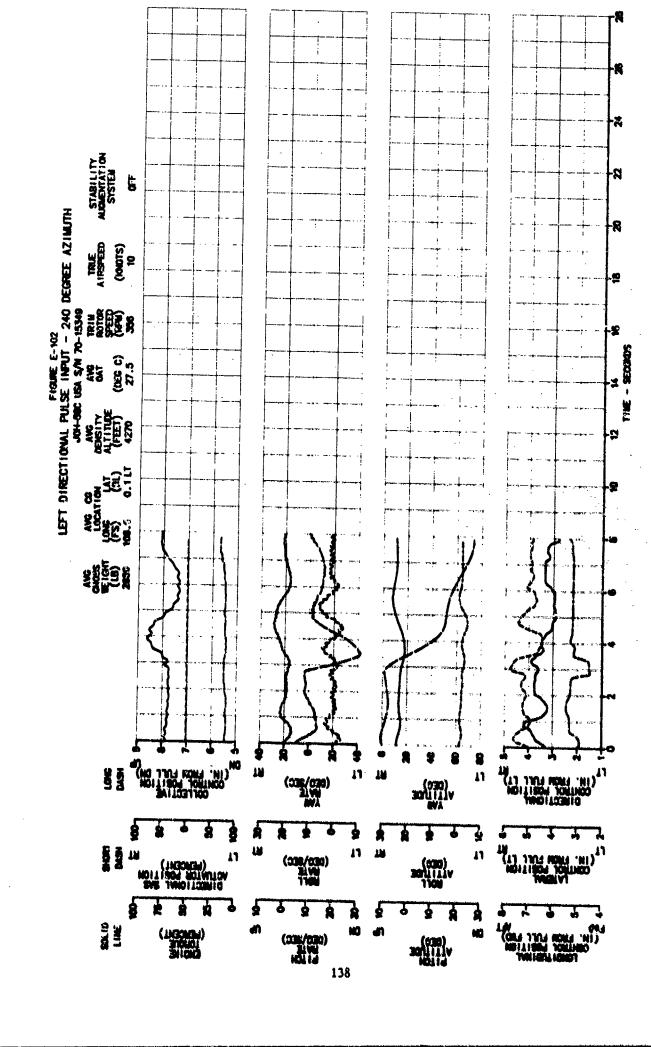


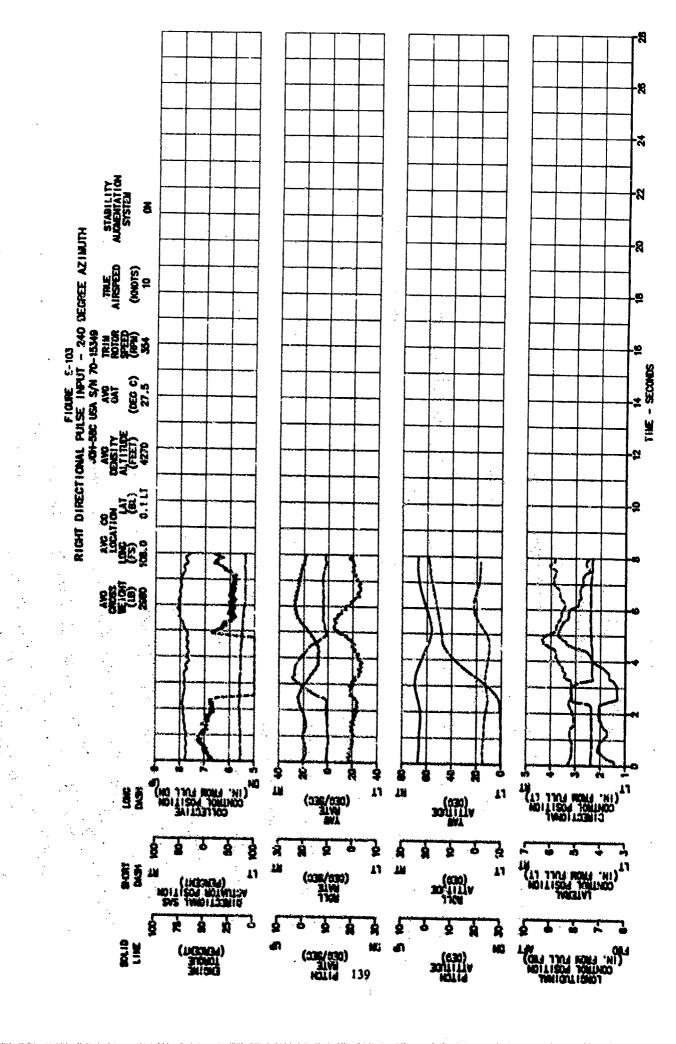


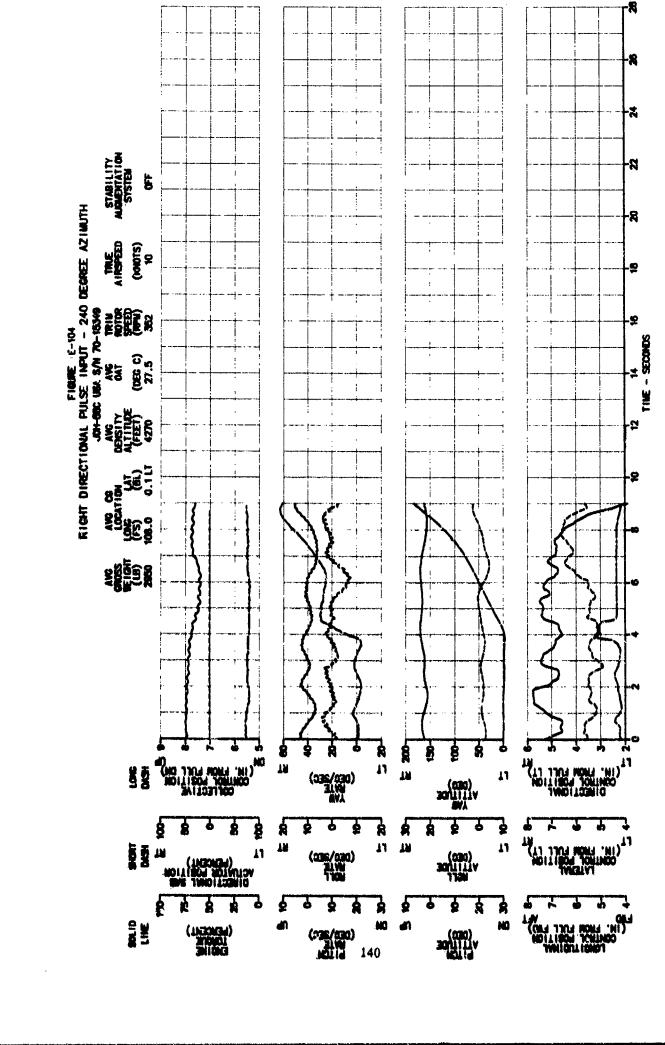


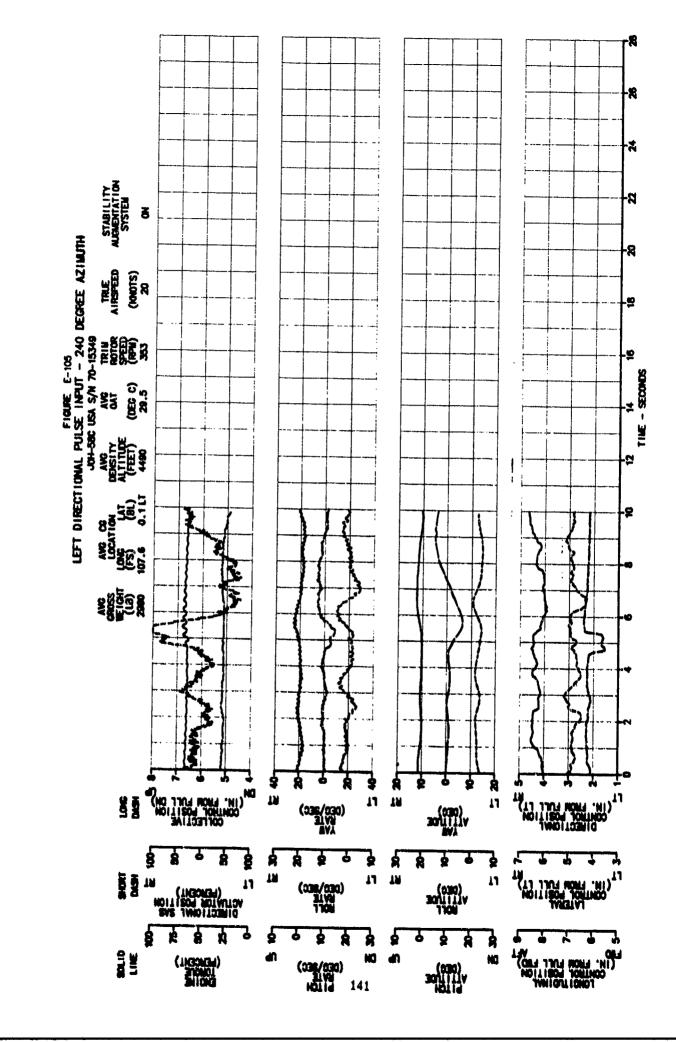


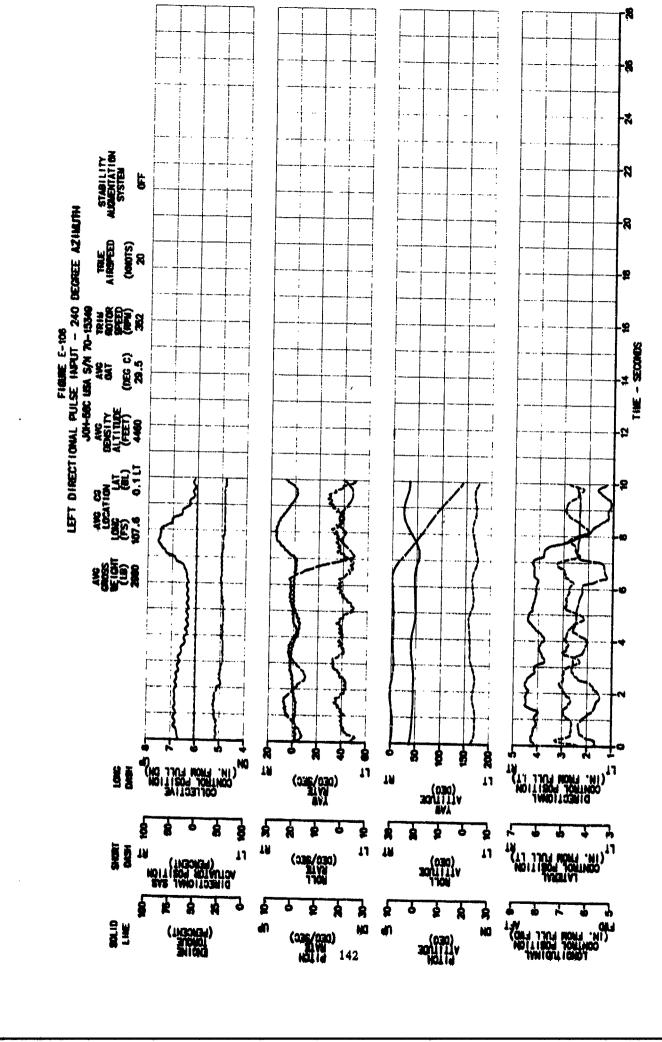


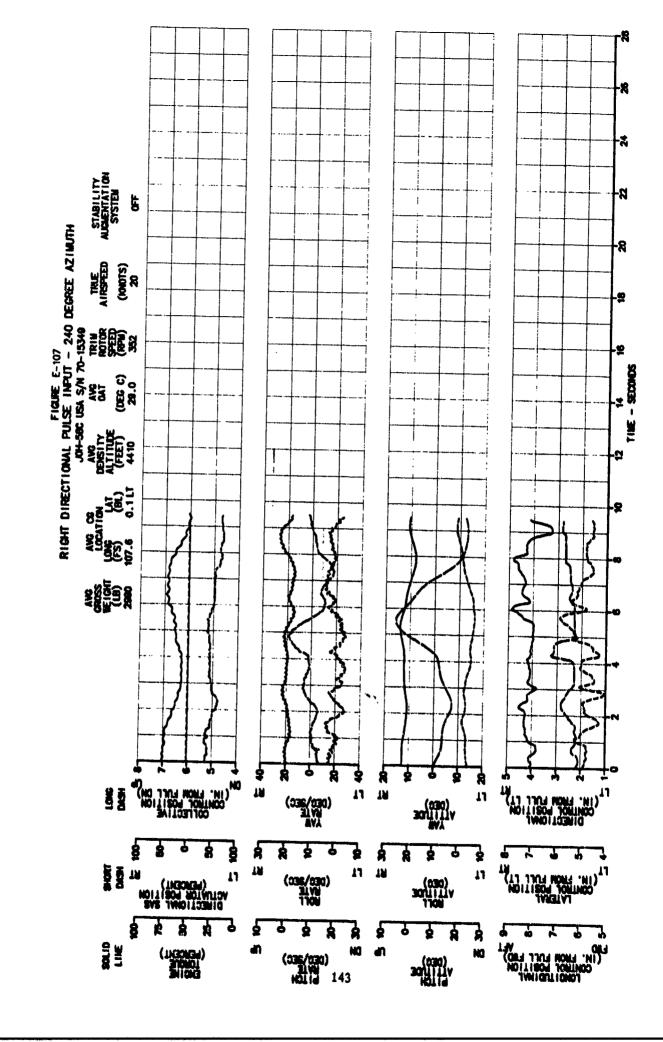


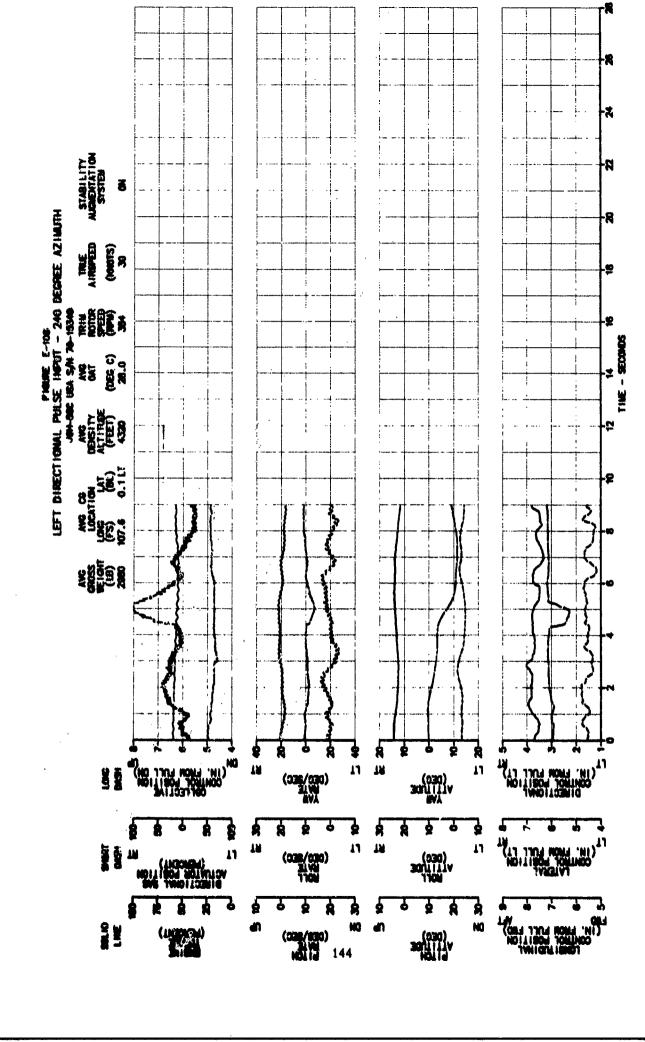


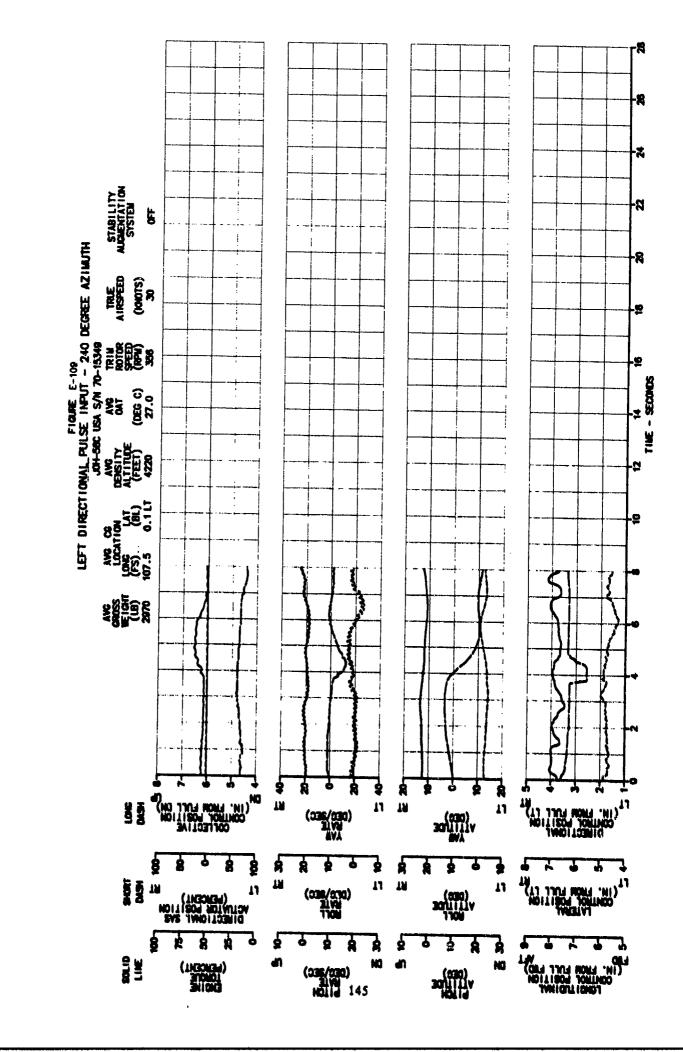


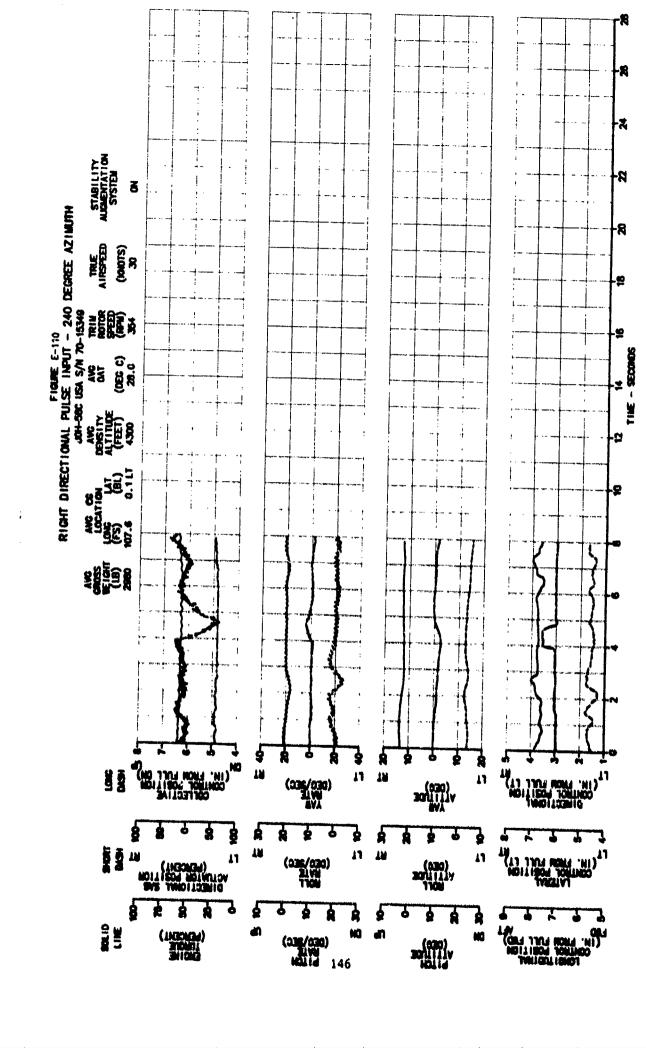


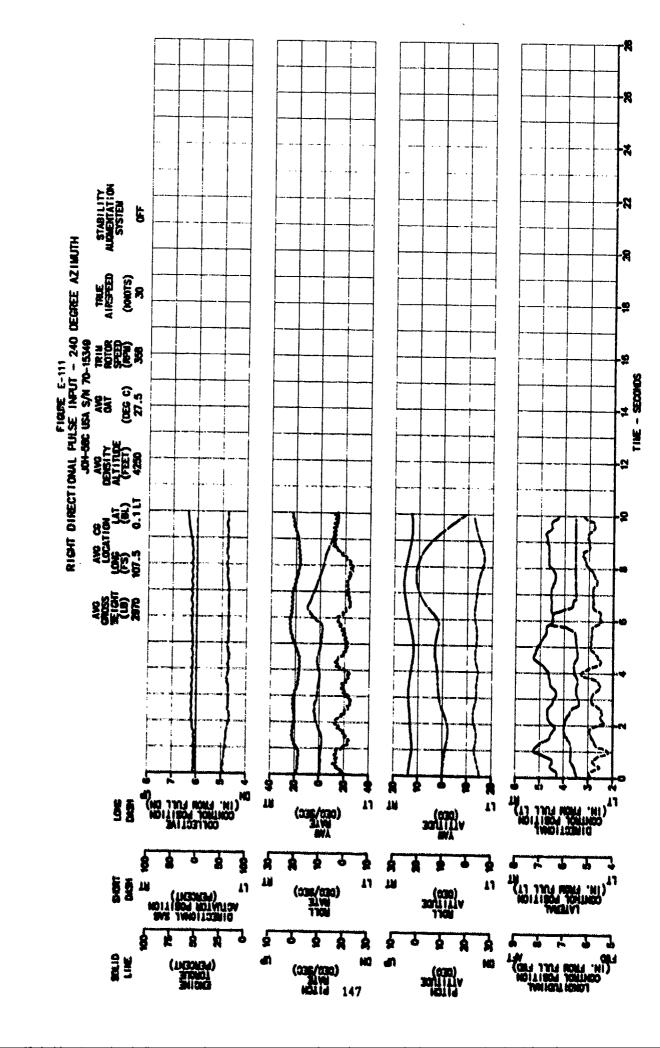


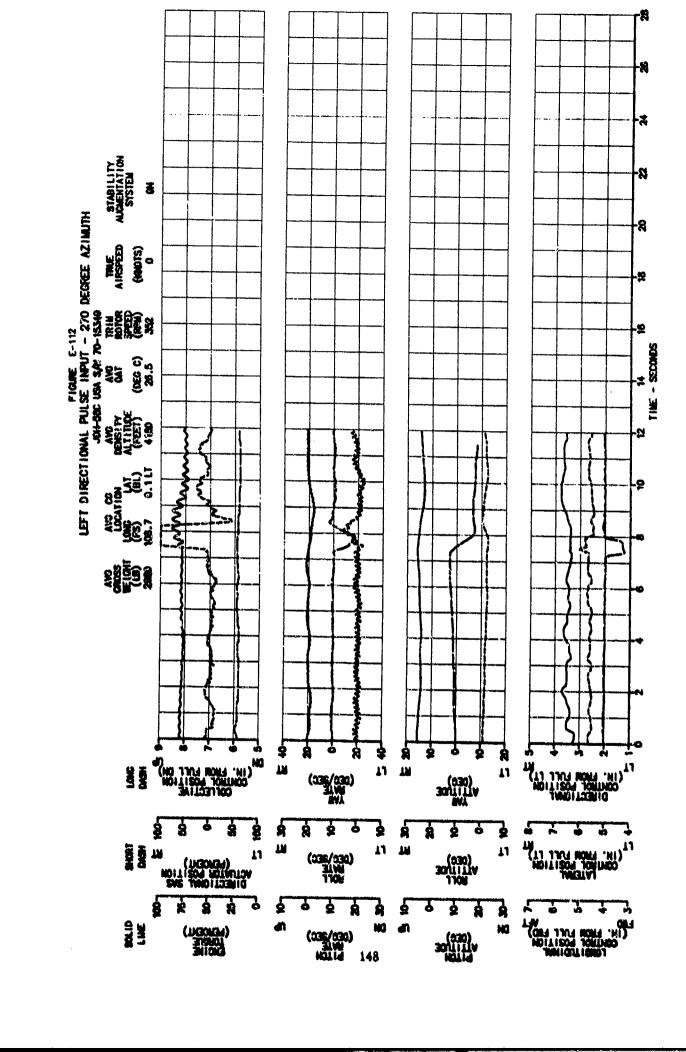


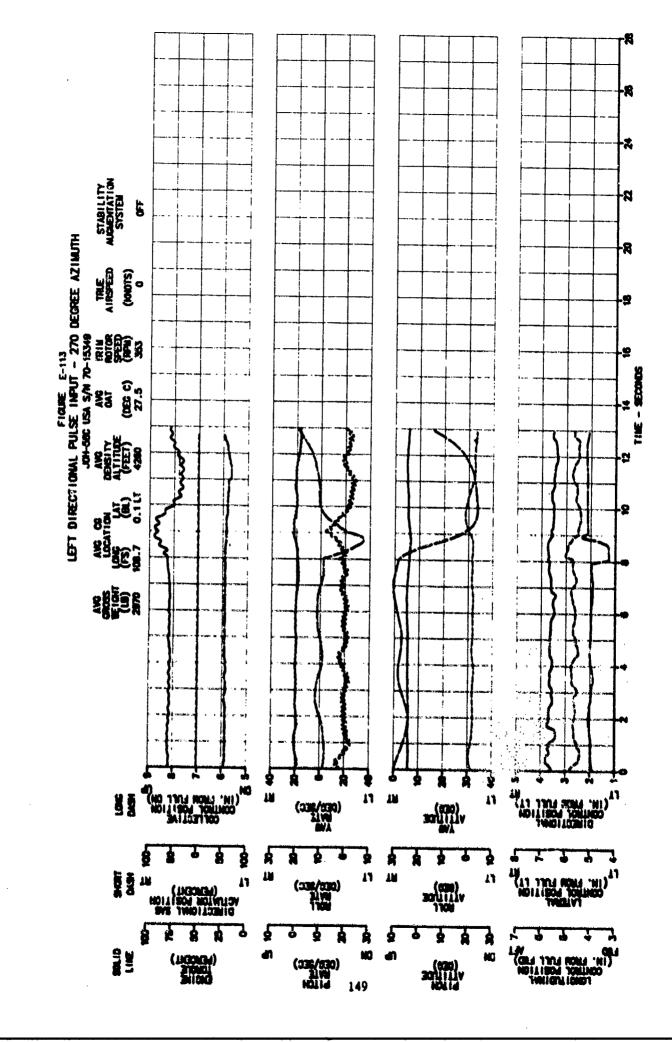


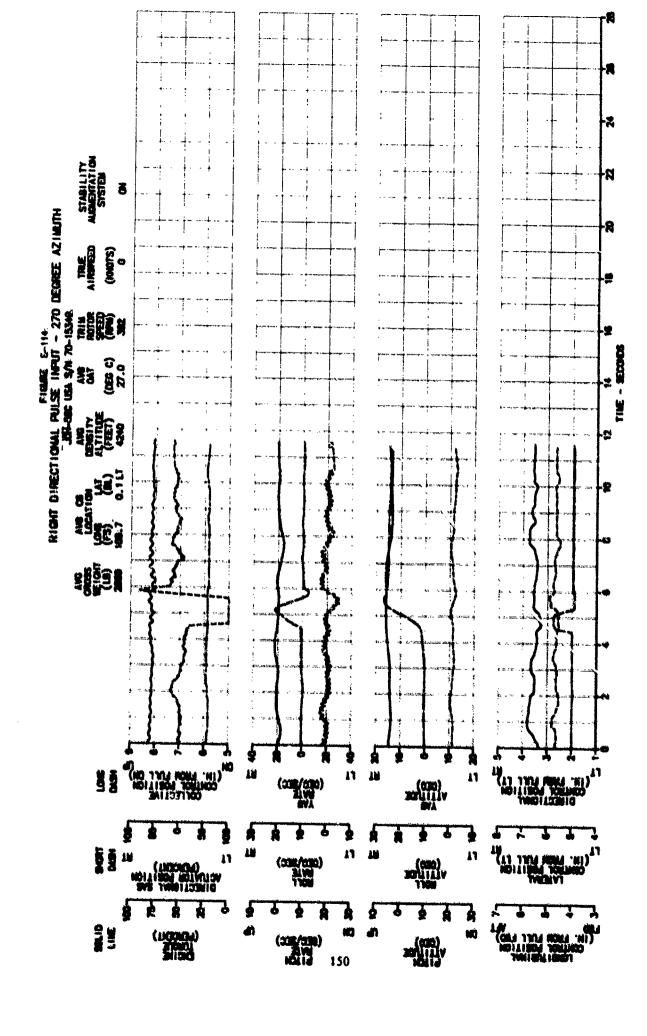


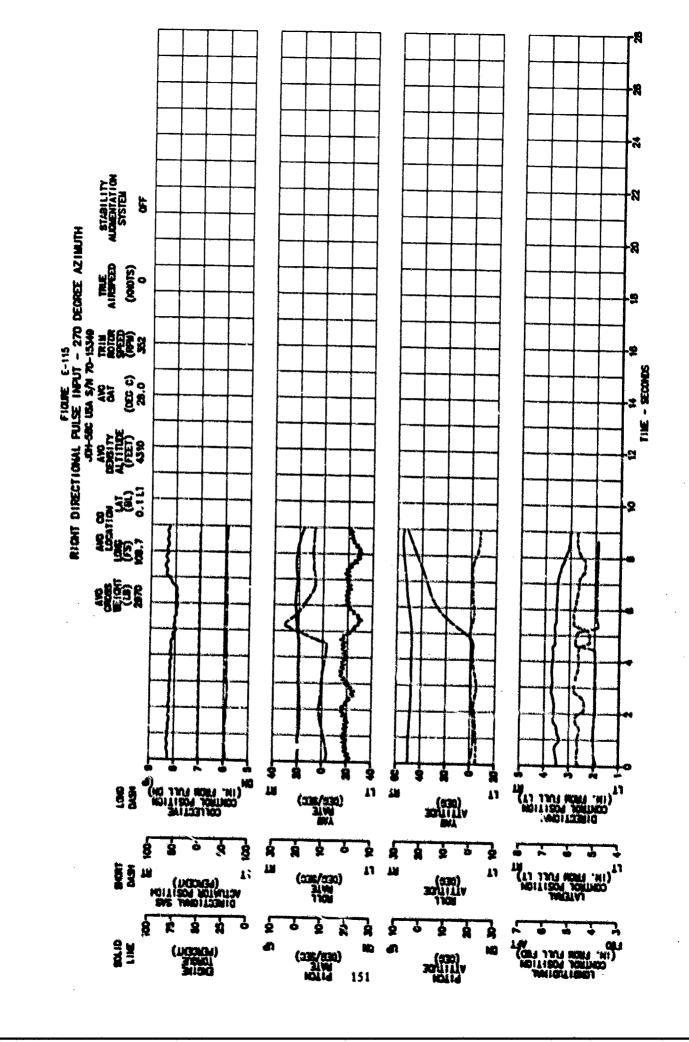


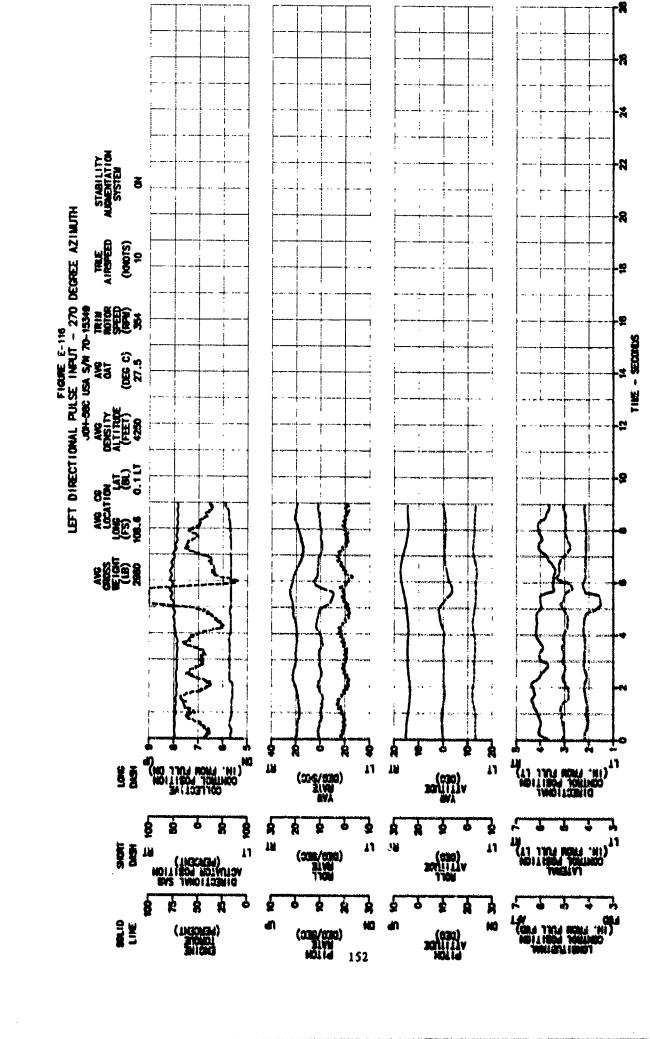


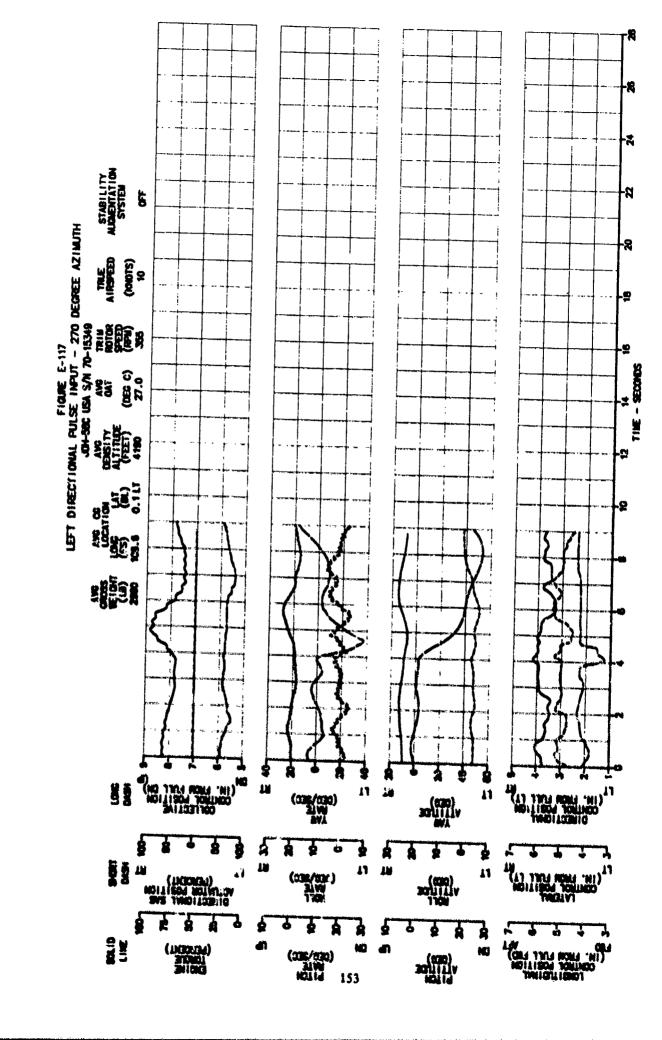


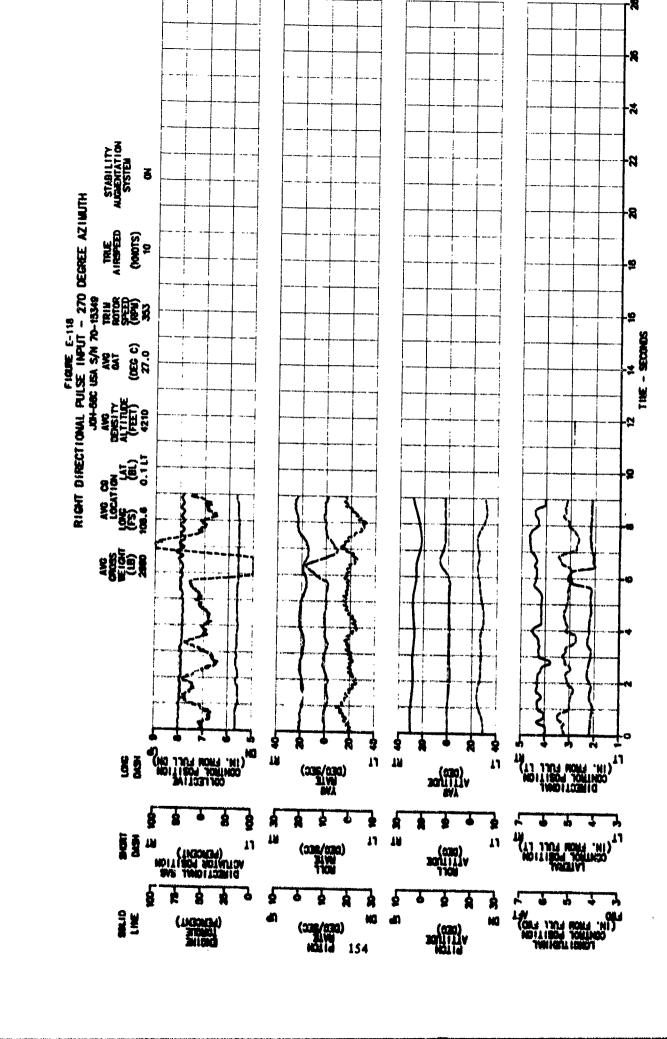


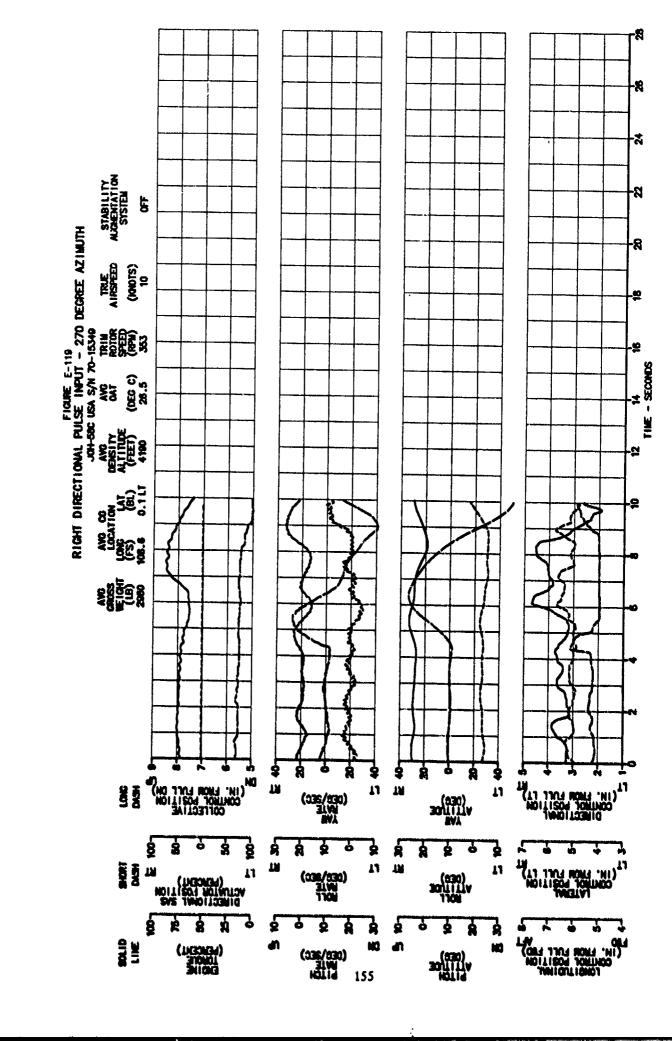


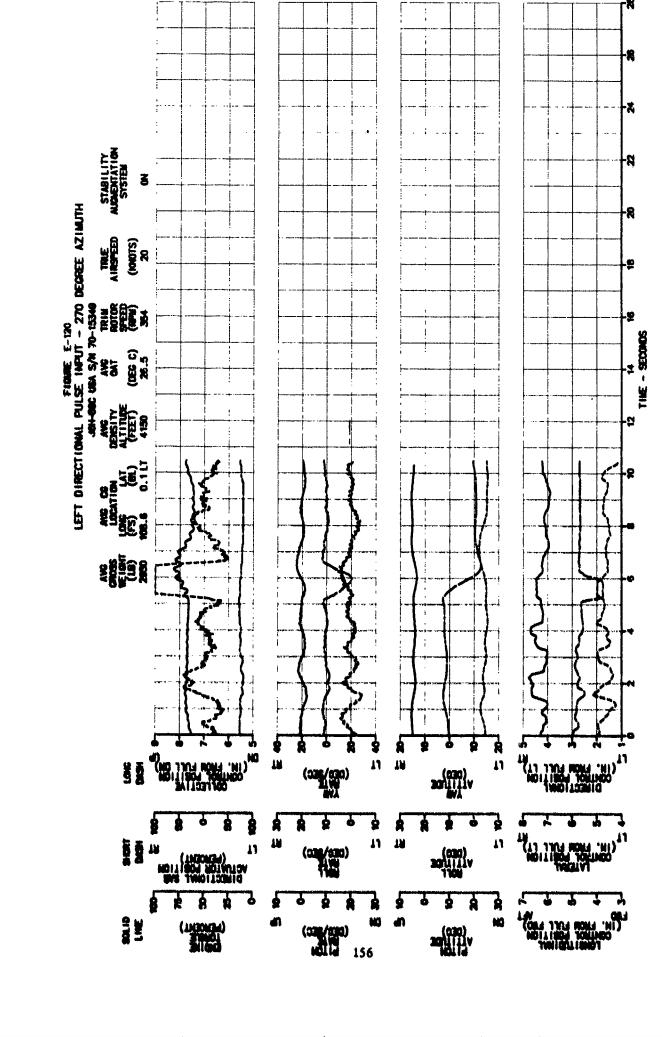


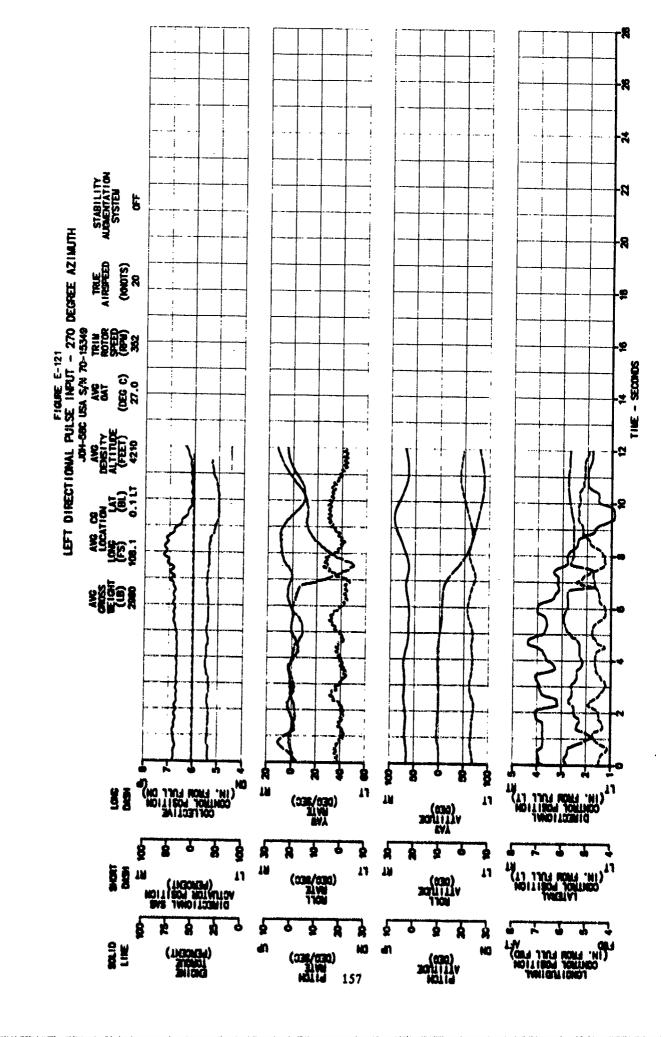


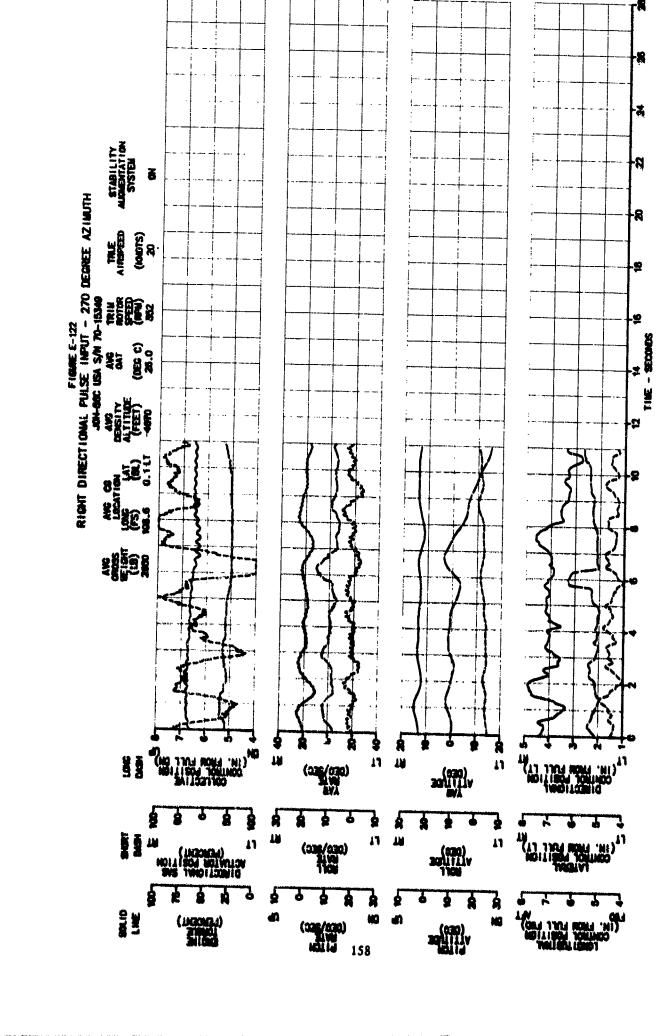


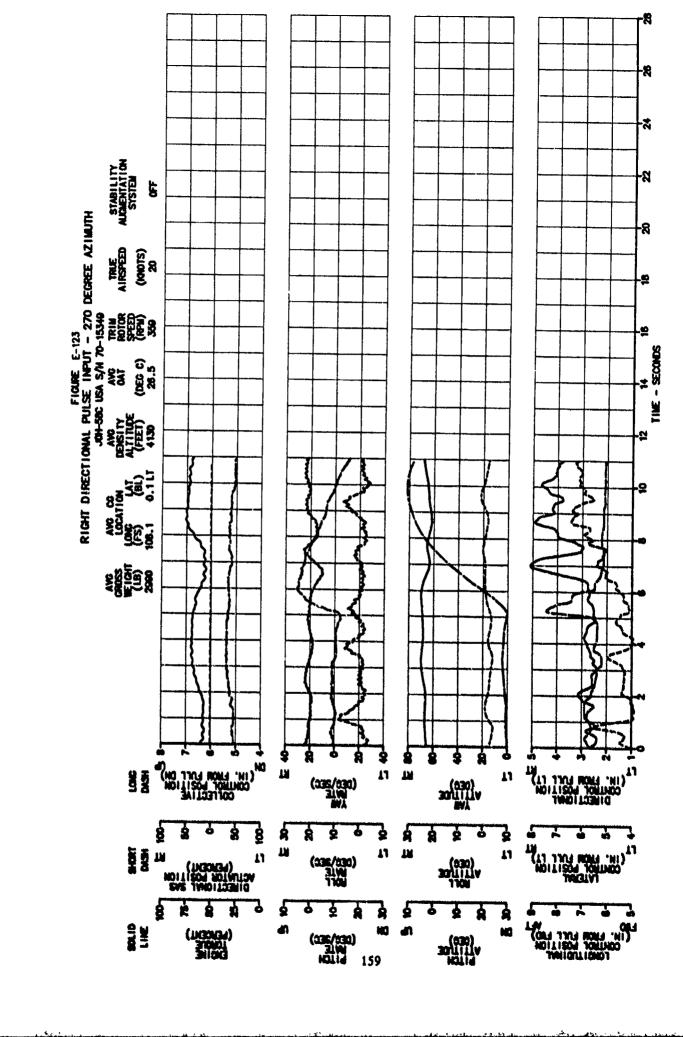


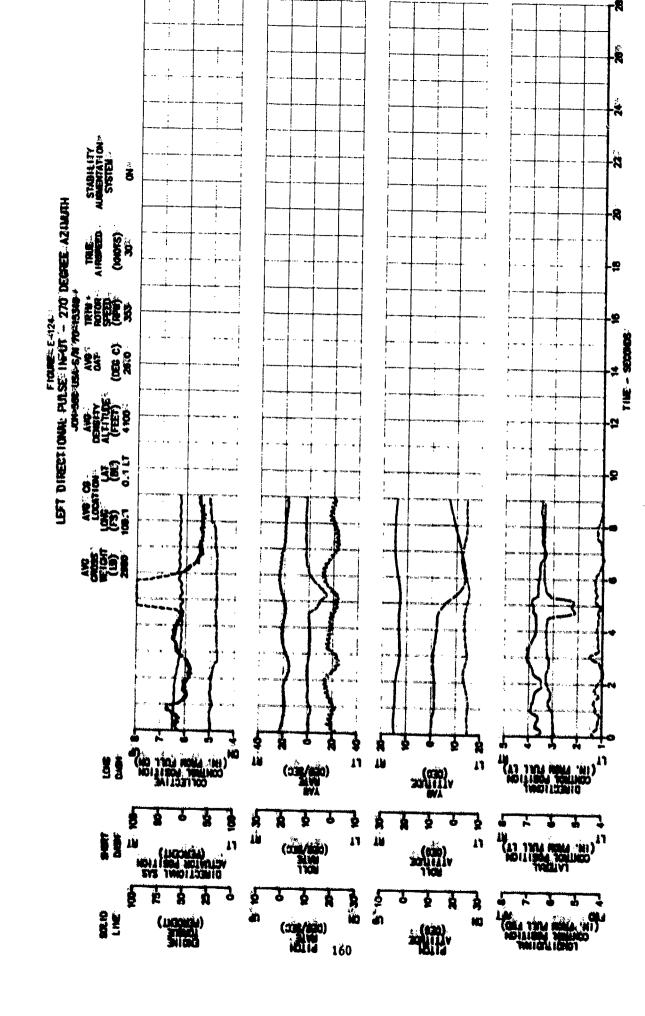


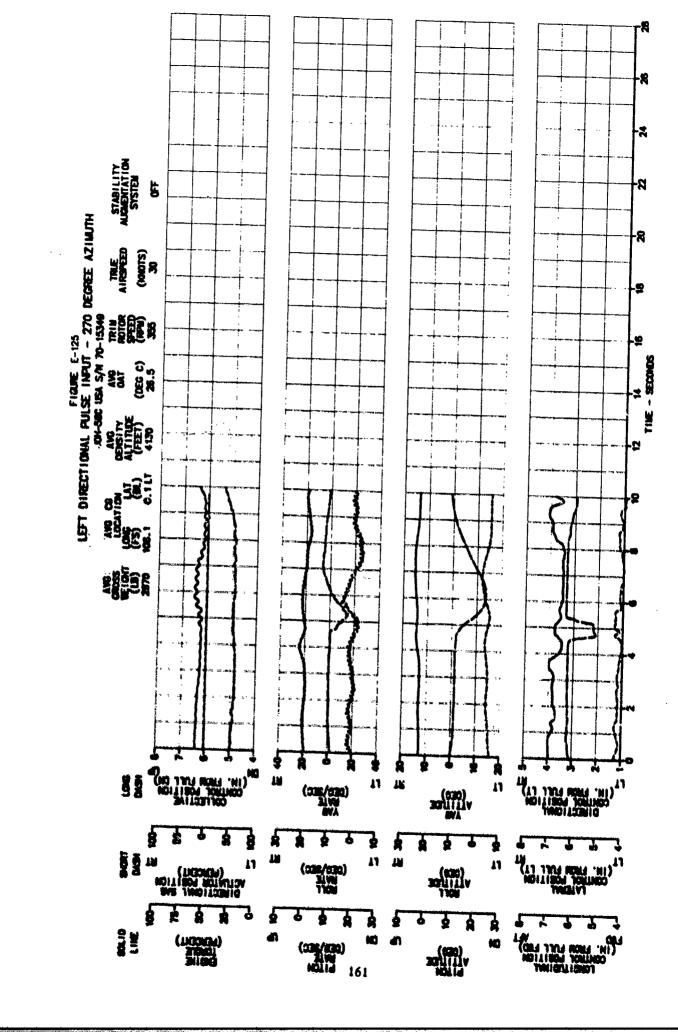


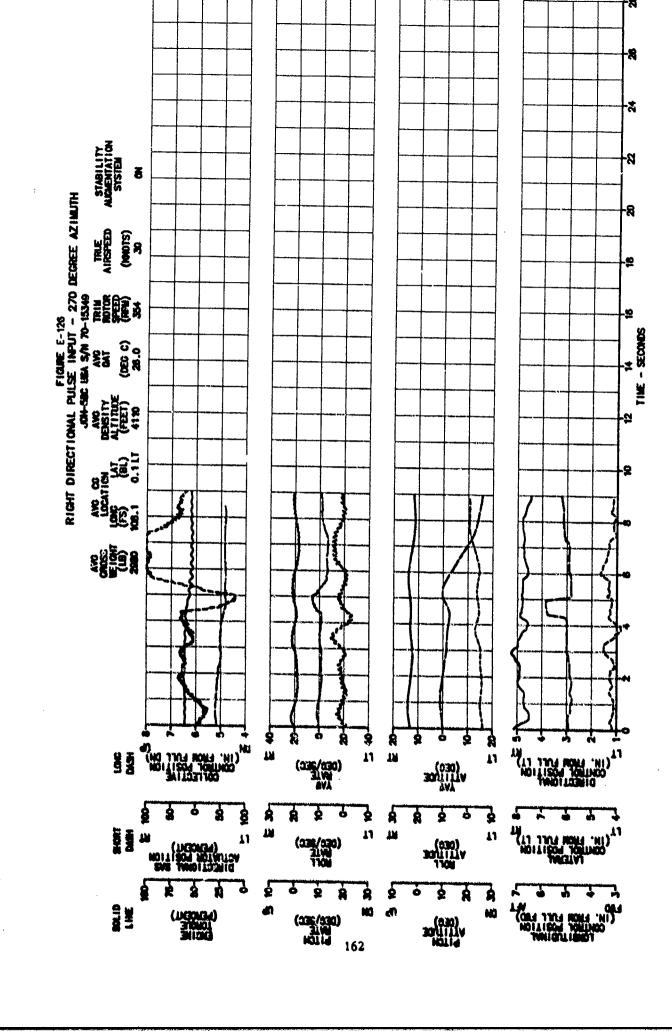


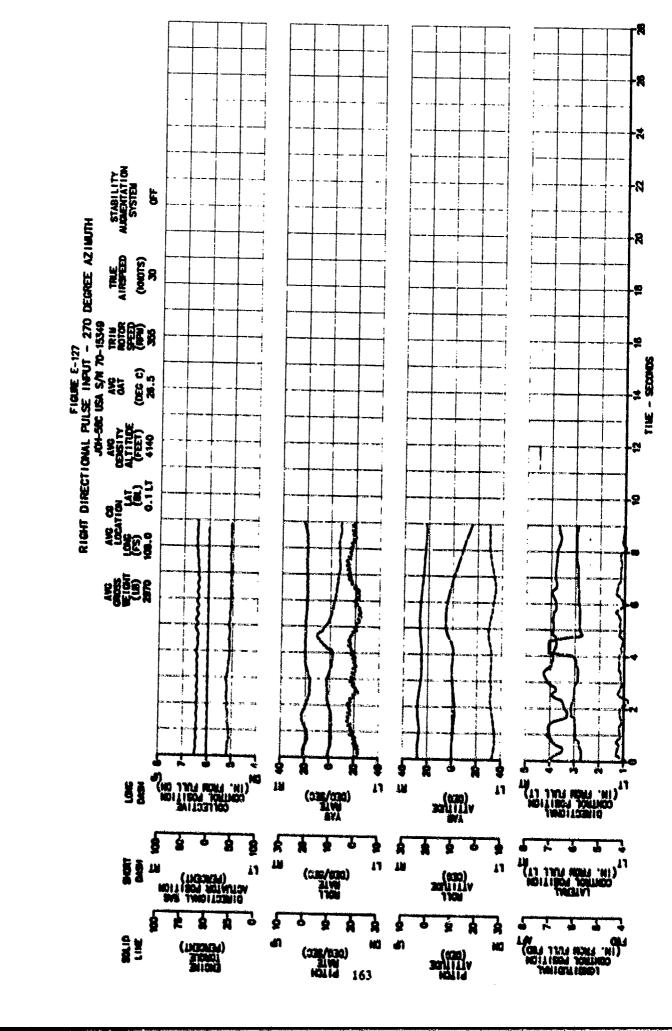


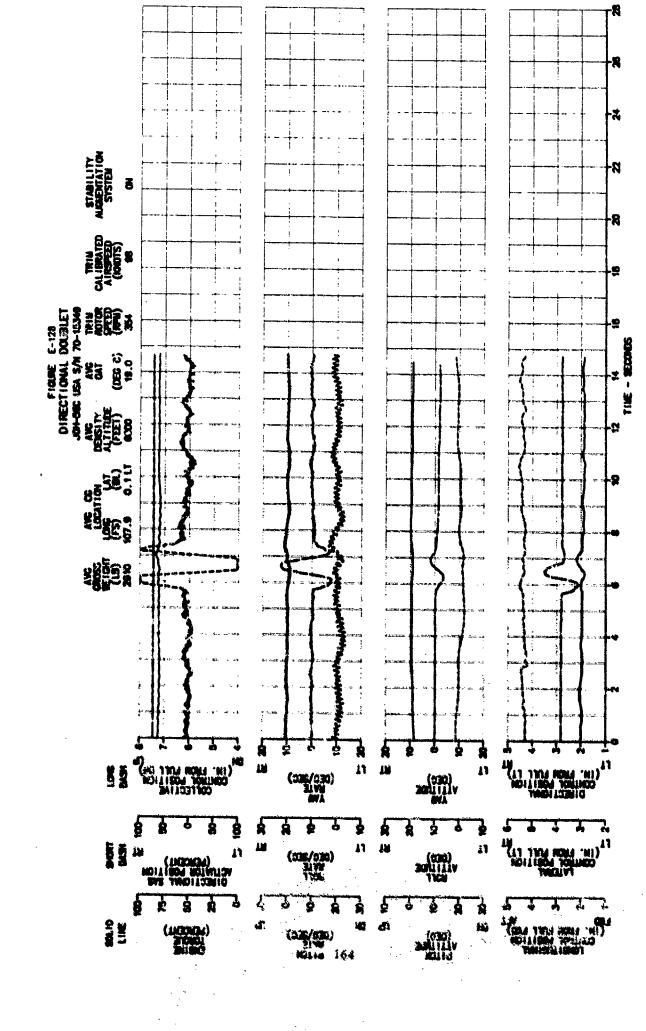


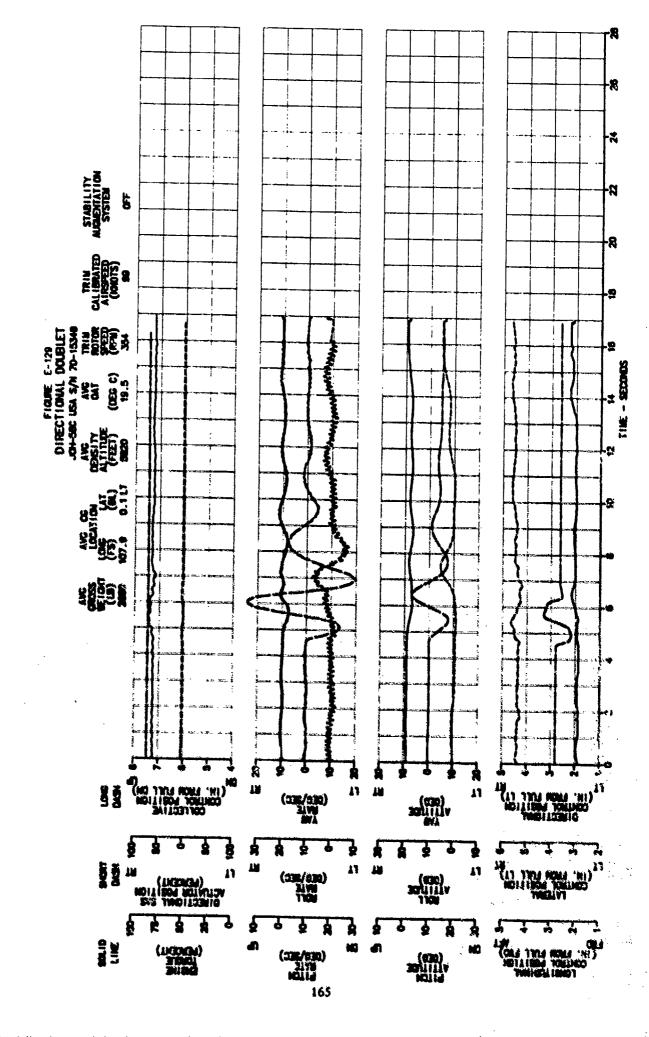


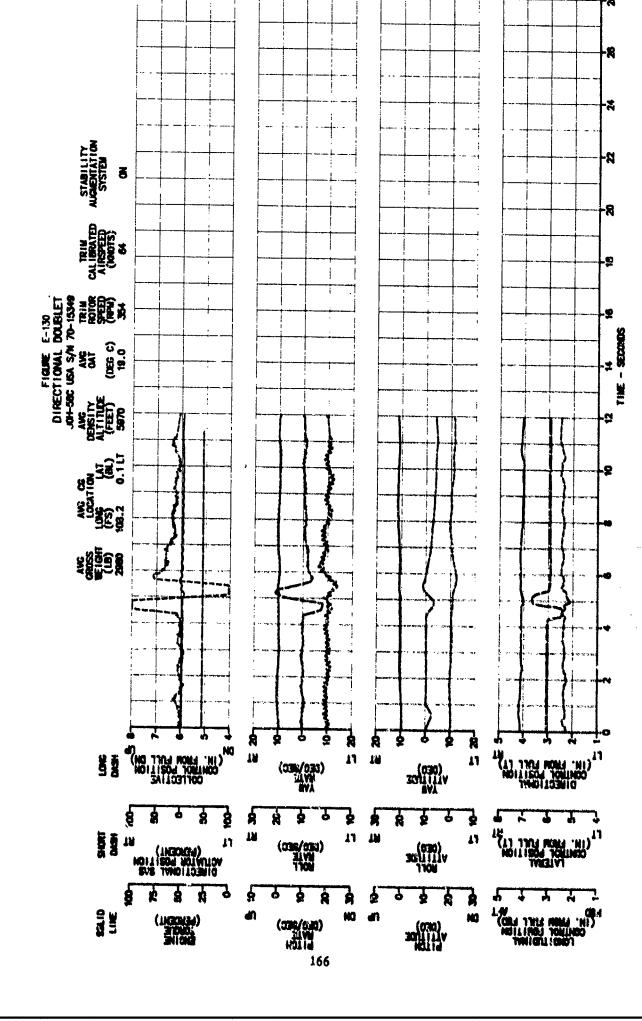


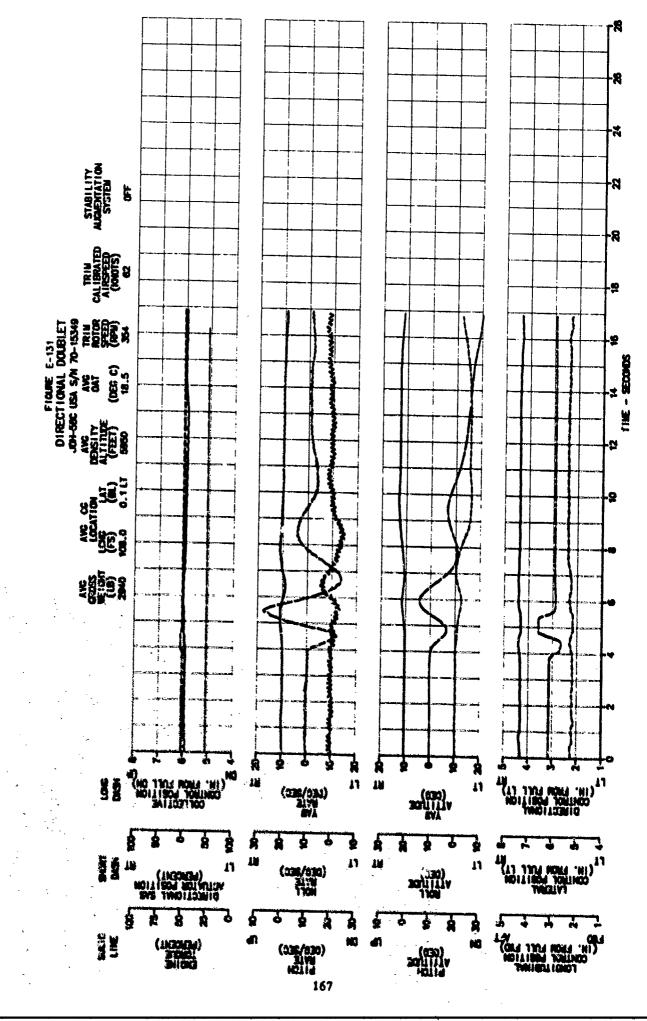


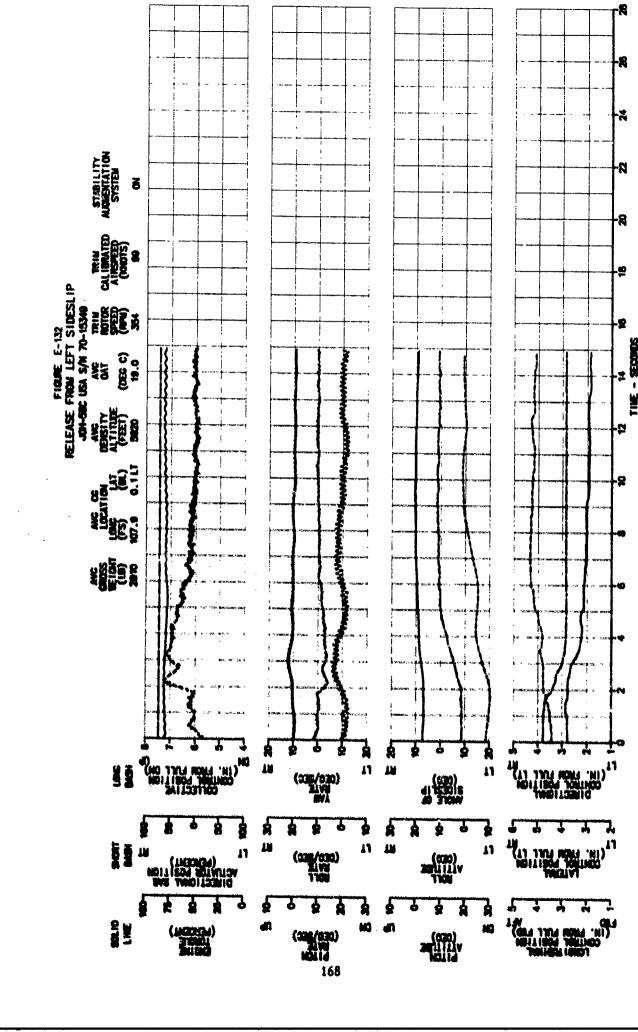


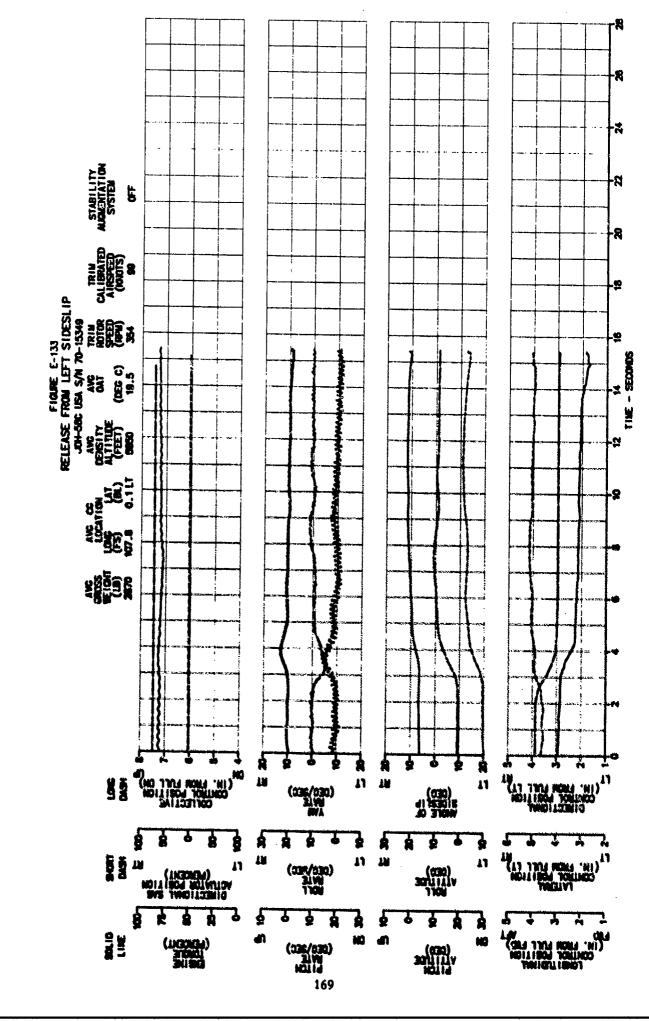


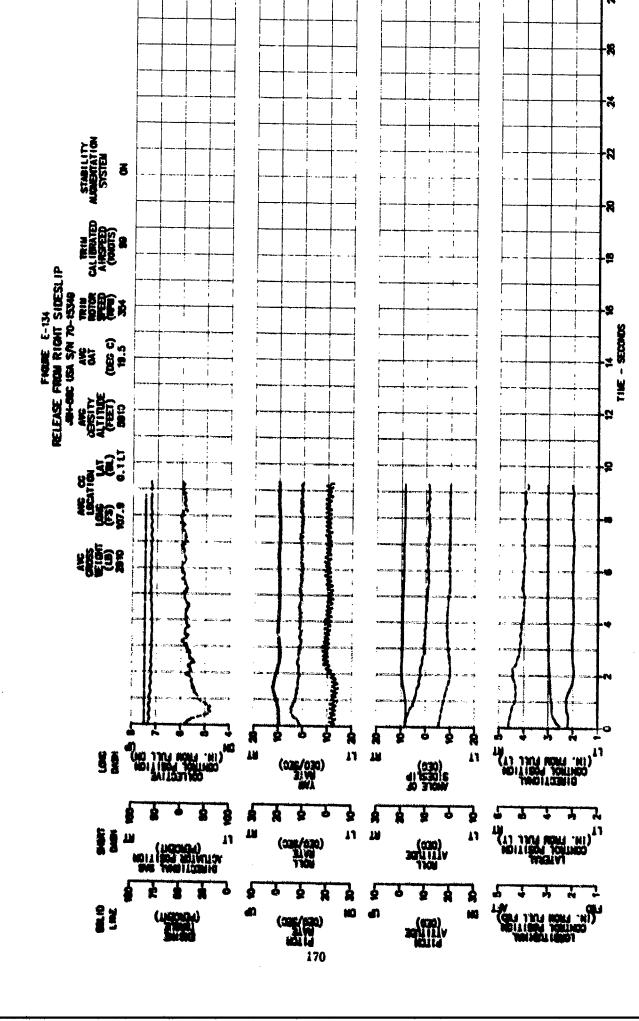


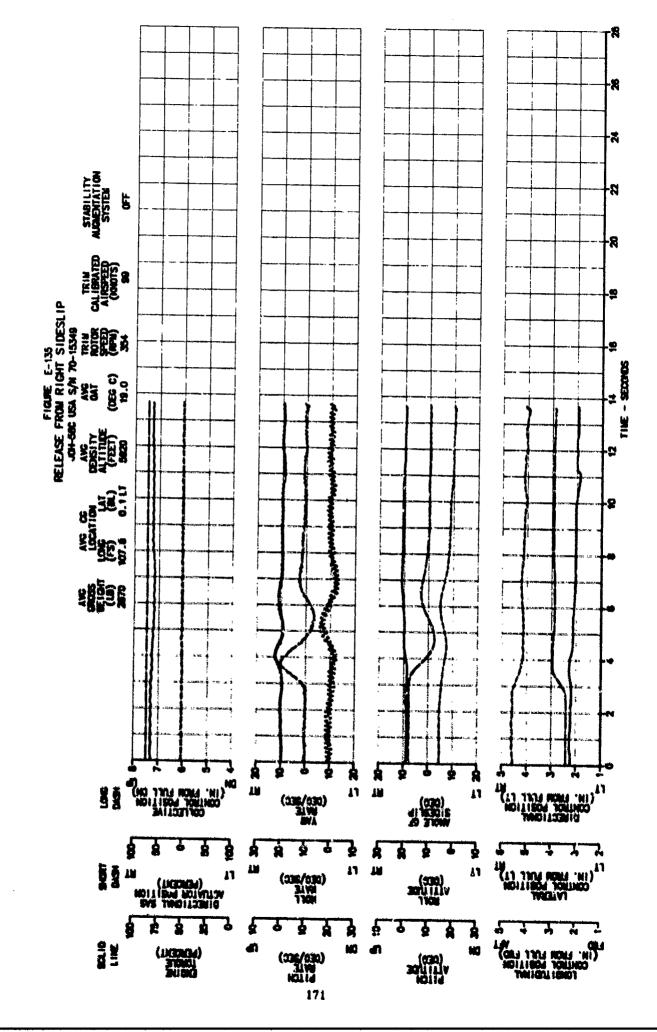


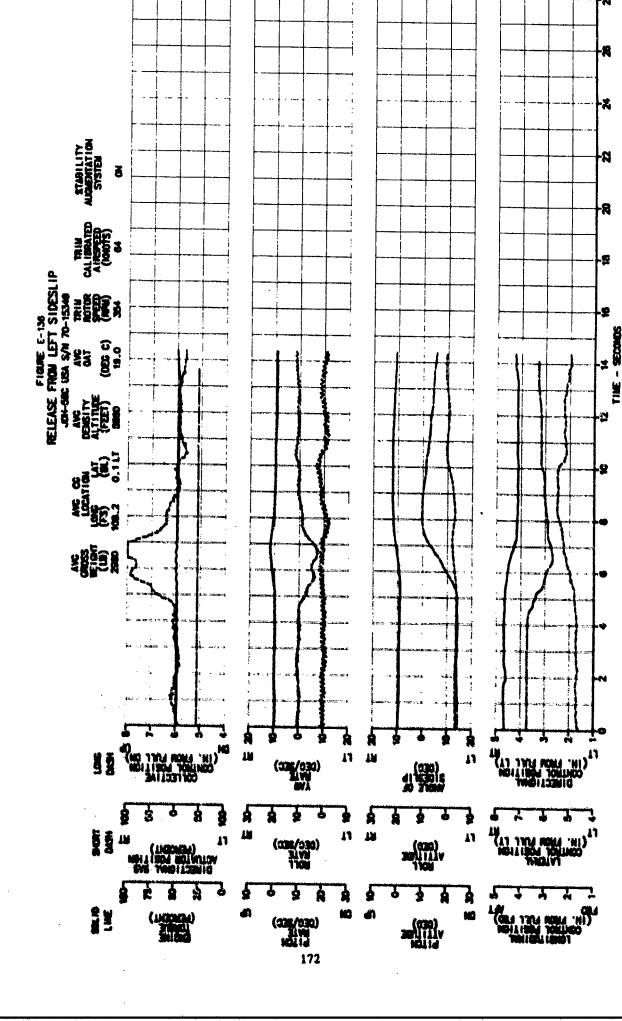


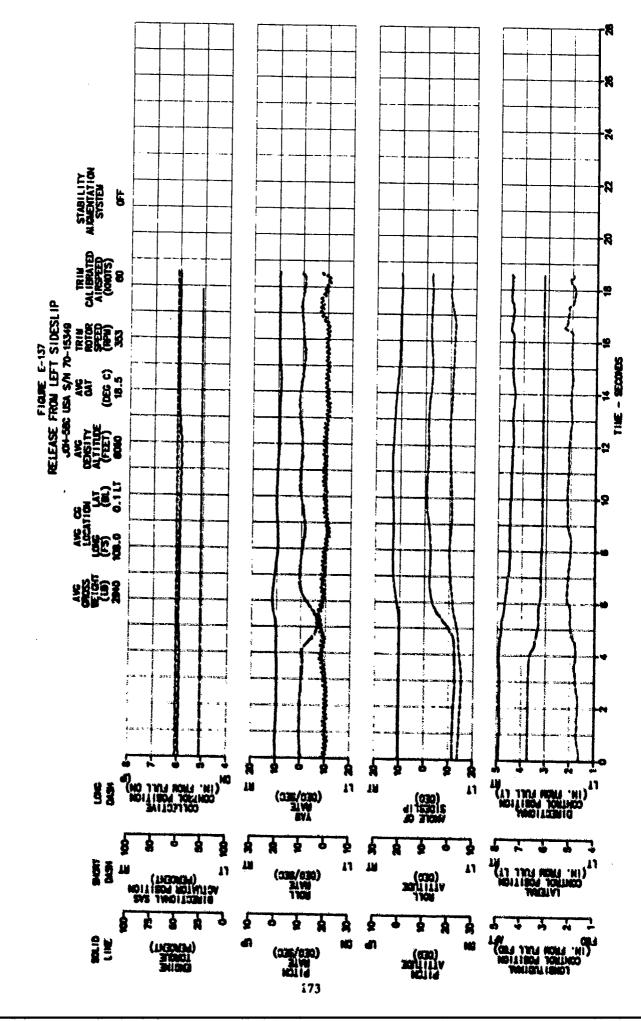


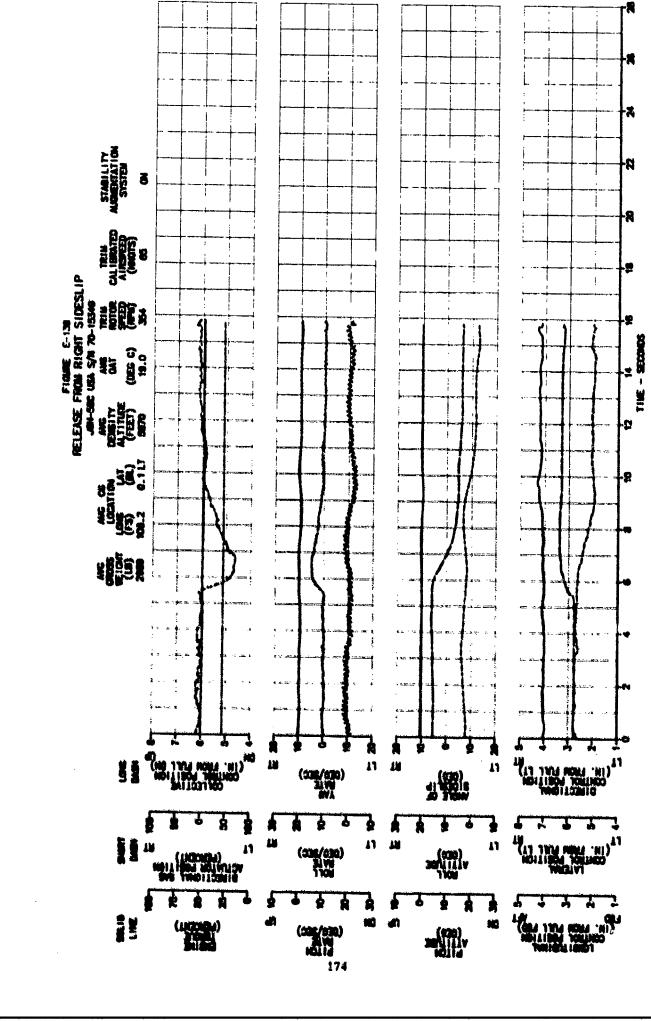


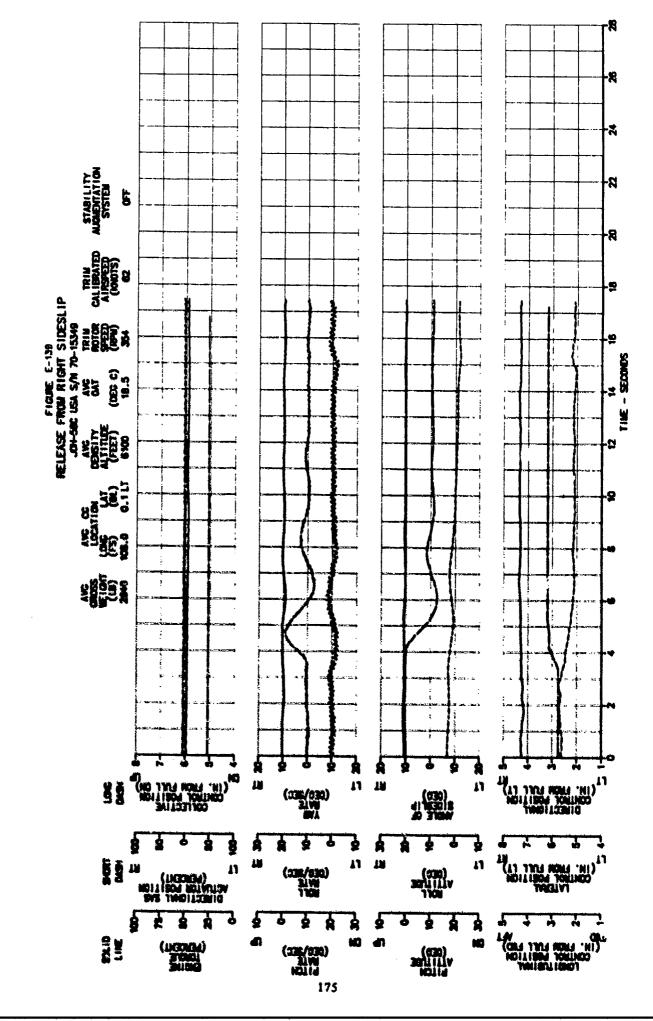


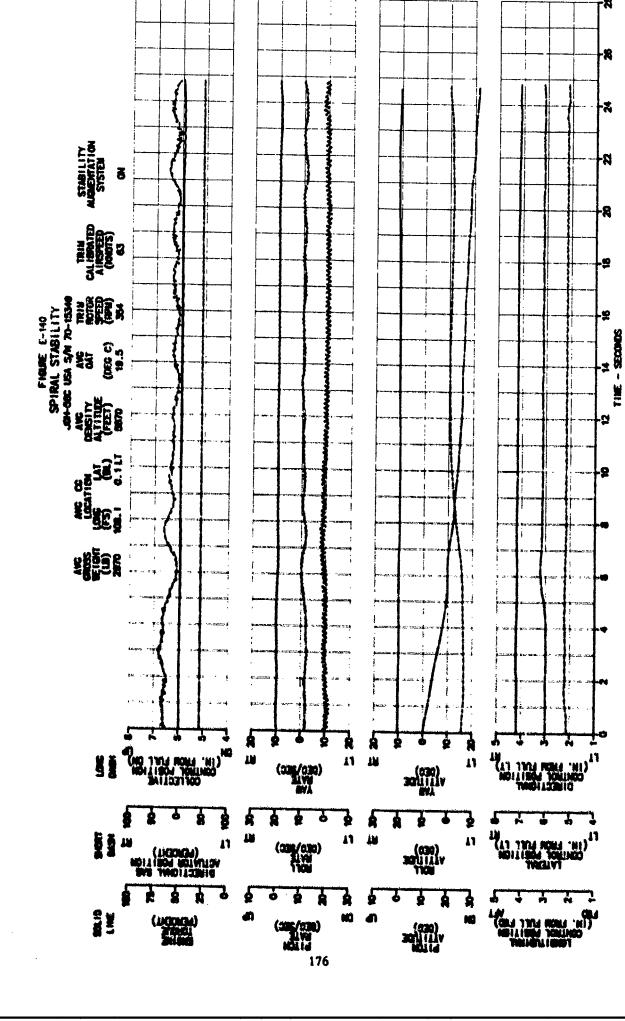


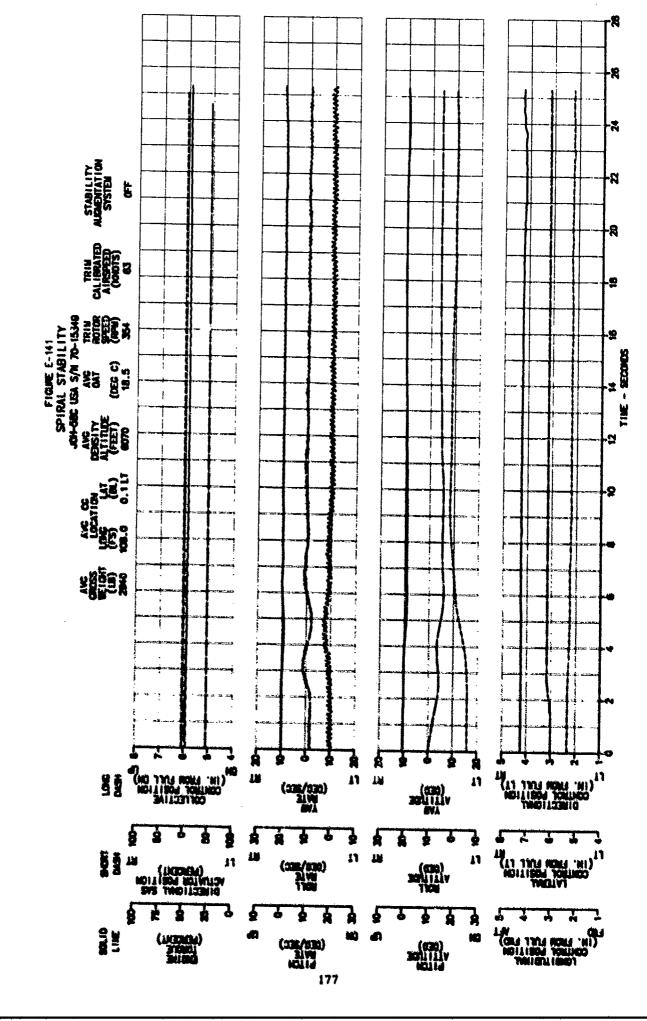


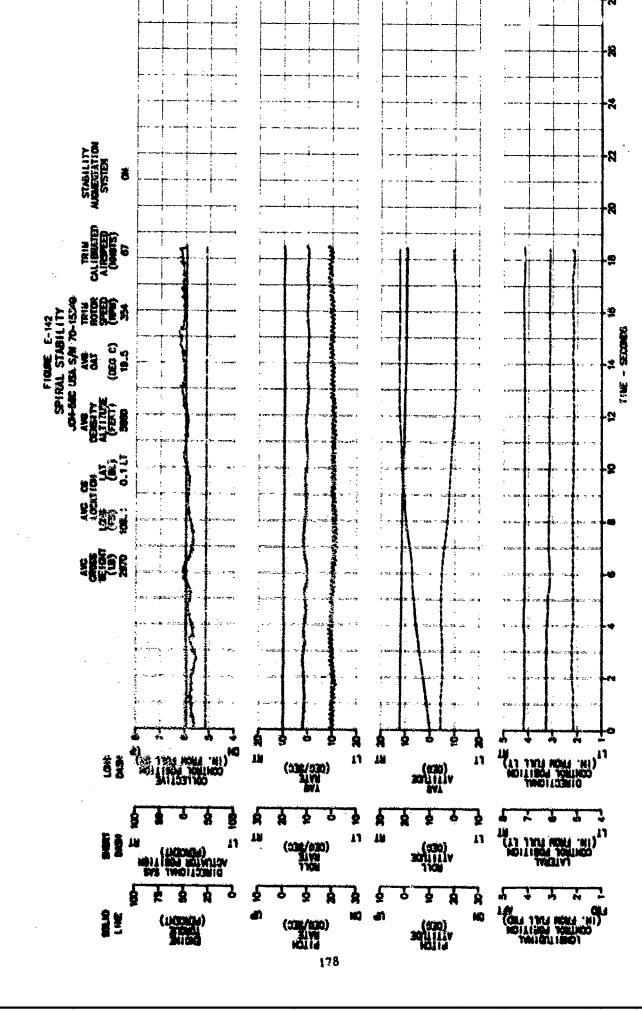


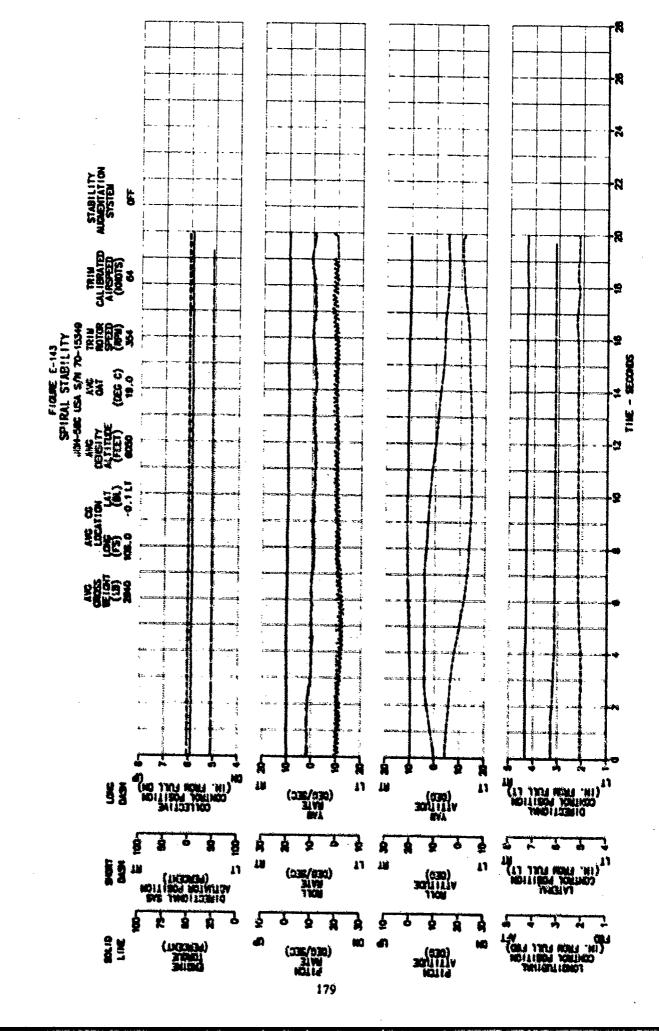


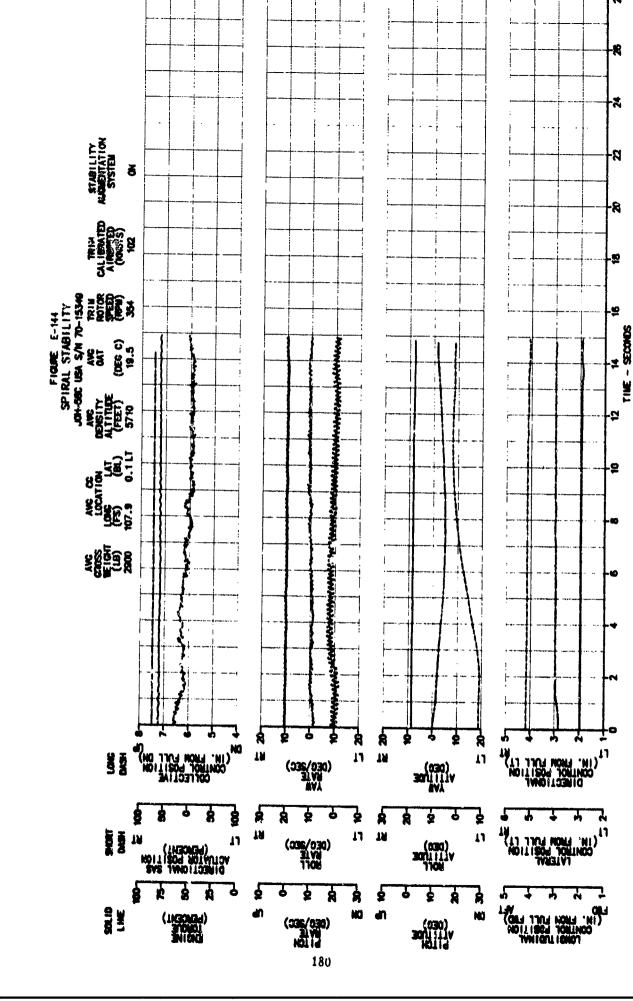


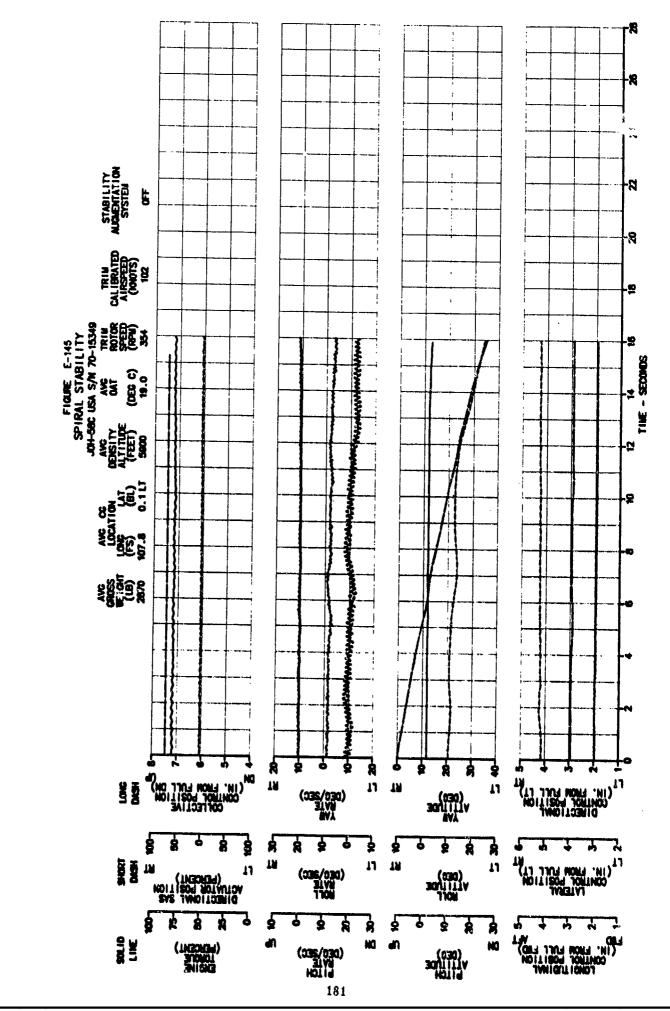


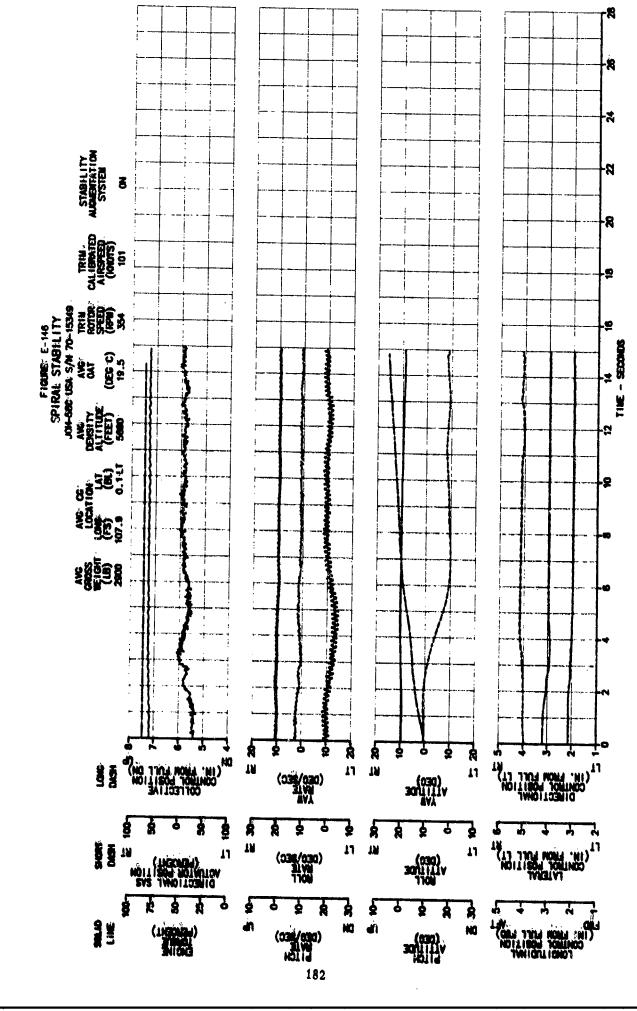


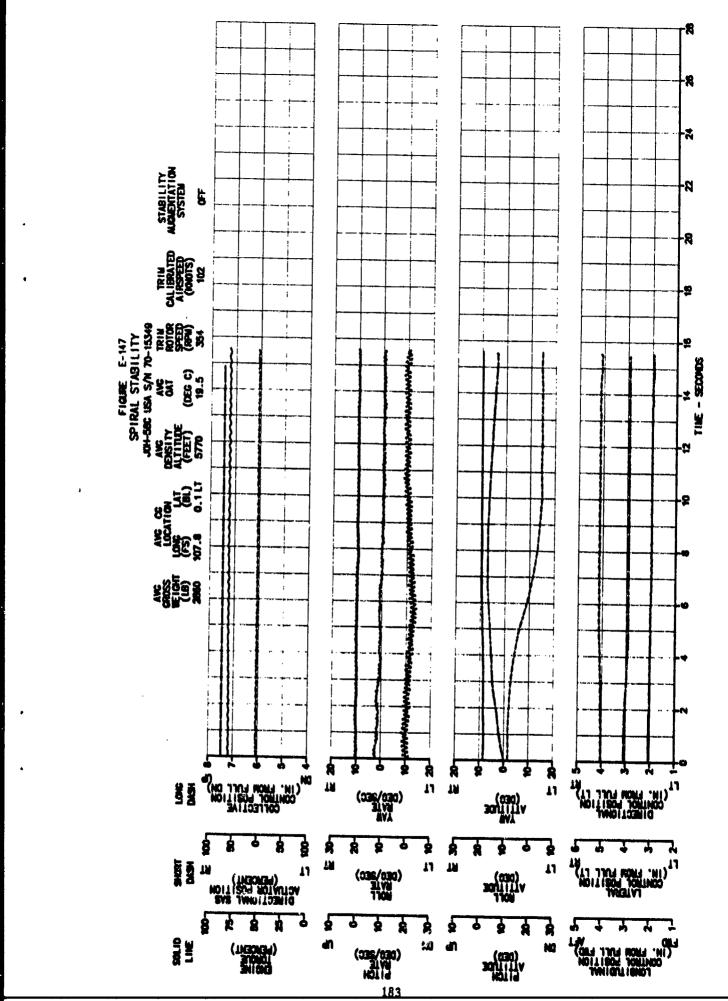


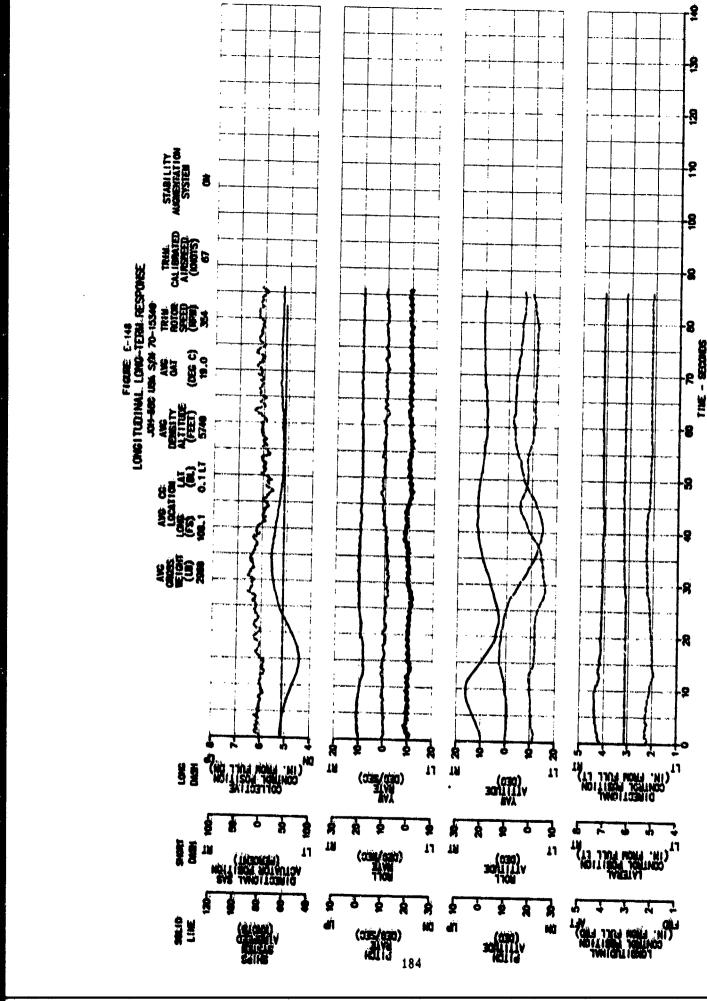


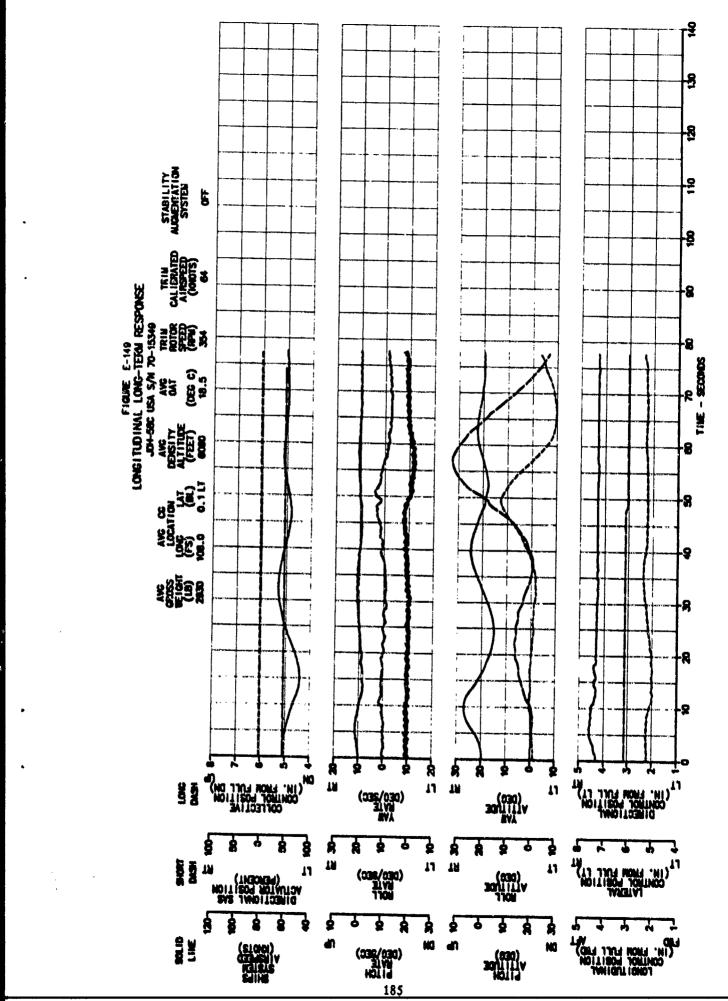


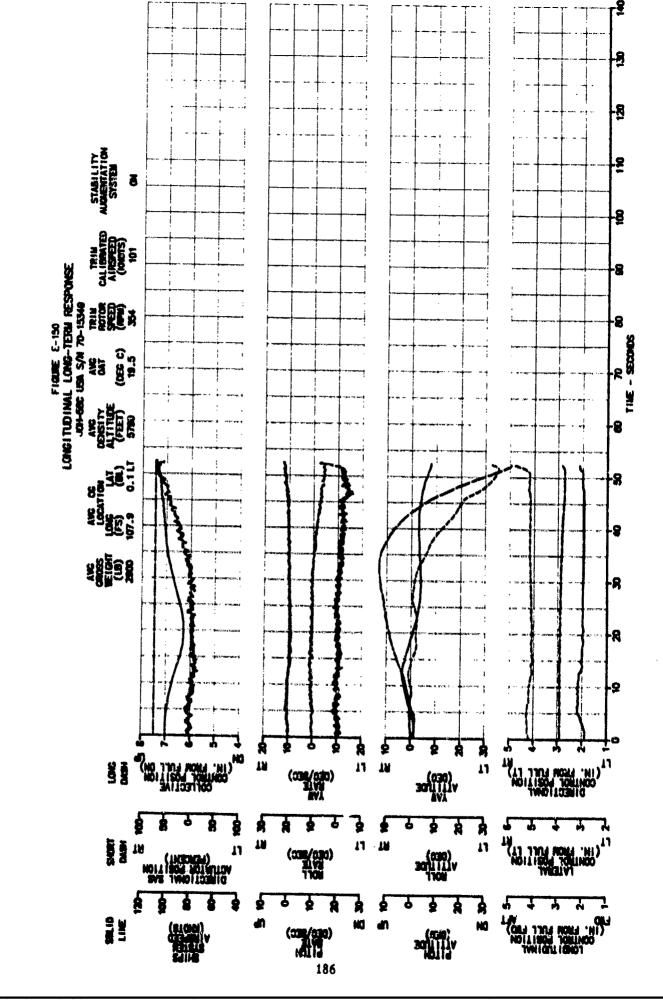












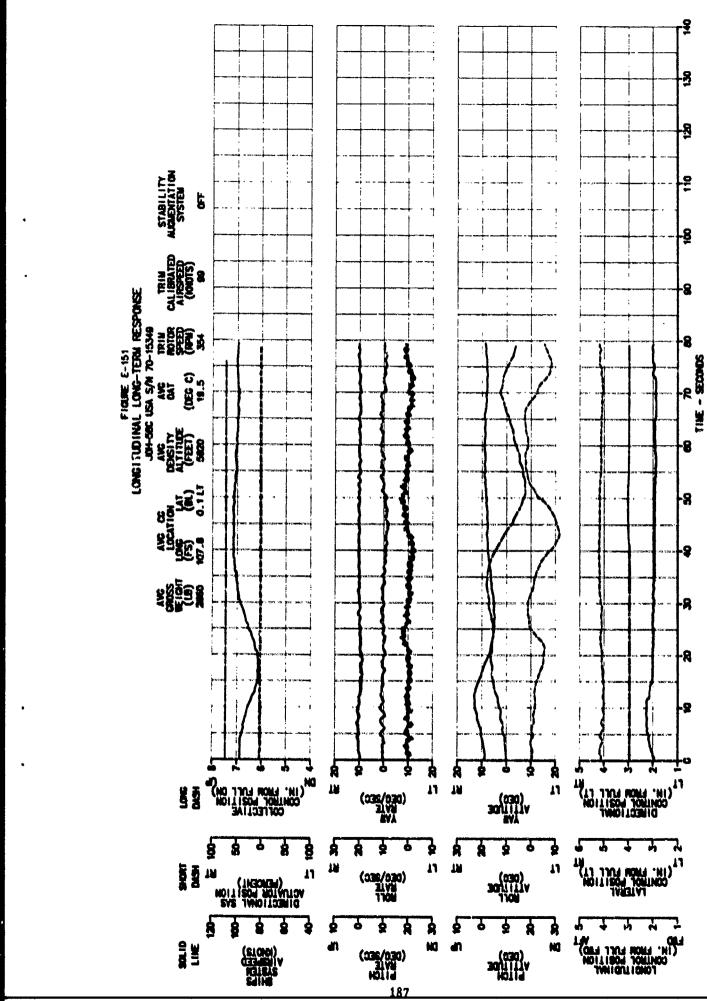


FIGURE E-152
DIRECTIONAL CONTROLLABILITY - HOVER
JOH-58C USA S/N 70-15349

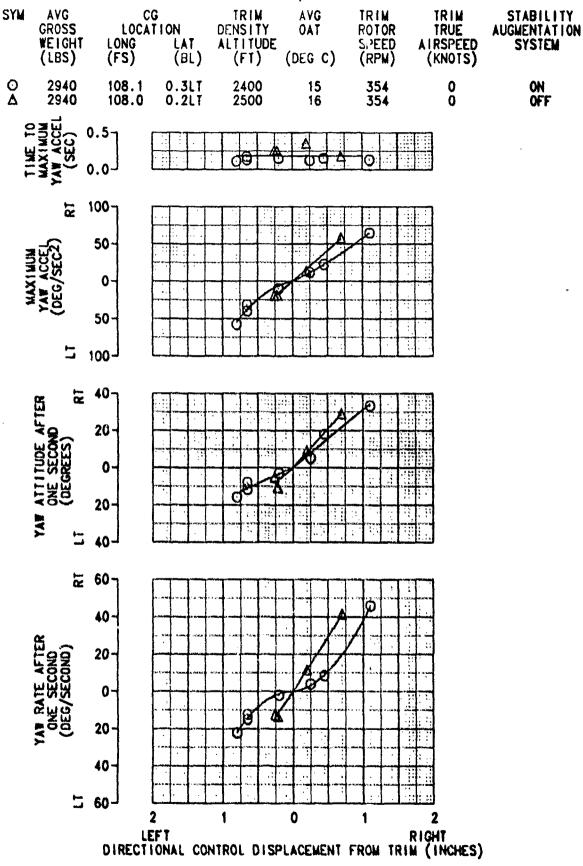


FIGURE E-153
DIRECTIONAL CONTROLLABILITY - 090 DEGREE AZIMUTH
JOH-58C USA S/N 70-15349

STABILITY AUGMENTATION SYSTEM

> ON OFF

				JOH-58C US	A S/N 70-	15349	WEL ALIMU
SYM	AVG GROSS WEIGHT (LBS)	LOC	CG CATION LAT (BL)	TRIM DENSITY ALTITUDE (FT)	AVG OAT (DEG C)	TRIM ROTOR SPEED (RPM)	TRIM TRUE AIRSPEED (KNOTS)
⊙ ∆	2890 2880	108.5 108.4	0.0	3300 3350	19.0 19.5	354 354	10 10
7.1%F 70	MAXIMUM YAW ACCEL (SEC)	0.5		ď	A C		
	R	1007					
35	(Z)	50-					
MAXINGN	YAW AC (DEG/SE	0-		Q.	B		
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	11	100					
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71 847	355 1	20-					
\$	ב ב	40					
	8	607					AV 1 December 2
	_	40-					74.13 74.13 74.13 74.13 74.13
AFTER		20-					
ATE /	S SEC	0-		0	6		
YAN	OE CE	20-					
		40-					Actal Parks 61 b Actal Prings
		60			0		
				rol Displ		1 ROM TRIM	2 IGHT (INCHES)

FIGURE E-154
DIRECTIONAL CONTROLLABILITY - 090 DEGREE AZIMUTH
JOH-58C USA S/N 70-15349

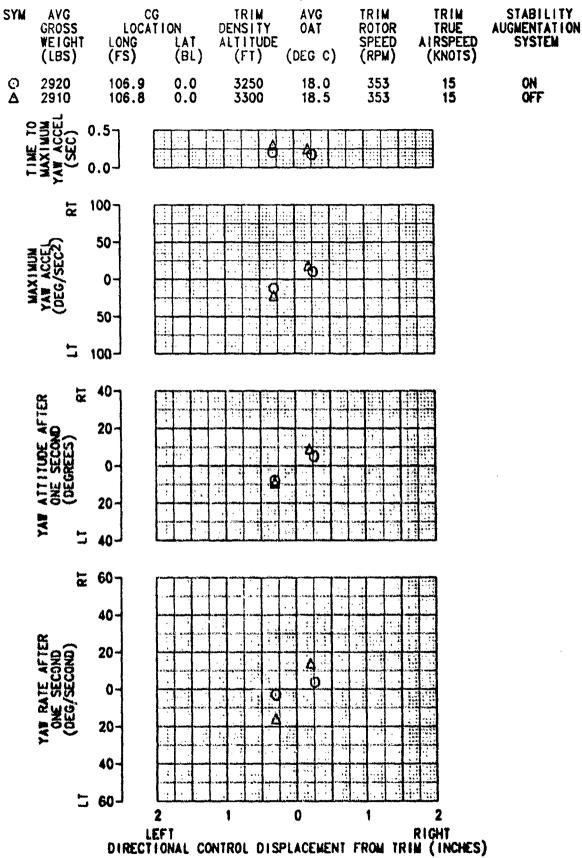


FIGURE E-155
DIRECTIONAL CONTROLLABILITY - 090 DEGREE AZIMUTH
JOH-58C USA S/N 70-15349

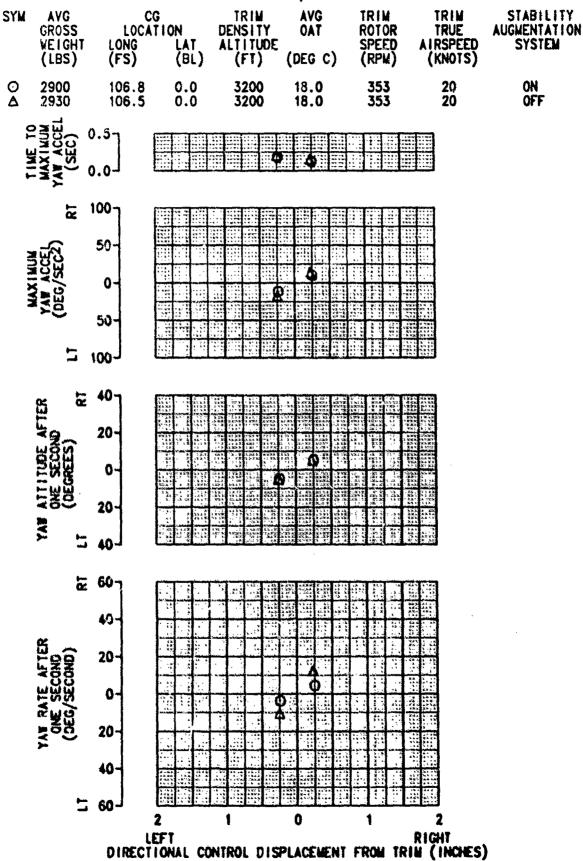


FIGURE E-156

DIRECTIONAL CONTROLLABILITY - 270 DEGREE AZIMUTH

JOH-58C USA S/N 70-15349

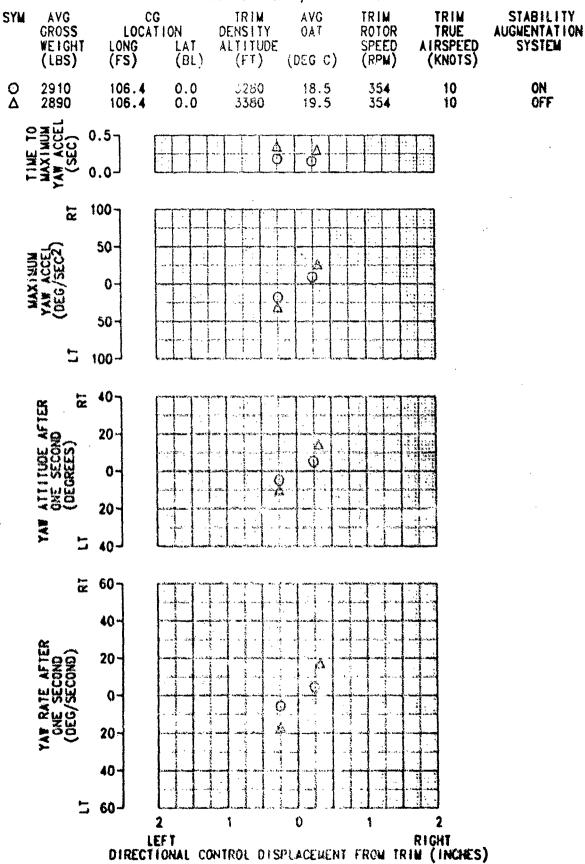


FIGURE E-158 LOW SPEED FLIGHT 180 AND 360 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID HEIGHT
WEIGHT (LB)	(FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2970	107.7	0.0	3360	19.5	354	10

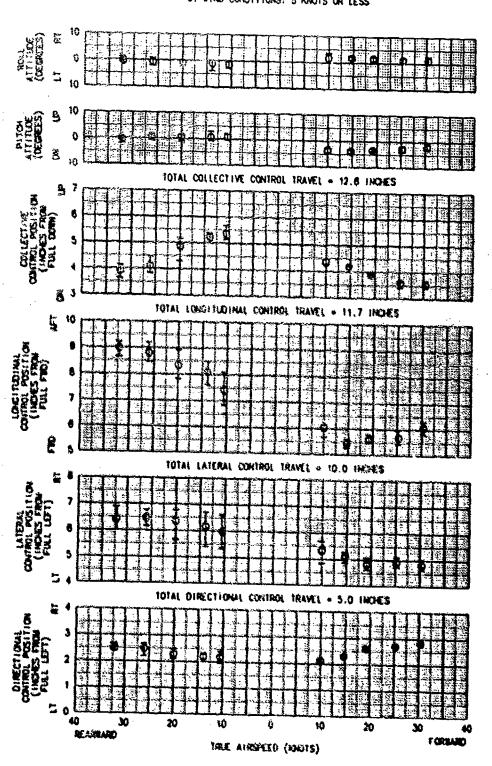


FIGURE E-158 LOW SPEED FLIGHT 180 AND 360 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT	LONG (FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2970	107.7	0.0	3380	19.5	354	10



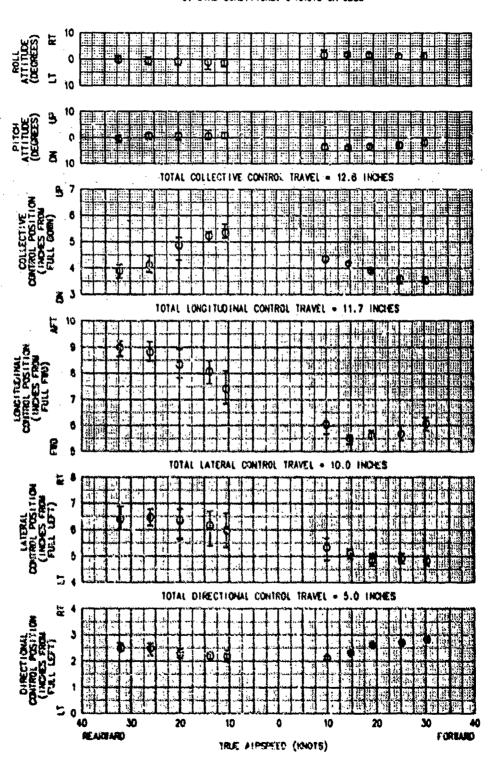


FIGURE E-159 LOW SPEED FLIGHT 180 AND 360 DEGREE AZ IMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID HEIGHT
WEIGHT (LB)	LONG (FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2970	107.7	0.0	3350	19.5	354	10

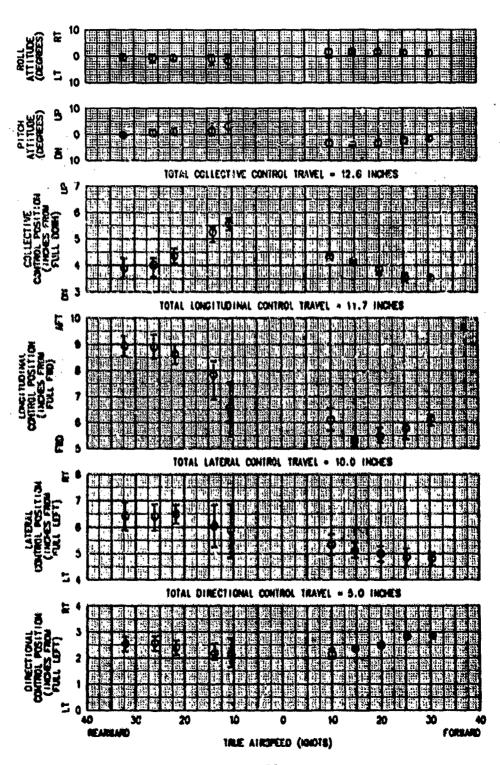


FIGURE E-180 LOW SPEED FLIGHT 45 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVC GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT (LB)	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2950	107.2	0.0	3020	16.5	354	10

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	TOTAL COLLECTIVE CONTROL TRAVEL = 12.6 INCHES
5_ ^{9 7}]	推設的壓倒性準度吸引起應的短期的阻性可能
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8	
¥ 22	TOTAL LONGITUDINAL CONTROL TRAVEL - 11,7 INCHES
<u>.</u> 57	
로드라 아	
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5 5 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
8 6 2	
	TOTAL LATERAL CONTROL TRAVEL . 10.0 INCHES
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3835 o	
그은 말씀	
コ島 ラ 4 コ 4 7	TOTAL DIRECTIONAL CONTROL TRAVEL - 3.0 INCES
3855 6-	TOTAL DIRECTIONAL CONTROL TRAVEL - 5.0 INC.
38 5 4 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	TOTAL DIRECTIONAL CONTROL TRAVEL - 5.0 INC.
38 5 4 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	TOTAL DIRECTIONAL CONTROL TRAVEL - 5.0 INC.
38 5 4 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
ALT THE CONTROL OF TH	
38 5 4 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	

FIGURE E-161 LOW SPEED FLIGHT 45 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVC GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID HEIGHT
WEIGHT	(FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2960	107.1	0.0	3040	16.5	354	10

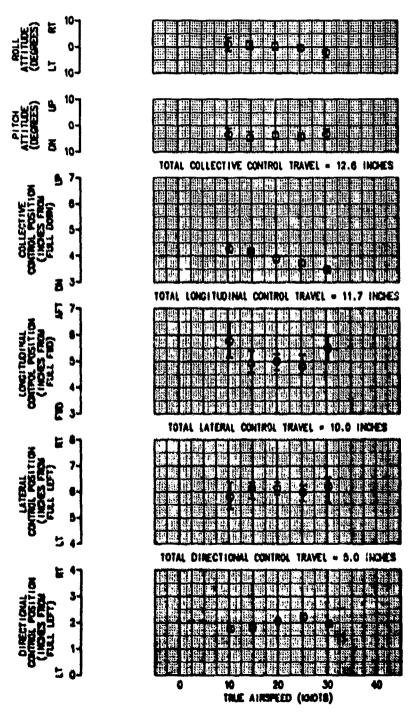


FIGURE E-162 LOW SPEED FLIGHT 270 AND 90 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG Location		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT (LB)	(FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2980	107.2	0.0	3400	20.0	355	10

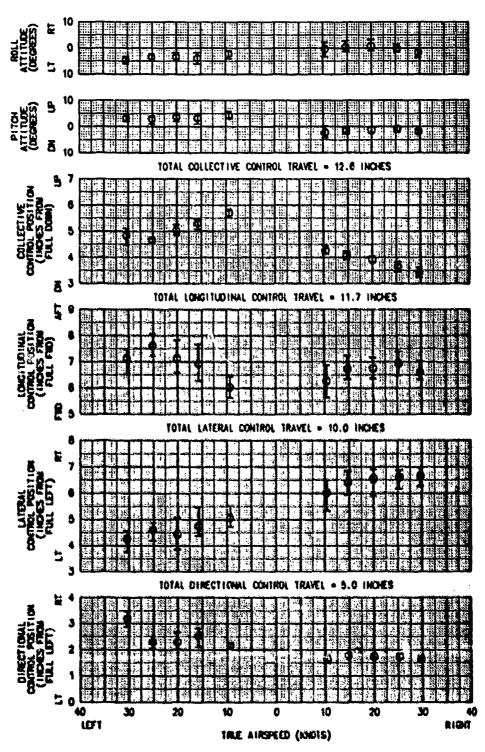


FIGURE E-163 LOW SPEED FLIGHT 270 AND 90 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WE IGHT	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2970	107.2	0.0	3410	20.0	358	10

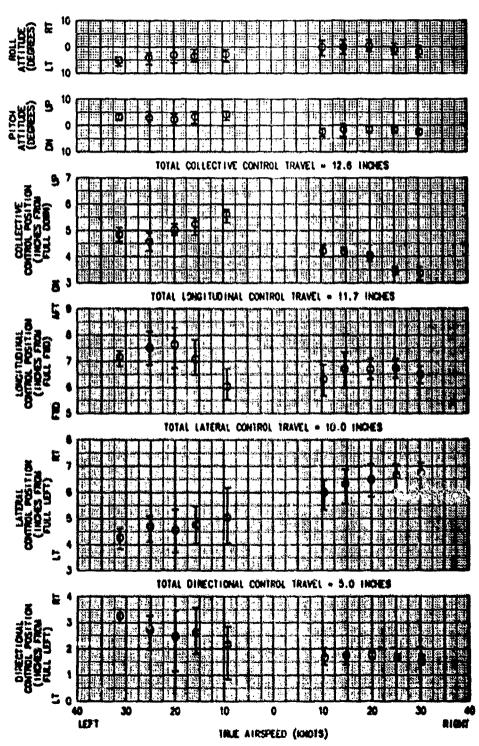


FIGURE E-164 LOW SPEED FLIGHT 120 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG GAT	AVG ROTOR	SKID
(FB)	(FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2960	106.4	0.0	3290	19.0	354	10

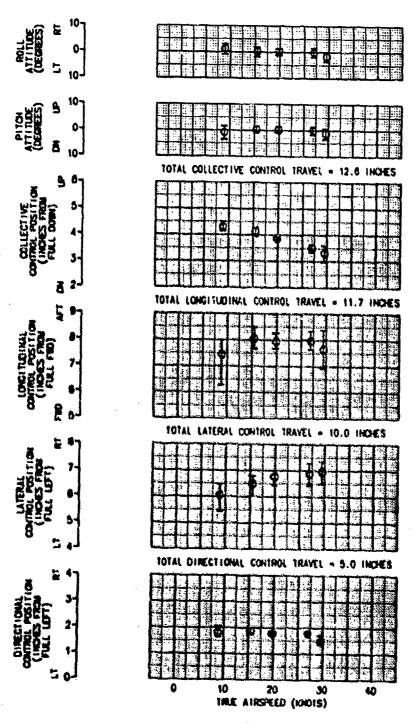


FIGURE E-185 LOW SPEED FLIGHT 120 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT	LONG (FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2960	106.3	0.0	3280	18.5	354	10

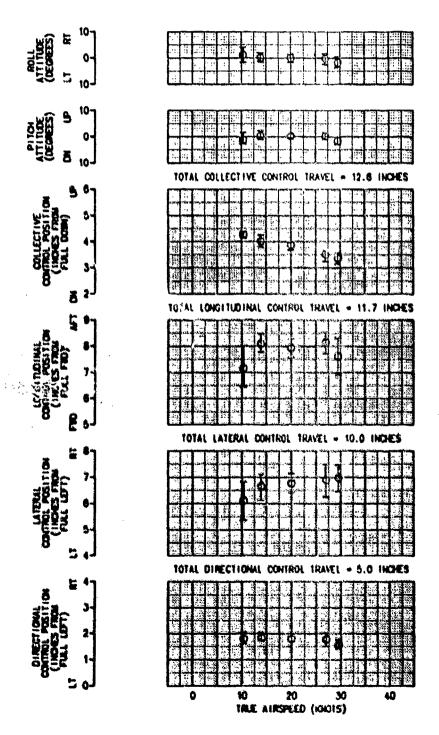


FIGURE E-166 LOW SPEED FLIGHT 150 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT (LB)	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
3020	108.1	0.0	3730	23.0	354	10

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FIGURE E-167 LOW SPEED FLIGHT 150 DEGREE AZIMUTH Jul: 580 S/N 70-15349

AVC GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
(LB)	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
3020	105.1	0.0	3770	23.0	354	10

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FIGURE E-168 LOW SPEED FLIGHT 210 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CS LOCATION		AVG DENSITY	AVG OAT	AVC ROTOR	PE IGHT
(18)	(FS)	(BL)	ALTITUDE (FT)	(DEG C)	(REA)	(FT)
3020	107.2	0.0	4070	25.5	355	10

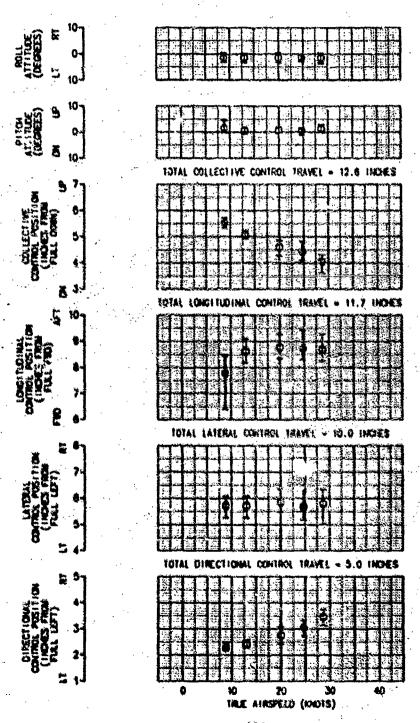


FIGURE E-169 LOW SPEED FLIGHT 210 DEGREE AZIMUTH JOH-58C S/N 70-15349

CK022	AVG CG LOCATION		AVG DENSITY	AVC	AVG ROTOR	SKID
(18) 3030	LONG (FS) 107. i	(BL) 0.0	ALTITUDE (FT) 4040	(DEG C) 25.5	SPEED (RFW) 355	(FT)

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FIGURE E-170 LOW SPEED FLIGHT 225 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	LOCAT	AVG CG LOCATION		AVG OAT	AVG RUTOR	SKID
WEIGHT	(FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
3050	106.8	0.0	4070	25.5	355	10

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CONTROL POSITION (INCLES FROM FULL LEFT) RT RT LT CONTROL LEFT) RT CONTROL	TOTAL DIRECTIONAL CONTROL TRAVEL - 5.0 INCHES
CONTROL POSITION (INCIES FROM FILL LEFT) RT LT FULL LEFT) RT FILL POSITION RT RT LT RT LT RT RT RT LT RT	TOTAL DIRECTIONAL CONTROL TRAVEL - 8.0 INCHES
CONTROL POSITION (INCIES FROM FILL LEFT) RT LT FULL LEFT) RT FILL POSITION RT RT LT RT LT RT RT RT LT RT	TOTAL DIRECTIONAL CONTROL TRAVEL - 5.0 INCHES
CONTROL POSITION (INCIES FROM FILL LEFT) RT LT FULL LEFT) RT FILL POSITION RT RT LT RT LT RT RT RT LT RT	TOTAL DIRECTIONAL CONTROL TRAVEL - 5.0 INCHES
CONTROL POSITION (INCIES FROM FILL LEFT) RT LT FULL LEFT) RT FILL POSITION RT RT LT RT LT RT RT RT LT RT	TOTAL DIRECTIONAL CONTROL TRAVEL - 5.0 INCHES
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FIGURE E-171 LOW SPEED FLIGHT 225 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	OAT	AVG ROTOR	SKID HEIGHT
WEIGHT (LB)	(FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(F1)
3050	106.8	0.0	4070	25.5	356	10

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FIGURE E-172 LOW SPEED FLIGHT 240 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVC GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT (LB)	LONG (FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2990	108.2	0.0	3500	21.0	356	10

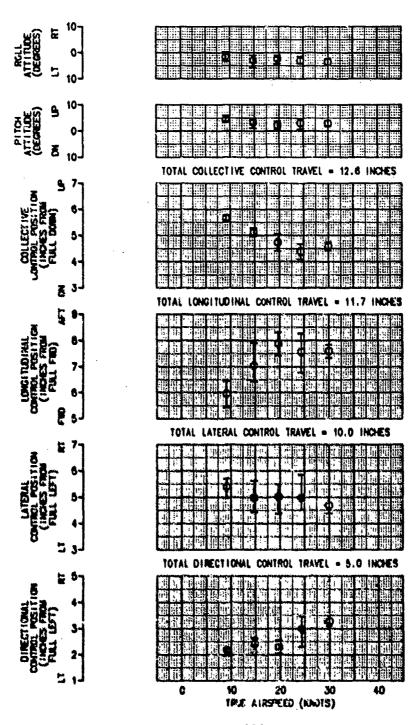


FIGURE E-173 LOW SPEED FLIGHT 240 DEGREE AZIMUTH JOH-58C S/N 70-15349

GROSS	AVG CG LOCATION		AYG DENSITY	AVC	AYC ROTOR	SKID HEIGHT
WE IGHT (LB) 2990	LONG (FS) 108.1	(BL) 0.0	ALTÍTUDE (FT) 3510	(DEG C) 21.0	SPEED (RPM) 356	(FT) 10

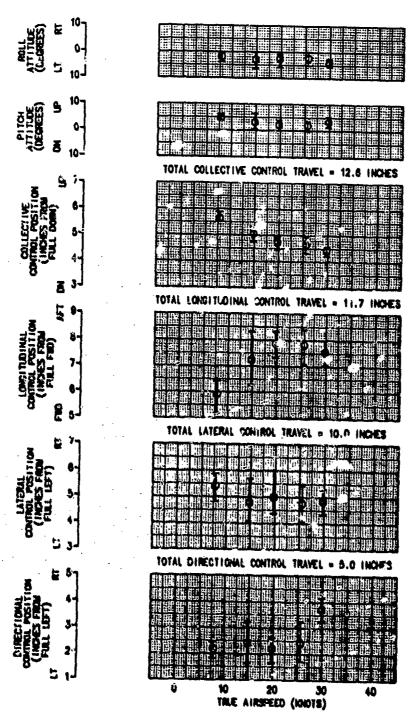


FIGURE E-174 LOW SPEED FLIGHT 280 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AYG DAT	AVG ROTOR	SKID HEIGHT
WEIGHT	(FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2990	107.2	0.0	3640	22.5	357	10

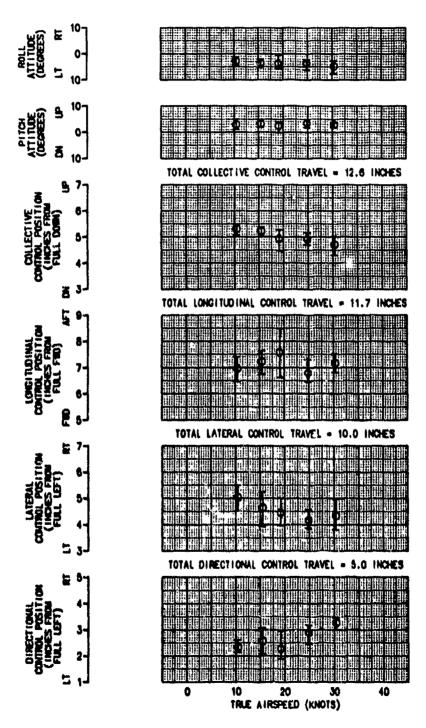


FIGURE E-175 LOW SPEED FLIGHT 280 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG	AVG ROTOR	SKID HEIGHT
(LB)	(FS)	(BL)	ALTÍTUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2990	107.2	0.0	3640	22.5	357	10

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DIRECTIONAL CONTROL POSITION (INCRES FROM FULL LISTY)	0 10 20 30 40 TRUE AIRSPEED (INDIS)

FIGURE E-176 LOW SPEED FLIGHT 290 DEGREE AZIMUTH JOH-580 S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVS DENSITY	AVG OAT	AVG ROTOR	SKID
(LB)	LONG (FS)	(BL)	ALTÍTUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
3000	106.8	0.0	3630	22.5	356	10

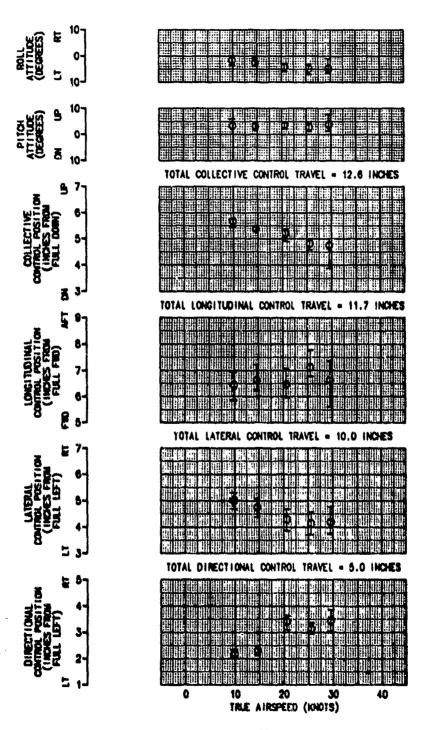


FIGURE E-177 LOW SPEED FLIGHT 290 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVC	AVG CO LOCATION		AYG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT (LB) 2990	LONG (FS) 106.8	(BL) 0.0	ALTÍTÚÓE (FT) 3660	(DEG C) 22.5	SPEED (RPM) 356	(FT)

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FIGURE E-178 LOW SPEED FLIGHT 300 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AYG DENSITY	AVG OAT	AVG ROTOR	SKID HEIGHT
WEIGHT (LB)	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2990	106.4	0.0	3720	23.0	358	10

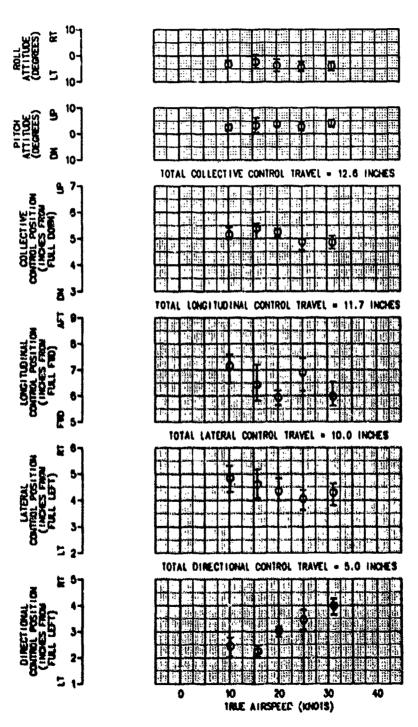


FIGURE E-179 LOW SPEED FLIGHT 300 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AYG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT (LB)	(FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2990	106.4	0.0	3740	23.5	356	10

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FIGURE E-180 LOW SPEED FLIGHT 310 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID HE I GHT
WE IGHT	(FS)	(BL)	ALTITUÓE (FT)	(DEG C)	SPEED (RPM)	(FT)
2990	108.1	0.0	3980	24.5	351	10

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ATTITUE (OEGOEES)	
ATTITUDE (DEGREES) OF 00 0	TOTAL COLLECTIVE CONTROL TRAVEL = 12.6 INCHES
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DIRECTIONAL COMPONE POSITION (HIGHES FROM FILL LETT) RE	TOTAL DIRECTIONAL CONTROL TRAVEL - 5.0 INCHES WHICH WIS

FIGURE E-181 LOW SPEED FLIGHT 310 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG CROSS	AVG CG LOCATION		AYG DENSITY	AVG OAT	AVG ROTOR	HE IGHT
GROSS WEIGHT (LB)	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2990	108.1	0.0	3950	24.5	351	10

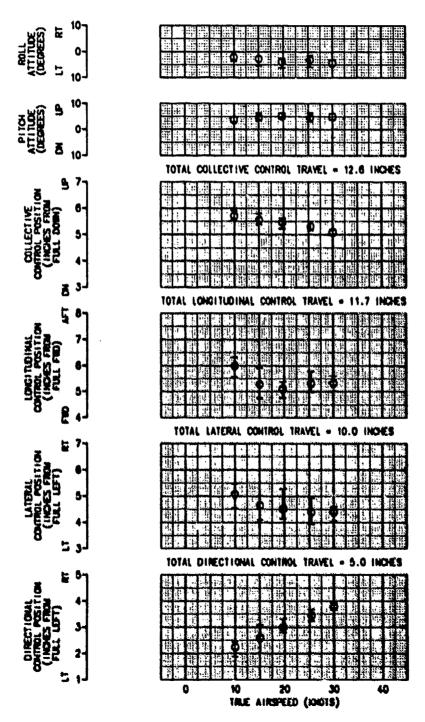


FIGURE E-182 LOW SPEED FLIGHT 320 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID HE IGHT
WEIGHT (LB)	(FS)	(BL)	ÄLTITUDE (FT)	(DEG C)	SPEED (RPM)	(F1)
2980	107.7	0.0	3980	24.5	351	10

NOTES: 1. CONFIGURATION: CLEAN, DOORS ON, SAS ON 2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS 3. BIND CONDITIONS: 5 IGNOTS OR LESS

ATTITUCE (DECREES)	
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FIGURE E-183 LOW SPEED FLIGHT 320 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVQ GROSS	AVG CG LOCAT JON		AYG DENSITY	AVG OAT	AVC ROTOR	HE IGHT
WE IGHT	(FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2960	107.7	0.0	3980	24.5	351	10

NOTES: 1. CONF.GURATION: CLEAN, DOORS ON, SAS OFF 2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS 3. WIND COMPITIONS: 5 KNOTS OR LESS

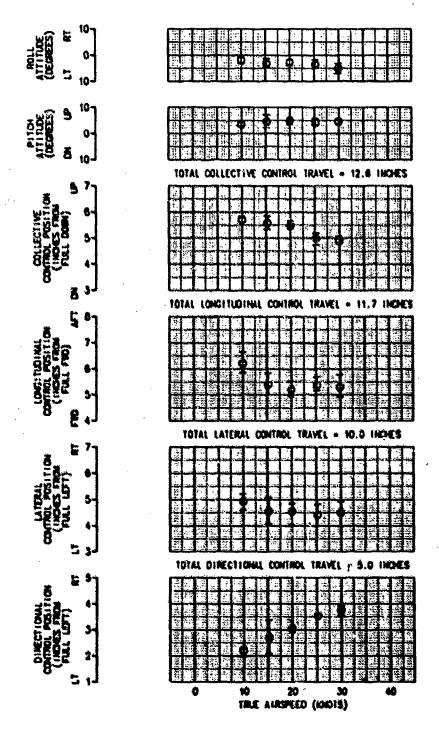


FIGURE E-184 LOW SPEED FLIGHT 330 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVC OAT	AVG ROTOR	SKID
WEIGHT (LB)	LONG (FS)	LAY (BL)	AL(ITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
3000	107.2	0.0	4050	25.5	350	10

NOTES: 1. CONFIGURATION: CLEAN, DOORS ON, SAS ON
2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS
3. WIND CONDITIONS: 5 KNOTS OR LESS

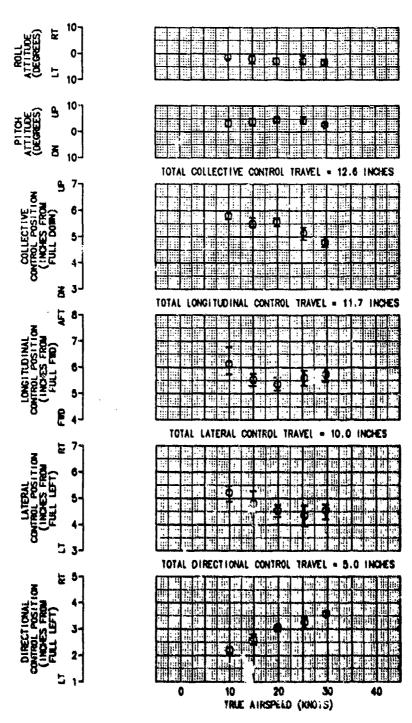


FIGURE E-185 LOW SPEED FLIGHT 330 DEGREE AZIMUTH JOH-18C S/N 70-15349

AVG GROSS	≠VG CG LOCATION		AYG DENSITY	AVG OAT	AVG ROTOR	HE IGHT SKID
WEIGHT (LB)	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEÉD (RPM)	(FT)
3000	107.2	0.0	4050	25.5	351	10

NOTES: 1. CONFIGURATION: CLEAN, DOORS ON, SAS OFF
2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS
3. WIND CONDITIONS: 5 KNOTS OR LESS

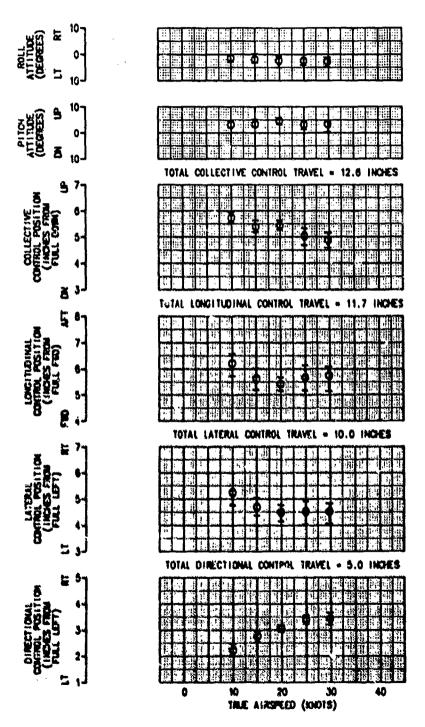


FIGURE E-186 LOW SPEED FLIGHT 340 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID HEIGHT
WE IGHT	(FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2290	106.9	0.0	4100	25.5	352	10

NOTES: 1. CONFIGURATION: CLEAN, DOORS ON, SAS ON
2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS
3. WIND CONDITIONS: 5 KNOTS OR LESS

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FIGURE E-187 LOW SPEED FLIGHT 340 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	HEIGHT
MEIGHT	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2990	106.9	0.0	4090	25.5	352	10

NOTES: 1. CONFIGURATION: CLEAN, DOORS ON, SAS OFF 2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS 3. WIND CONDITIONS: 5 KNOTS OR LESS

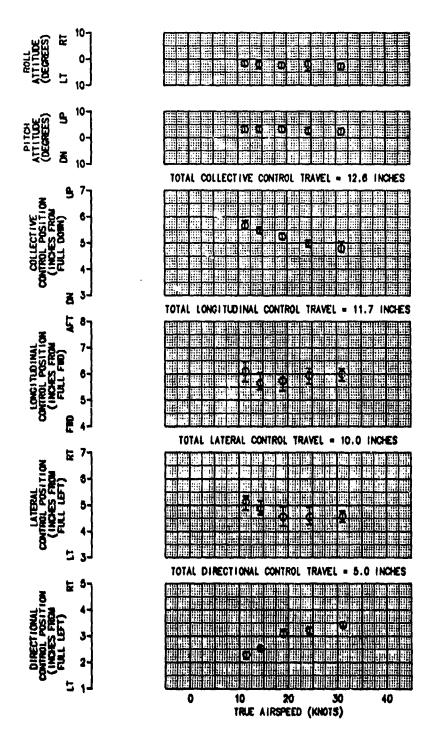


FIGURE E-188 LOW SPEED FLIGHT 350 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	HE IGHT
WEIGHT	LONG (FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2980	106.7	0.0	4120	26.0	35 3	10

NOTES: 1. CONFIGURATION: CLEAN, DOORS ON, SAS ON 2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS 3. WIND CONDITIONS: 5 KNOTS OR LESS

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MIRGI POSITION (INCLESS FROM FULL LEFT) RIT FRO 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	TOTAL LATERAL CONTROL TRAVEL - 10.0 INCHES
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CONTROL POSITION CONTROL POSITION CONTROL POSITION CONTROL POSITION CONTROL LEFT) RT FTD CONTROL CONTR	TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES
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POSITION CONTROL POSITI	TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL DIRECTIONAL CONTROL TRAVEL = 5.0 INCHES
POSITION CONTROL POSITI	TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL DIRECTIONAL CONTROL TRAVEL = 5.0 INCHES
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RECTIONAL CONTROL POSITION CONTROL LEFT) RT FTD CONTRO	TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL DIRECTIONAL CONTROL TRAVEL = 5.0 INCHES
RECTIONAL CONTROL POSITION CONTROL LEFT) RT FTD CONTRO	TOTAL LATERAL CONTROL TRAVEL - 10.0 INCHES TOTAL LATERAL CONTROL TRAVEL - 10.0 INCHES TOTAL DISCRIPTIONAL CONTROL TRAVEL - 5.0 INCHES
CONTROL POSITION CONTROL POSITION CHOES FROM FULL LEFT) RT LT FULL LEFT) RT FROM FOR EXAMPLE STATEMENT RT LT FULL LEFT) RT FROM FOR EXAMPLE STATEMENT RT LT FULL LEFT) RT LT FULL LEFT	TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL DIRECTIONAL CONTROL TRAVEL = 5.0 INCHES TOTAL DIRECTIONAL CONTROL TRAVEL = 5.0 INCHES TOTAL DIRECTIONAL CONTROL TRAVEL = 5.0 INCHES
CONTROL POSITION CONTROL POSITION CHOES FROM FULL LEFT) RT LT FULL LEFT) RT FROM FOR EXAMPLE STATEMENT RT LT FULL LEFT) RT FROM FOR EXAMPLE STATEMENT RT LT FULL LEFT) RT LT FULL LEFT	TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL LATERAL CONTROL TRAVEL = 10.0 INCHES TOTAL DISCRIPTIONAL CONTROL TRAVEL = 5.0 INCHES

FIGURE E-189 LOW SPEED FLIGHT 350 DEGREE AZIMUTH JOH-58C S/N 70-15349

AVG GROSS	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID HEIGHT
WEIGHT	LONG (FS)	(BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2980	106.7	0.0	4120	26.0	353	10

NOTES: 1. CONFIGURATION: CLEAN, DOORS ON, SAS OFF
2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS
3. WIND CONDITIONS: 5 KNOTS OR LESS

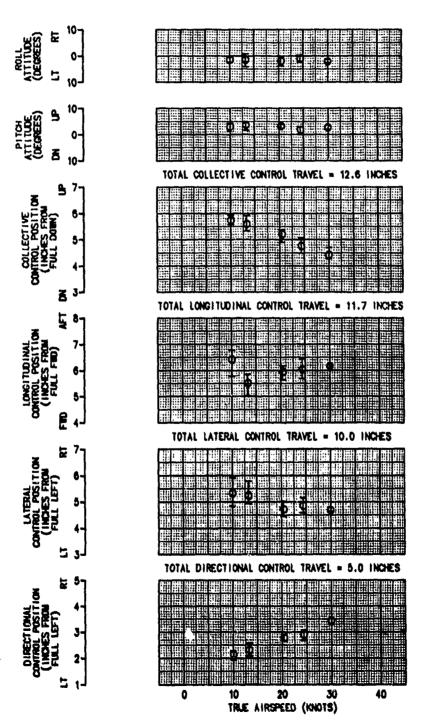


FIGURE E-190 LOW SPEED FLIGHT 120 DEGREE AZIMUTH JOH-58C S/N 70-15349

AYG GROSS WE IGHT (LB)	AVG CG LOCATION		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
	(FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2950	107.9	0.0	3760	22.5	352	10

NOTES: 1. CONFIGURATION: CLEAN, DOORS OFF, SAS ON 2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS 3. WIND CONDITIONS: 5 KNOTS OR LESS

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FIGURE E-191 LOW SPEED FLIGHT 180 DEGREE AZ IMUTH JOH-58C S/N 70-15349

AVG CROSS	AVG LOCAT		AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WEIGHT (LB)	LONG (FS)	LAT (BL)	ALTÍTUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2940	107.8	0.0	3900	24.0	353	10

1. CONFIGURATION: CLEAN, DOORS OFF, SAS ON 2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS 3. WIND CONDITIONS: 5 KNOTS OR LESS

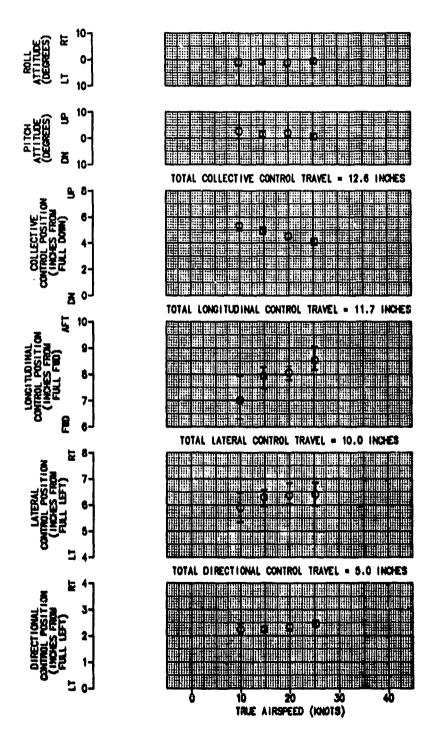
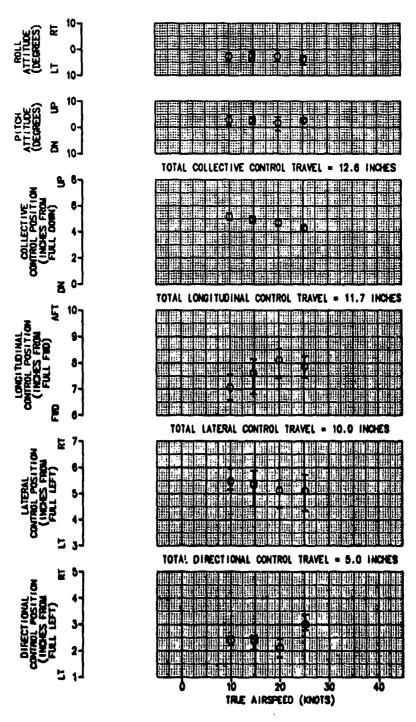
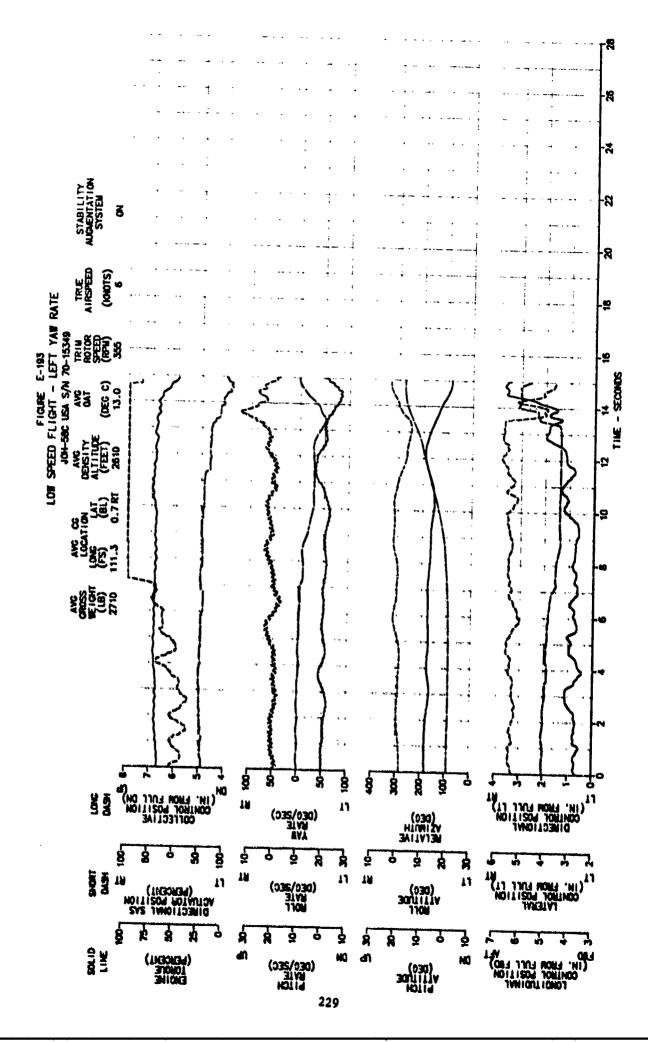


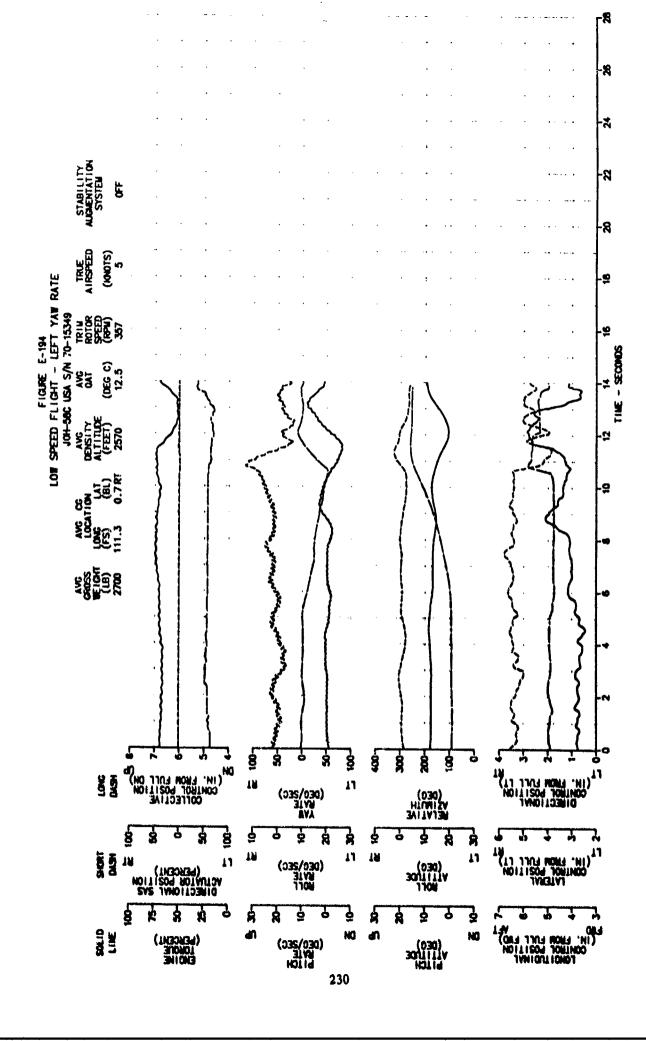
FIGURE E-192 LOW SPEED FLIGHT 240 DEGREE AZIMUTH JOH-58C S/N 70-15349

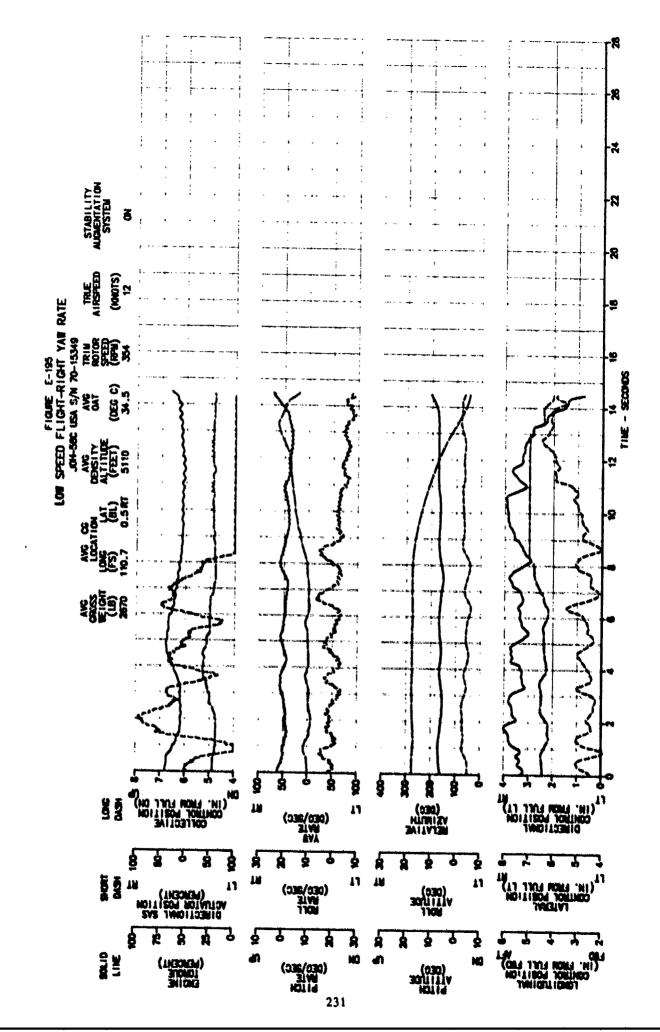
AVG GROSS	AVG LOCA	TÍÖN	AVG DENSITY	AVG OAT	AVG ROTOR	SKID
WE IGHT	(FS)	LAT (BL)	ALTITUDE (FT)	(DEG C)	SPEED (RPM)	(FT)
2950	107.4	0.0	3960	24.5	356	10

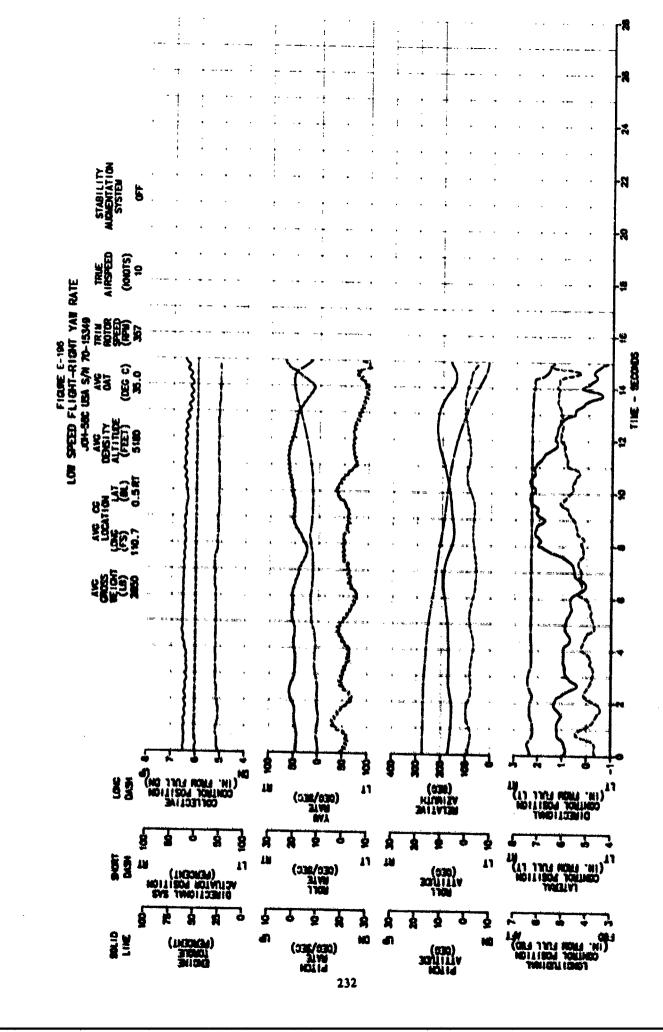
NOTES: 1. CONFIGURATION: CLEAN, DOORS OFF, SAS ON 2. I DENOTES CONTROL AND ATTITUDE EXCURSIONS 3. WIND CONDITIONS: 5 KNOTS OR LESS

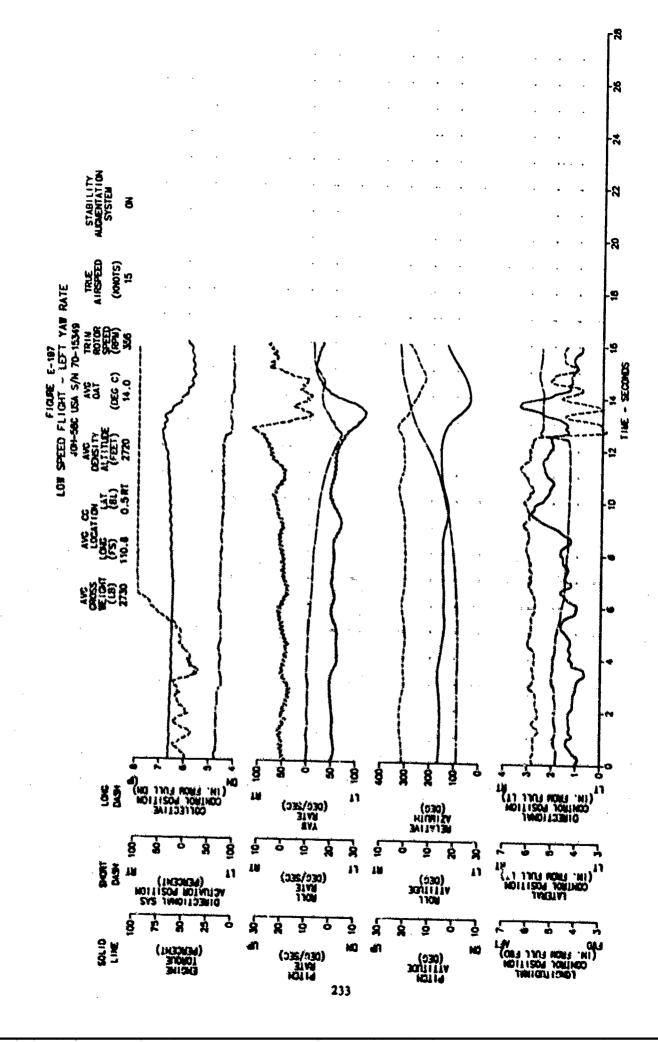


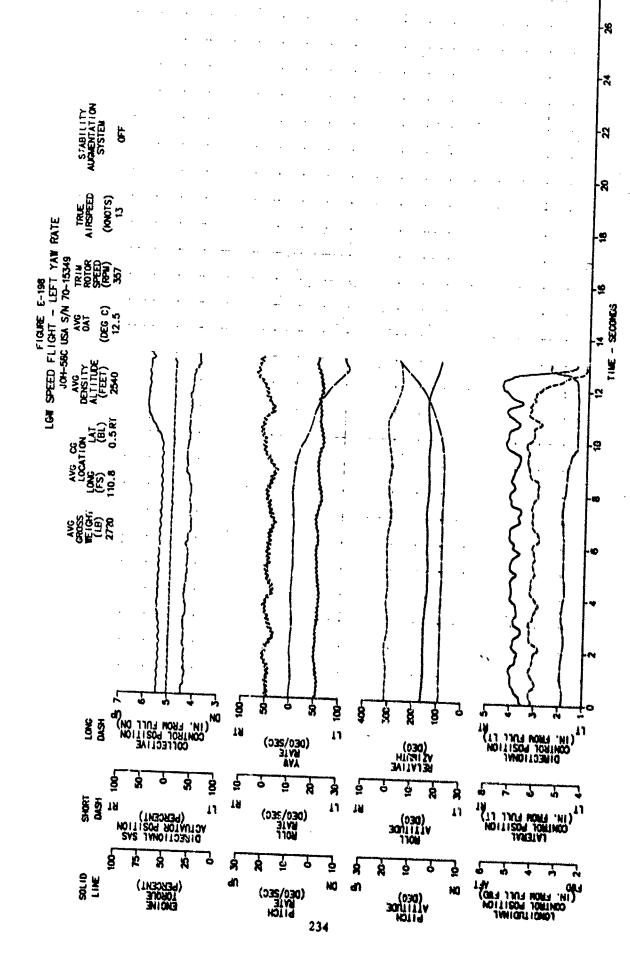


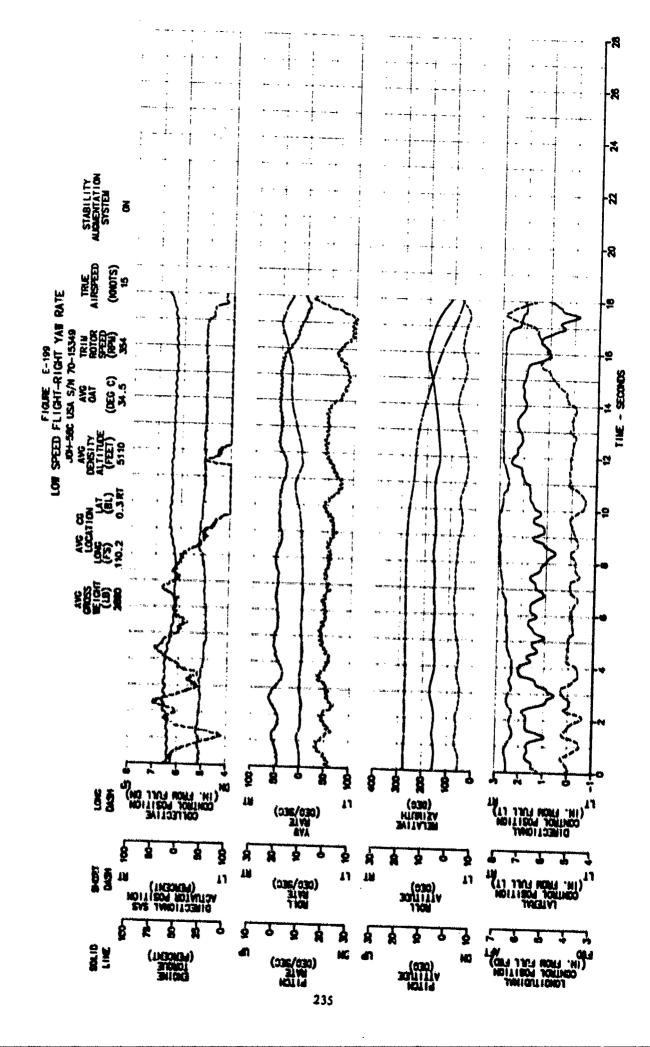


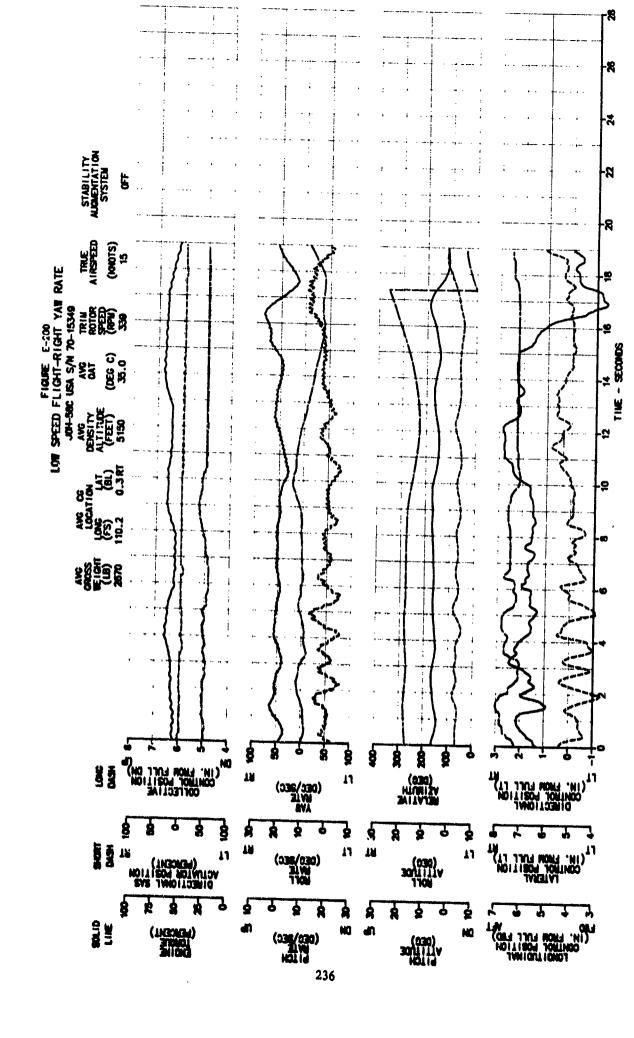


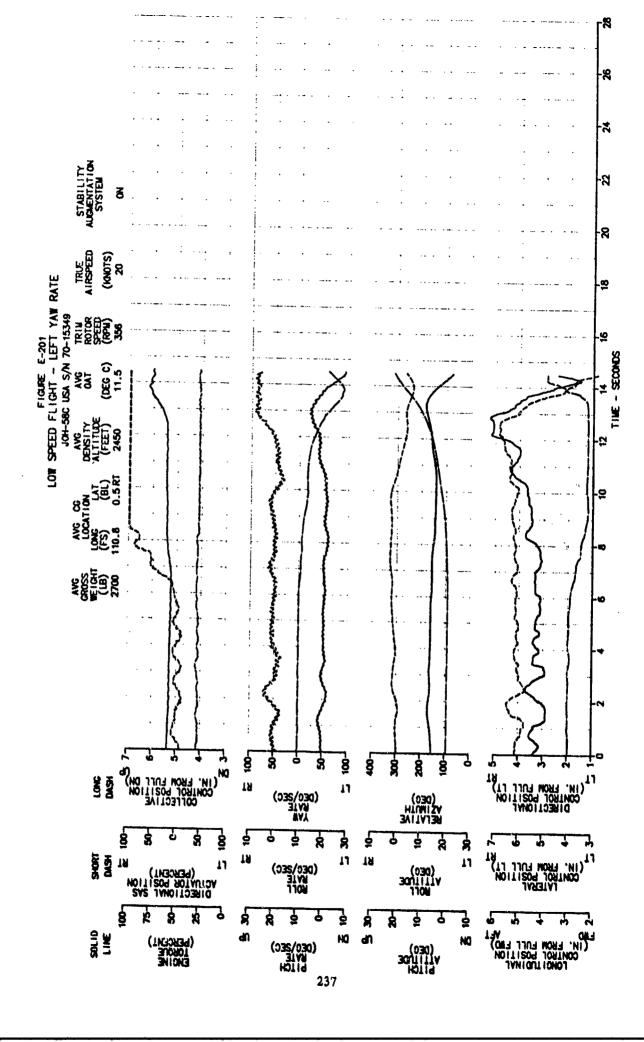


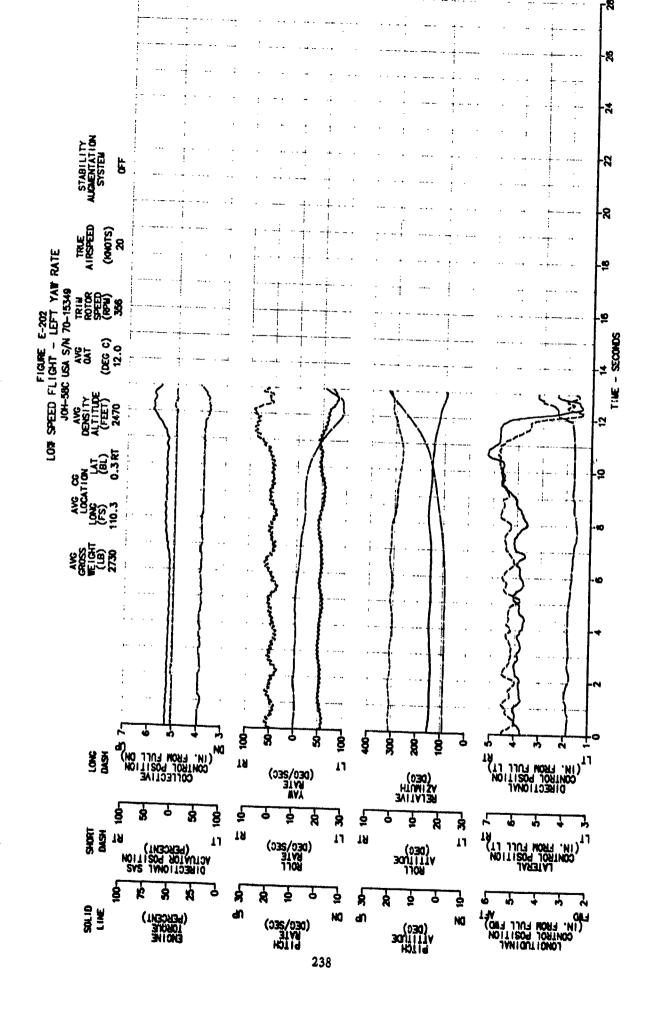


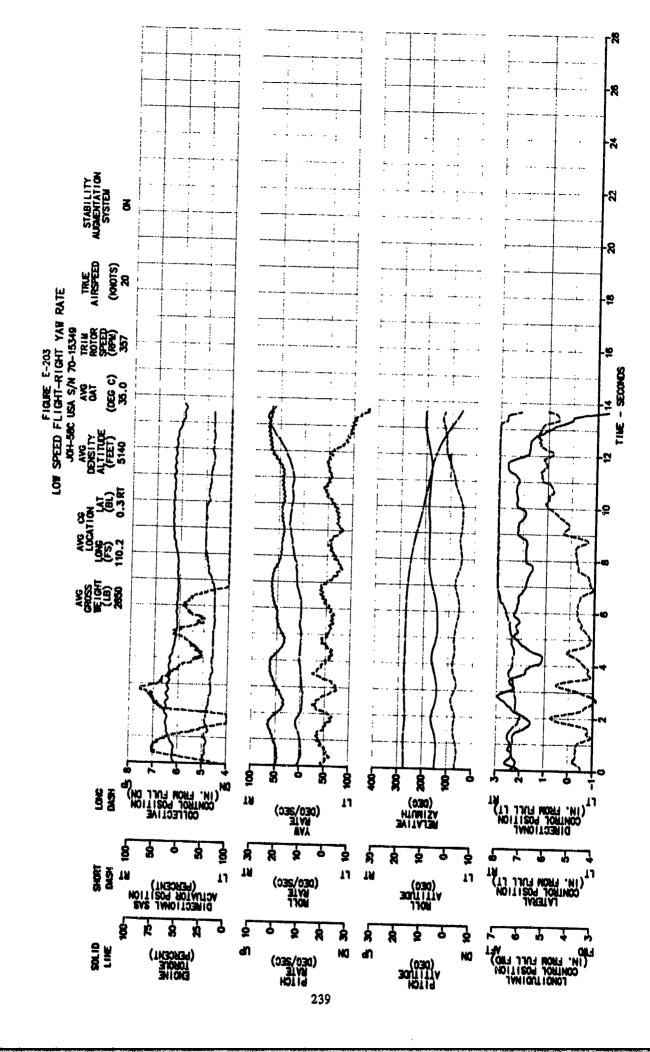


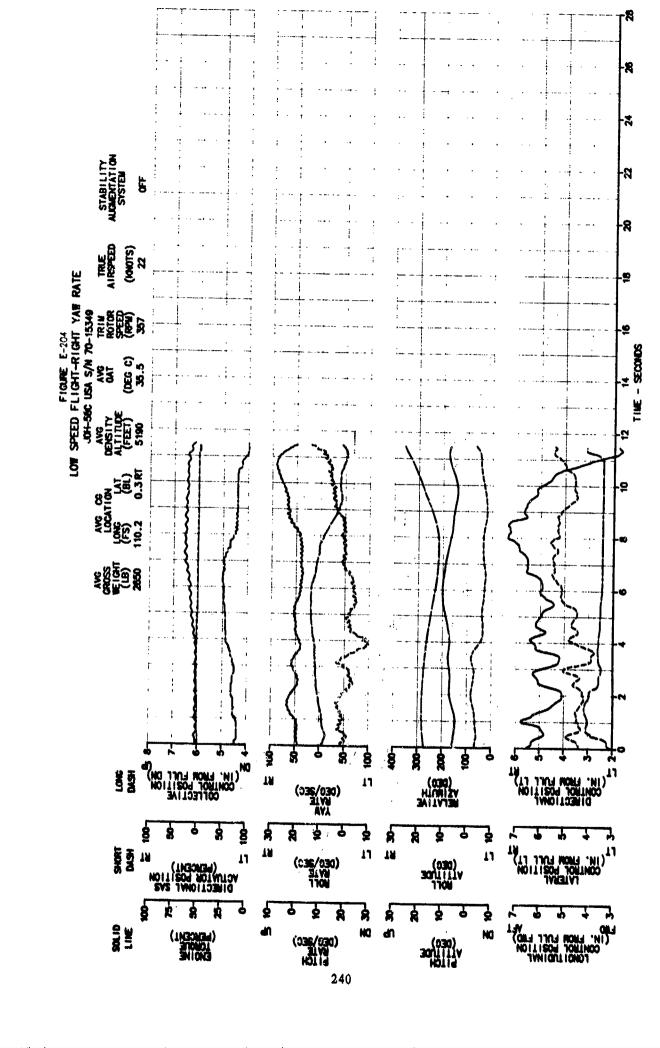


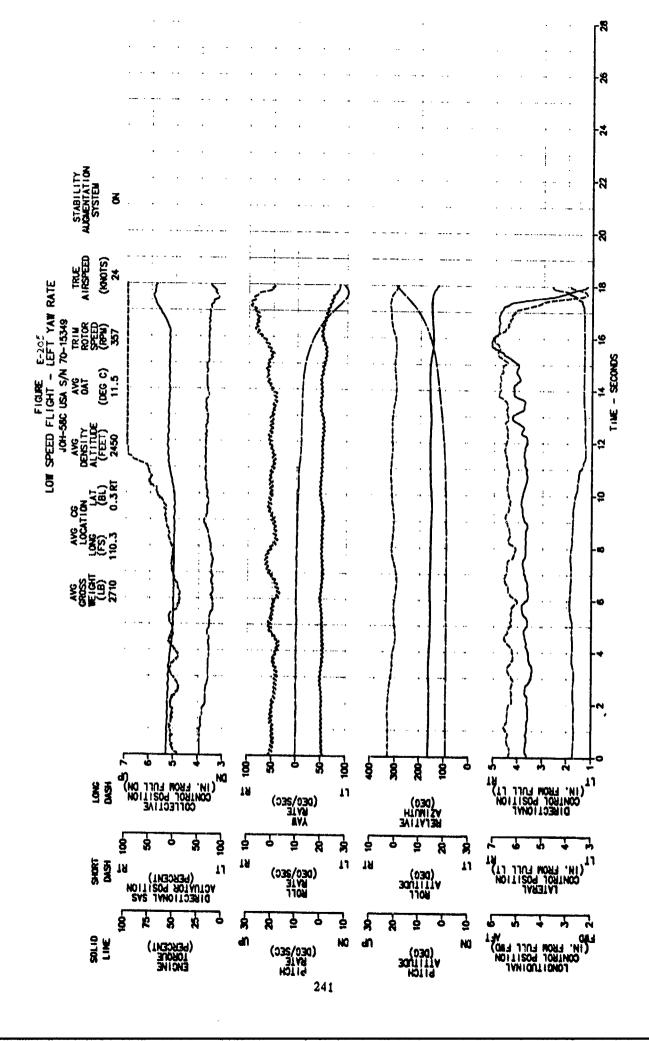


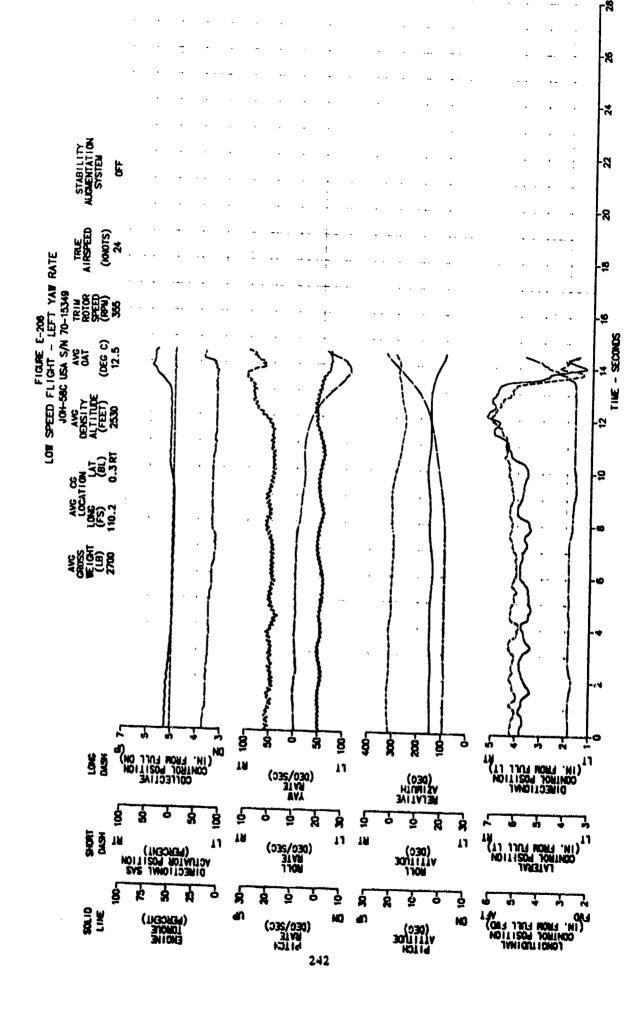


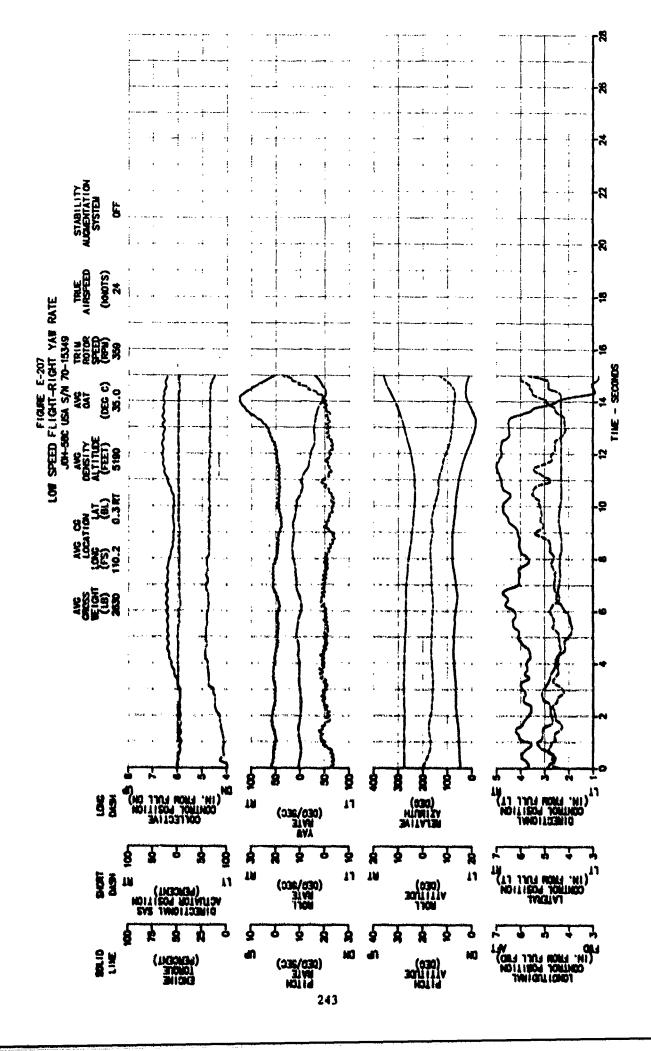












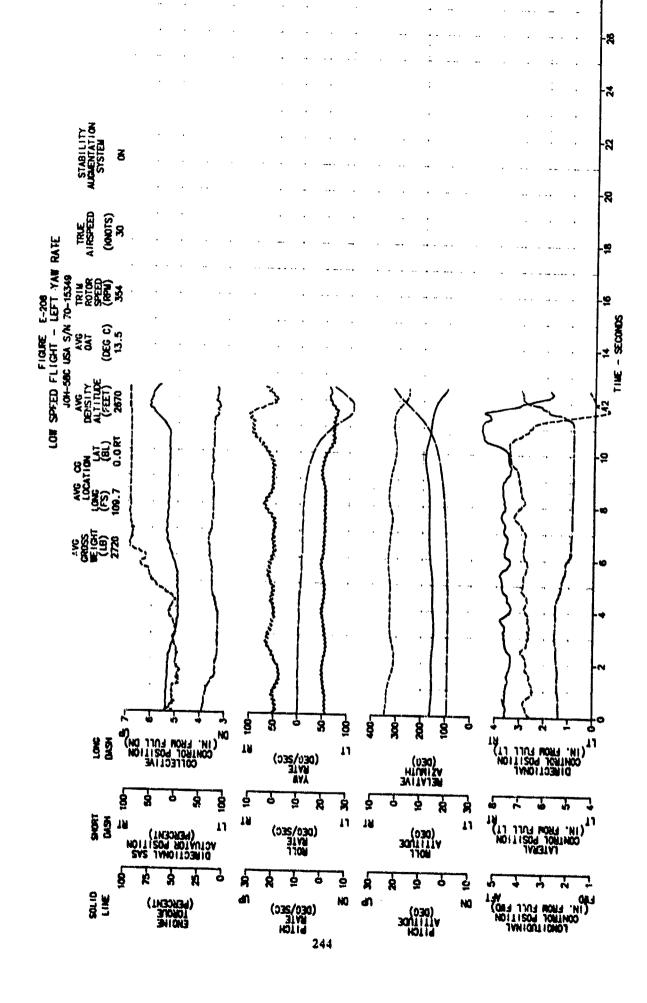


FIGURE E-209 DIRECTIONAL TRIM CHANGES WITH POWER JOH-58C S/N 70-15349

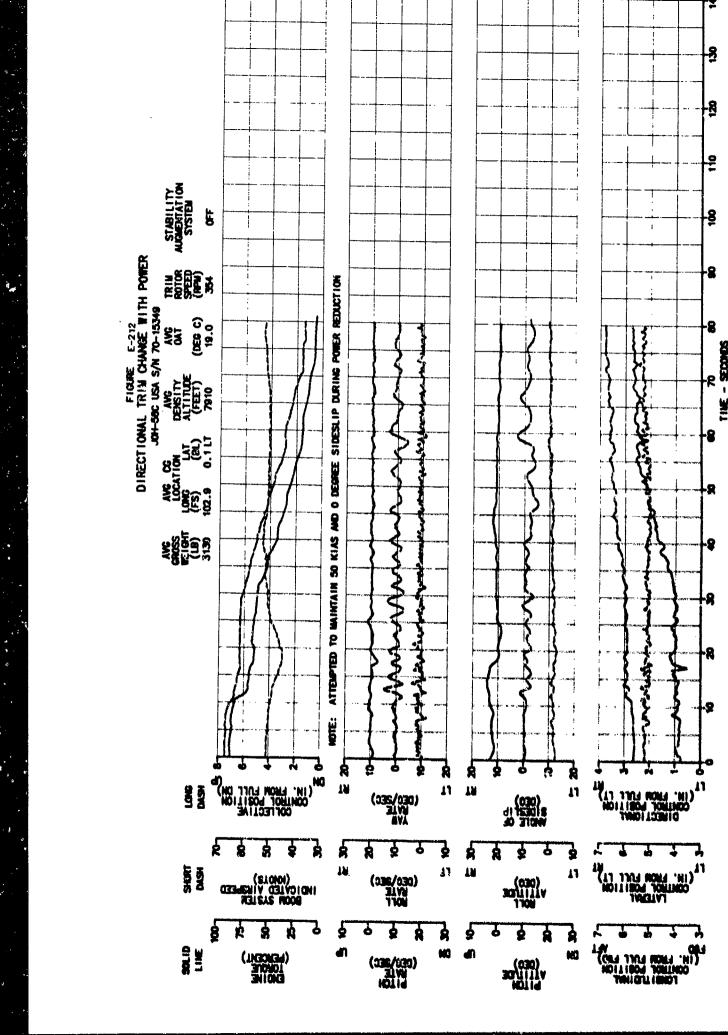
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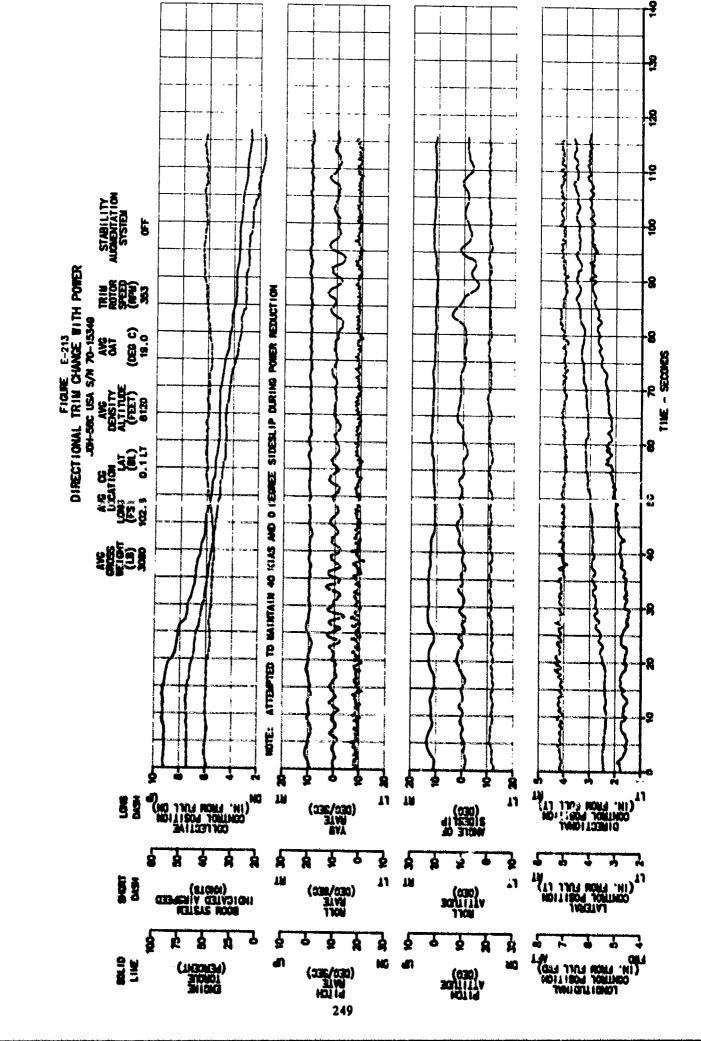
FIGURE E-210 DIRECTIONAL TRIM CHANGES WITH POWER JOH-58C S/N 70-15349

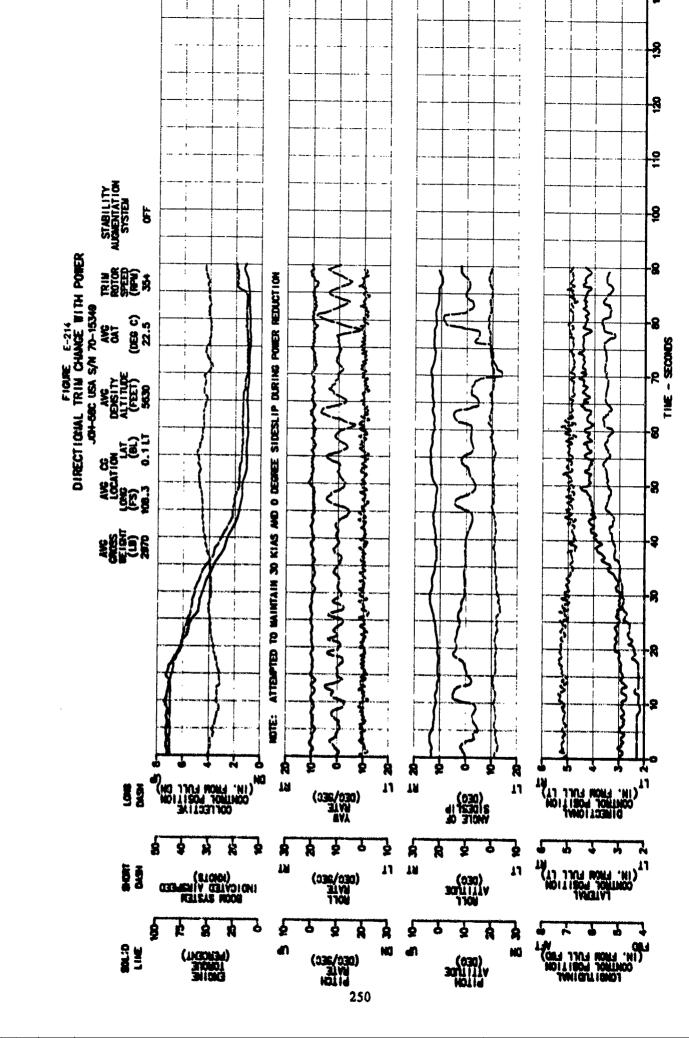
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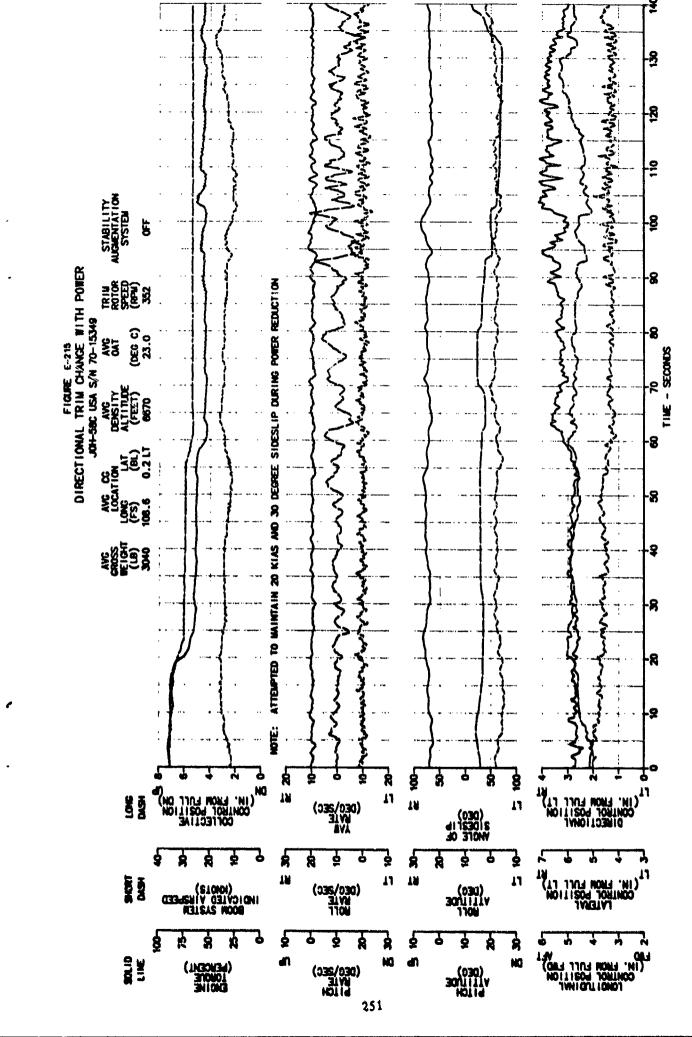
FIGURE E-211
DIRECTIONAL TRIM CHANGES WITH FOWER
JOH-58C S/N 70-15349

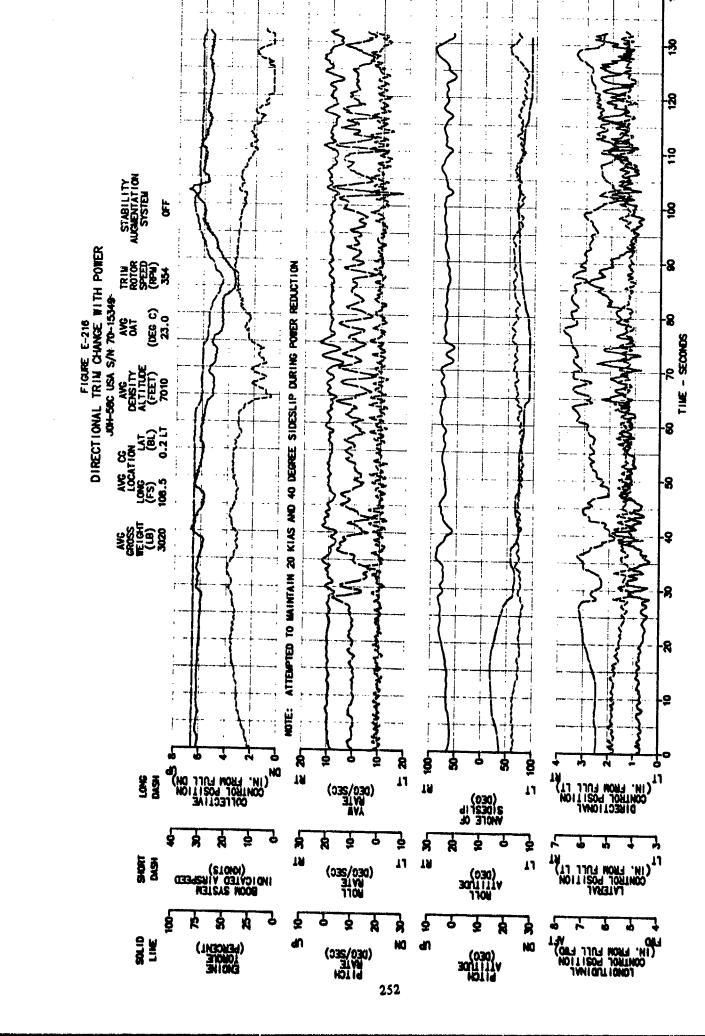
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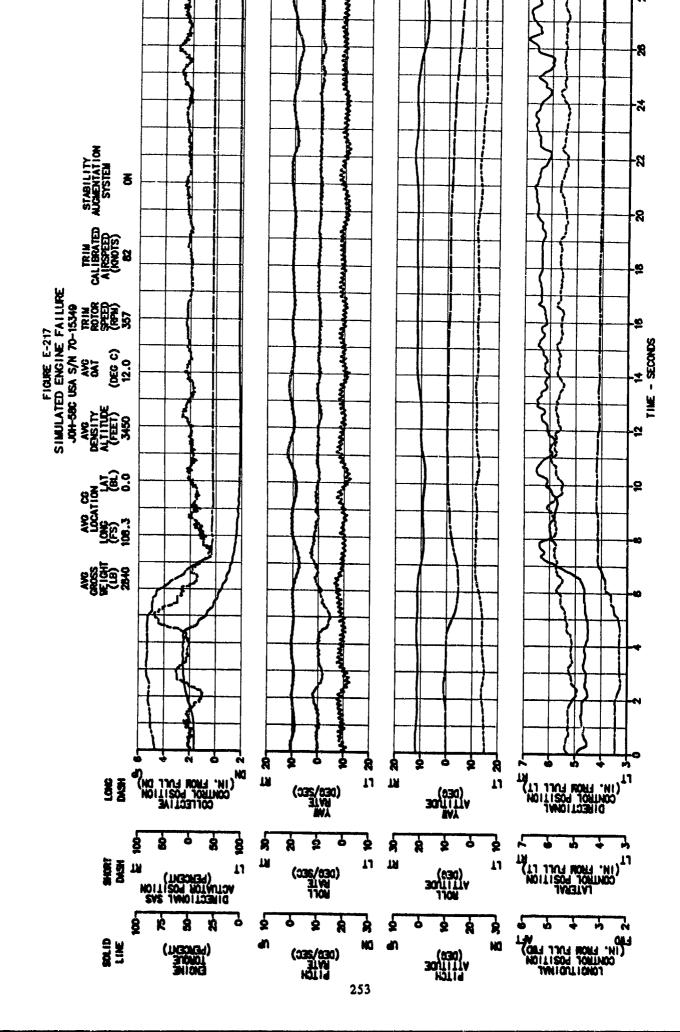


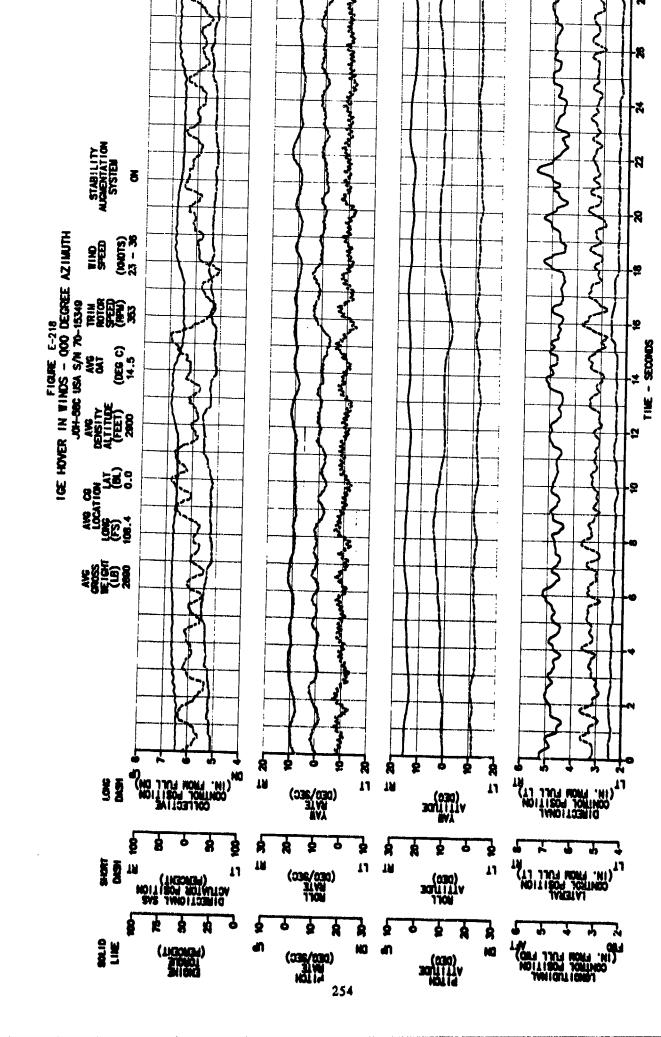


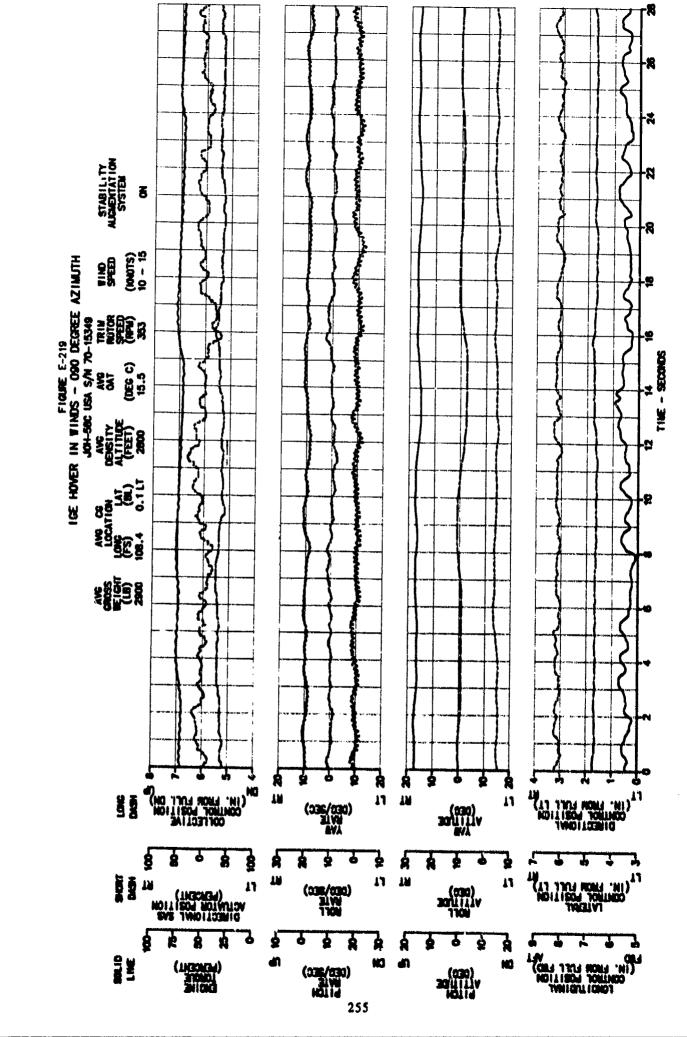


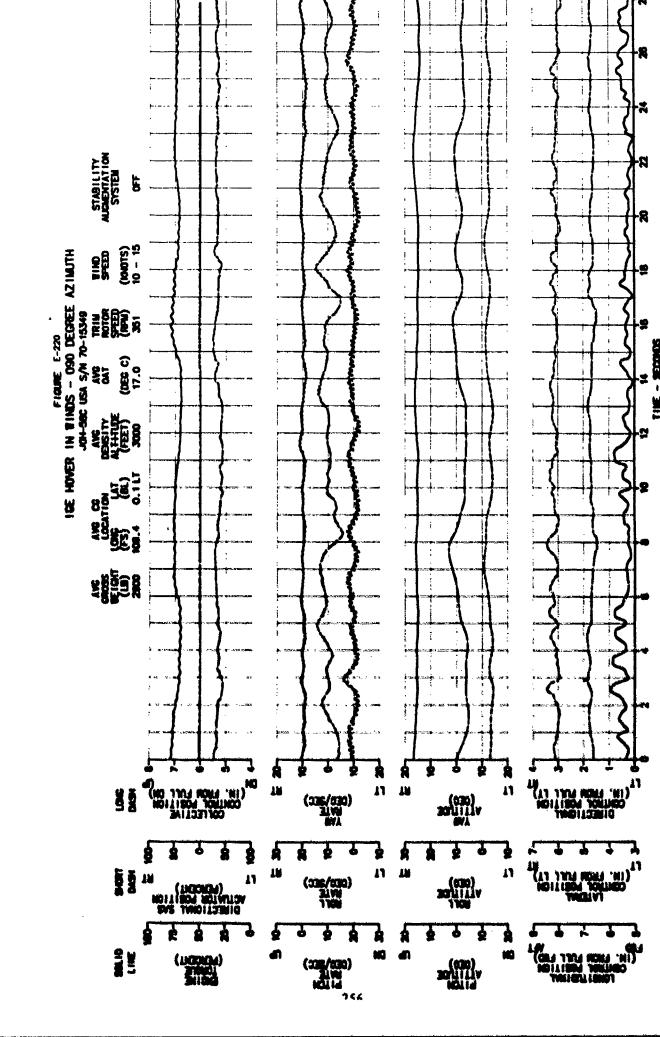


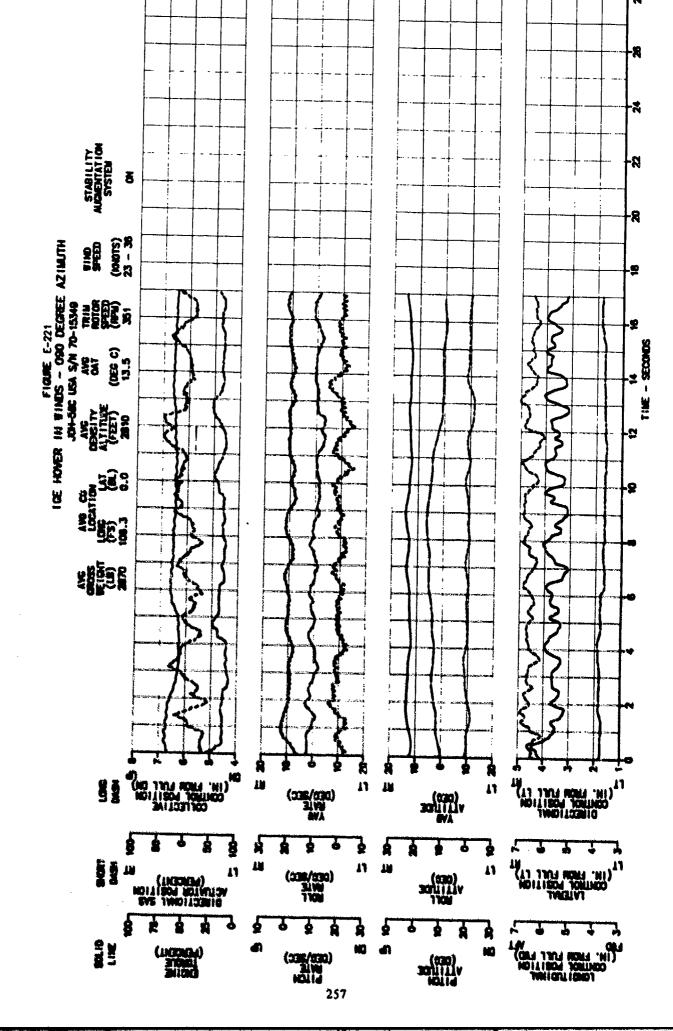


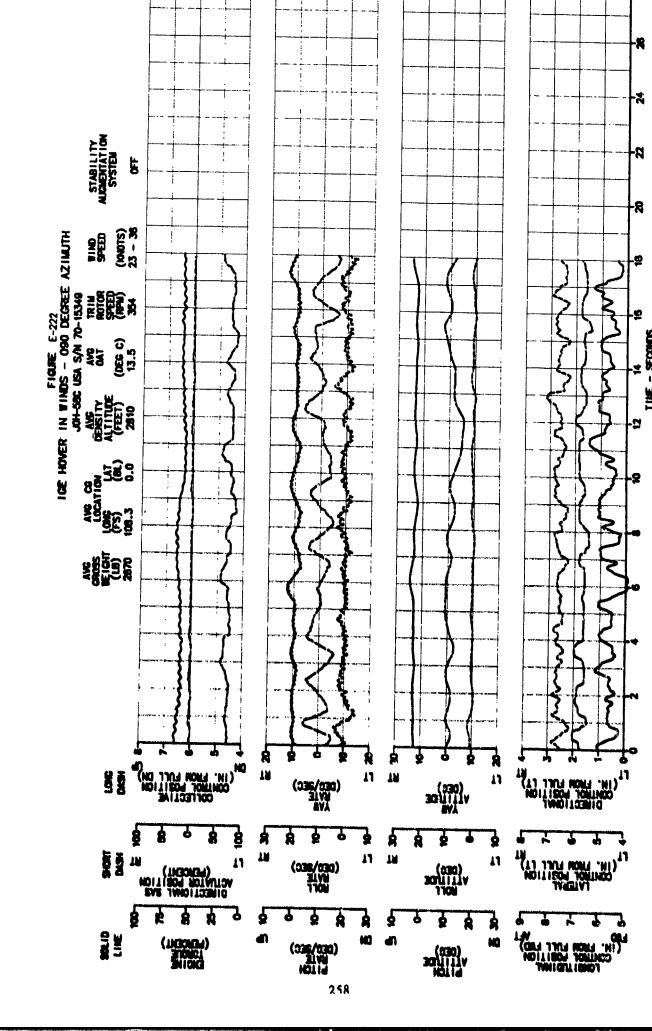


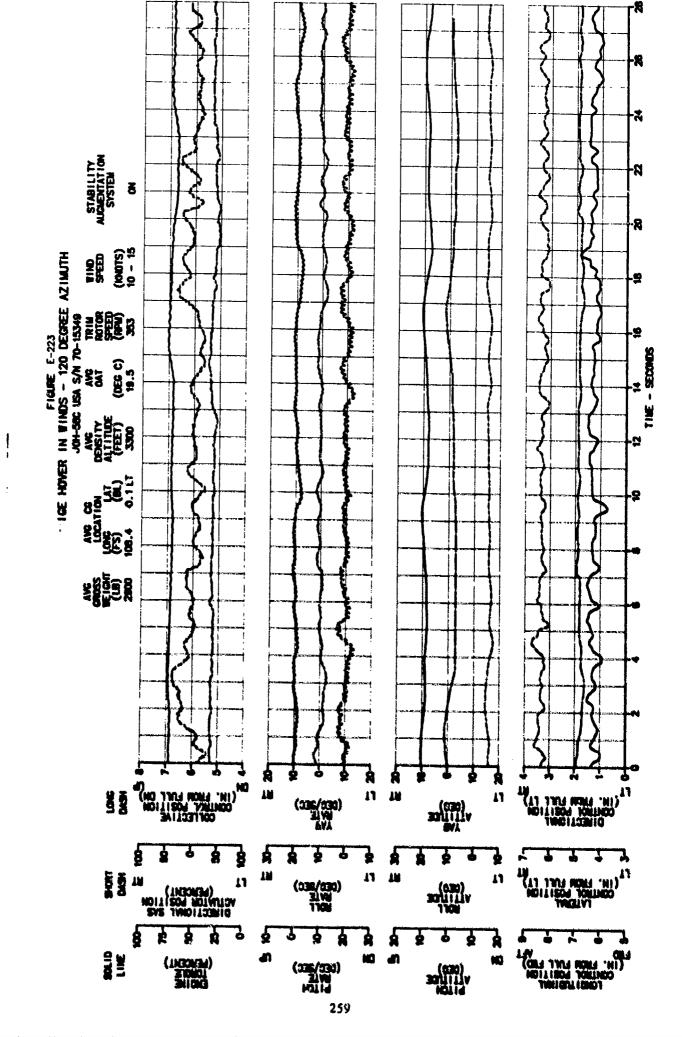


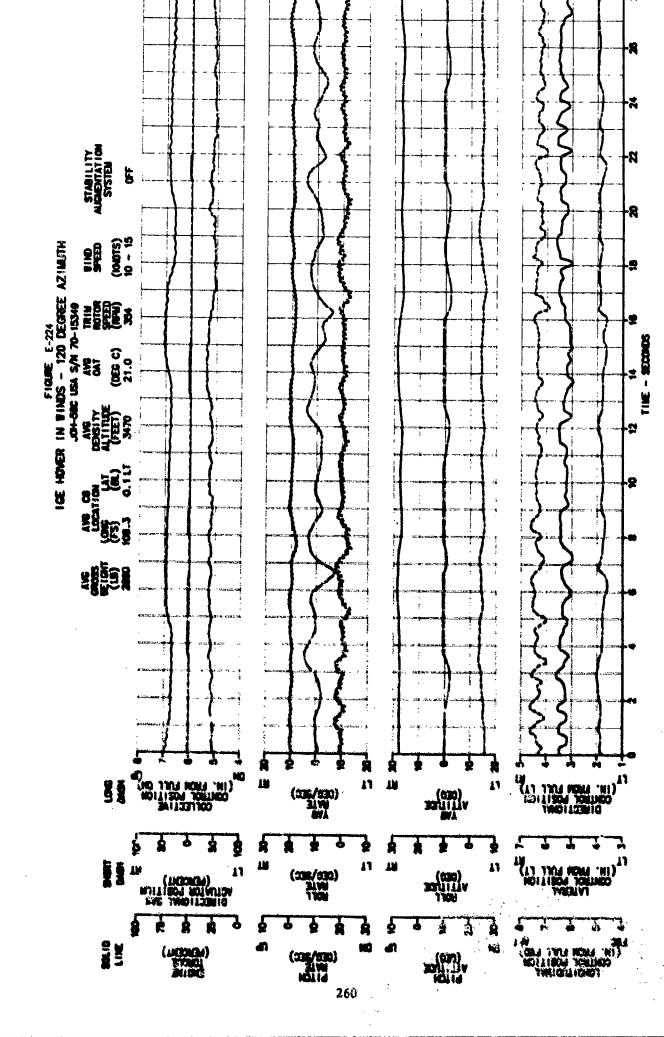


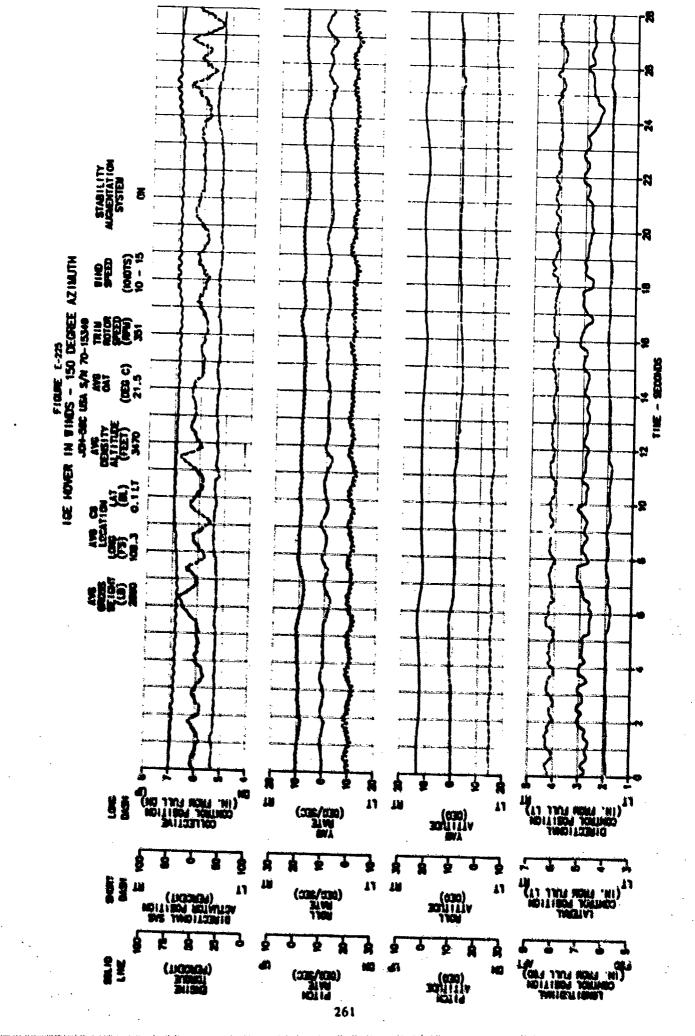


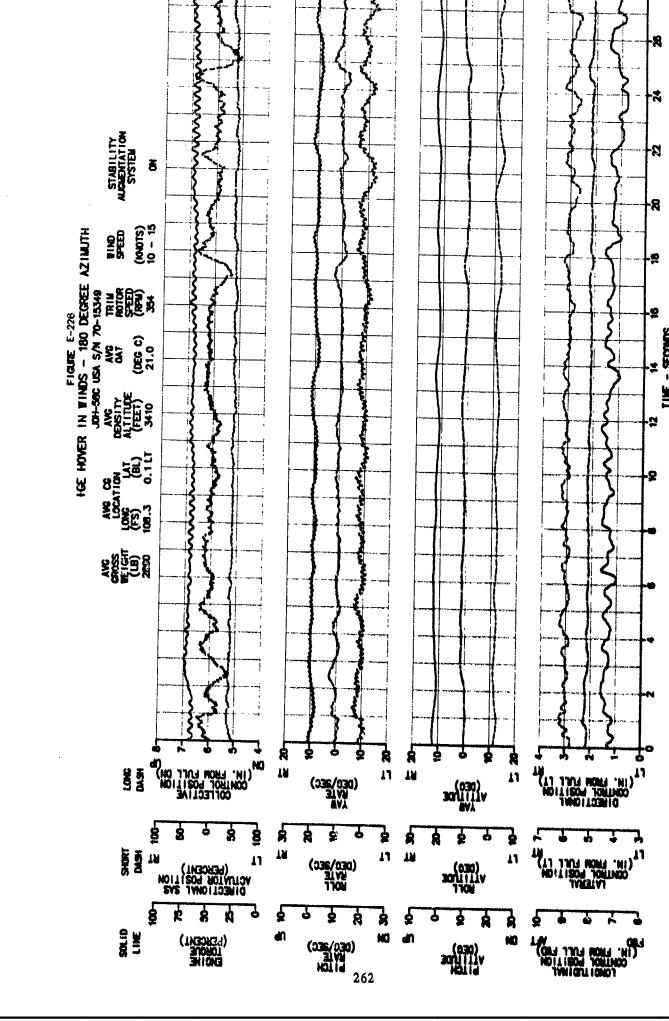


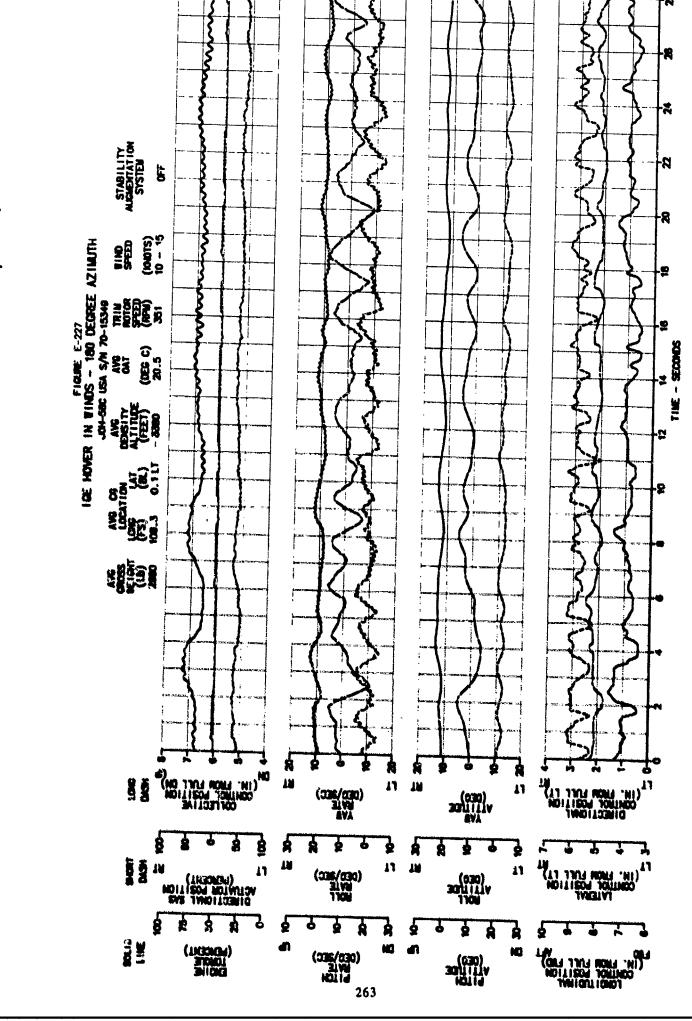


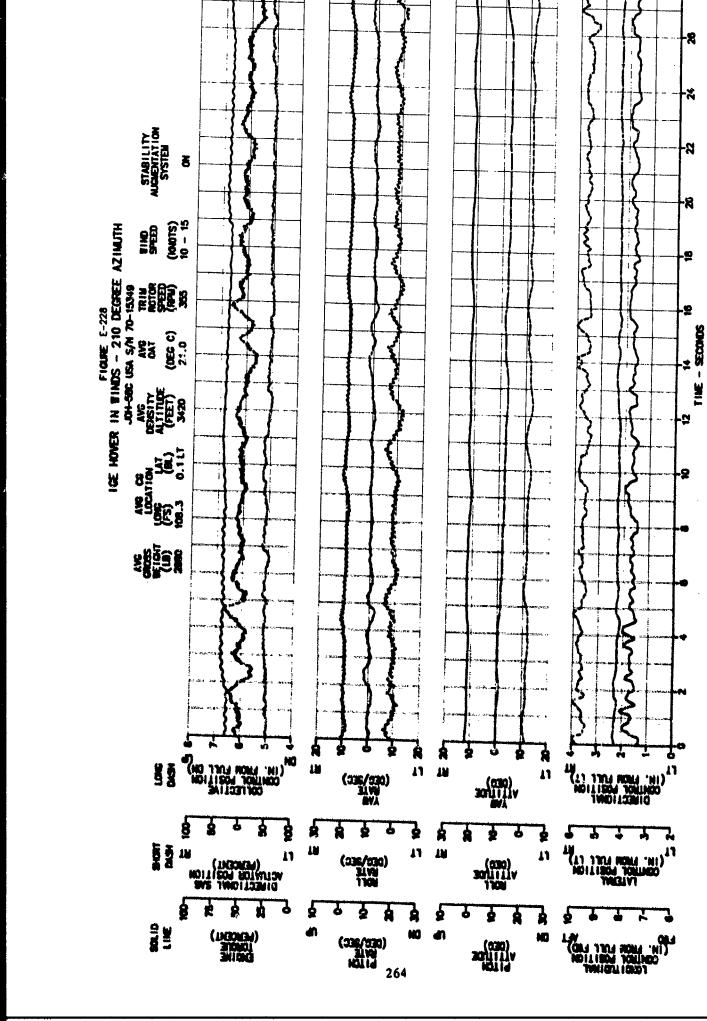


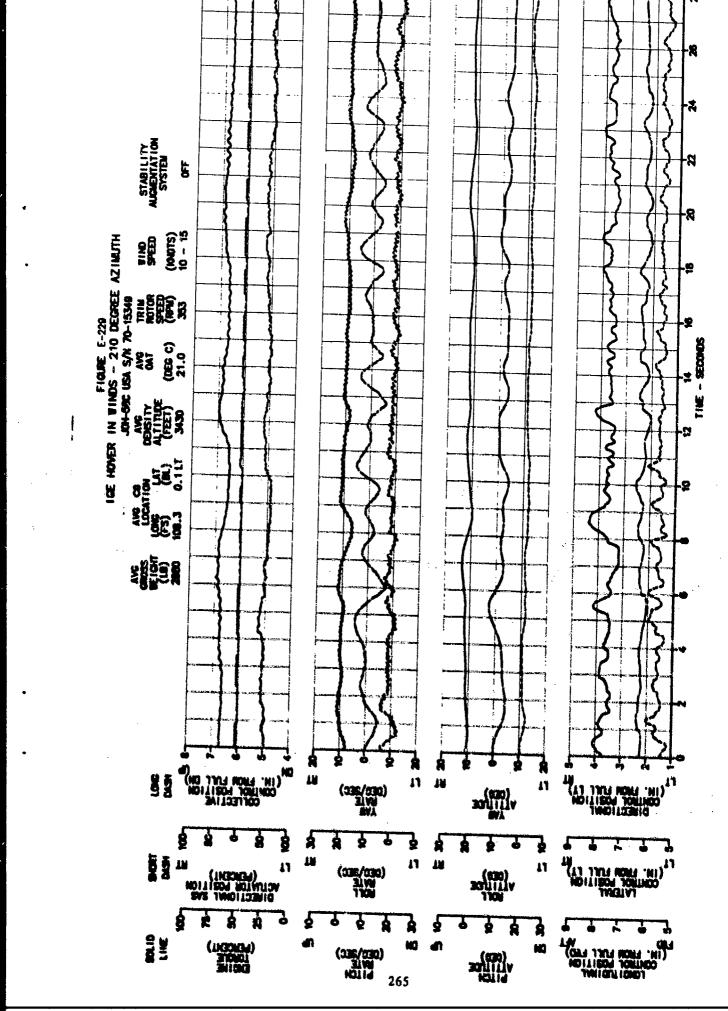


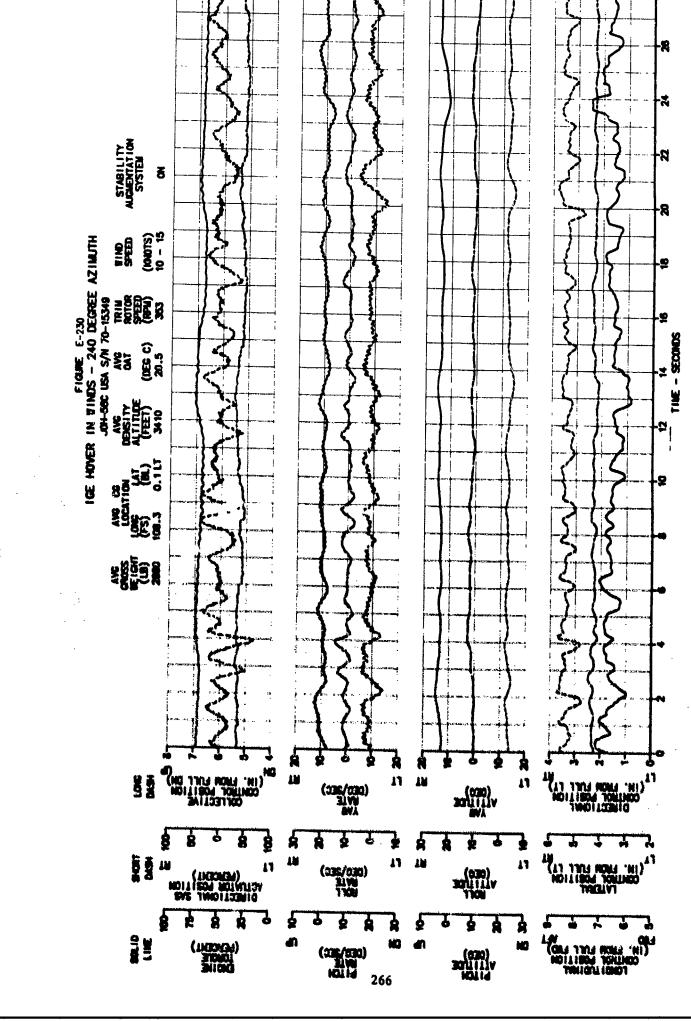


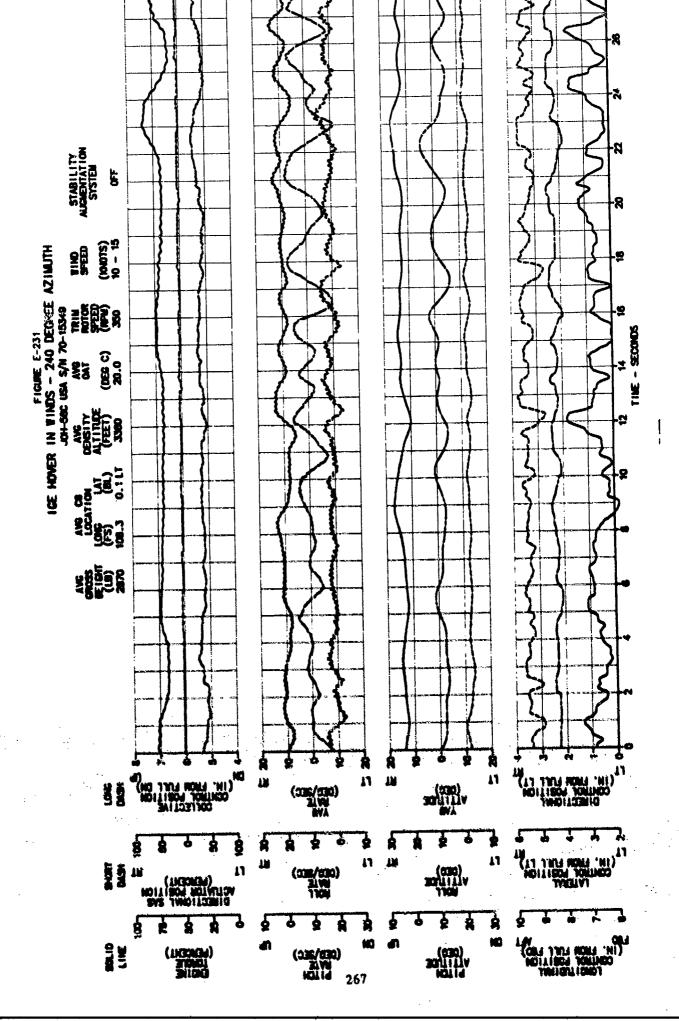


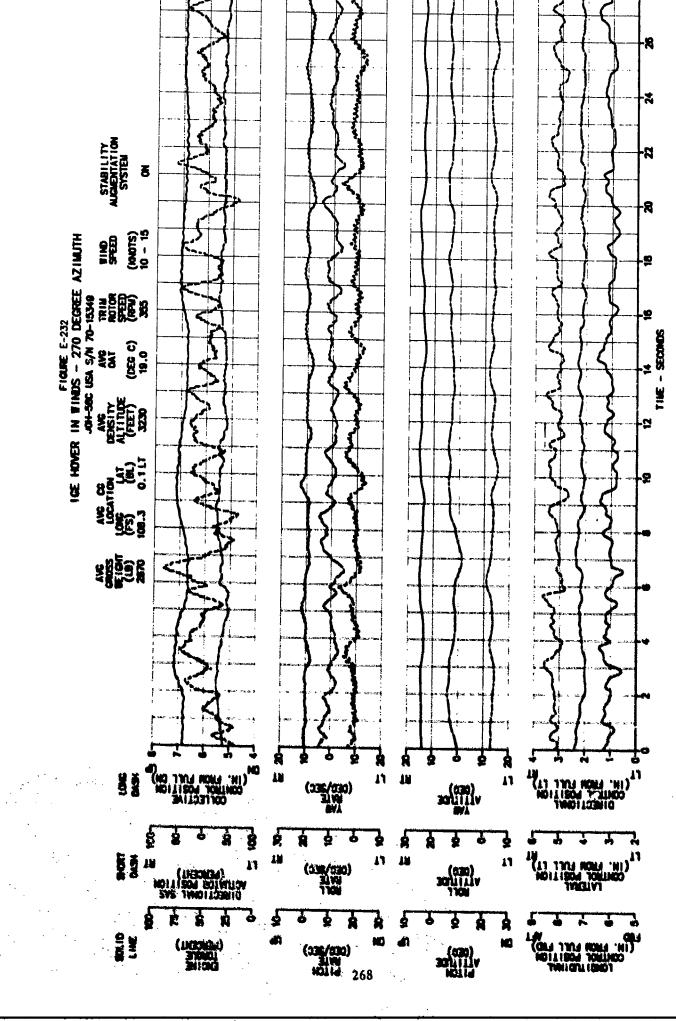


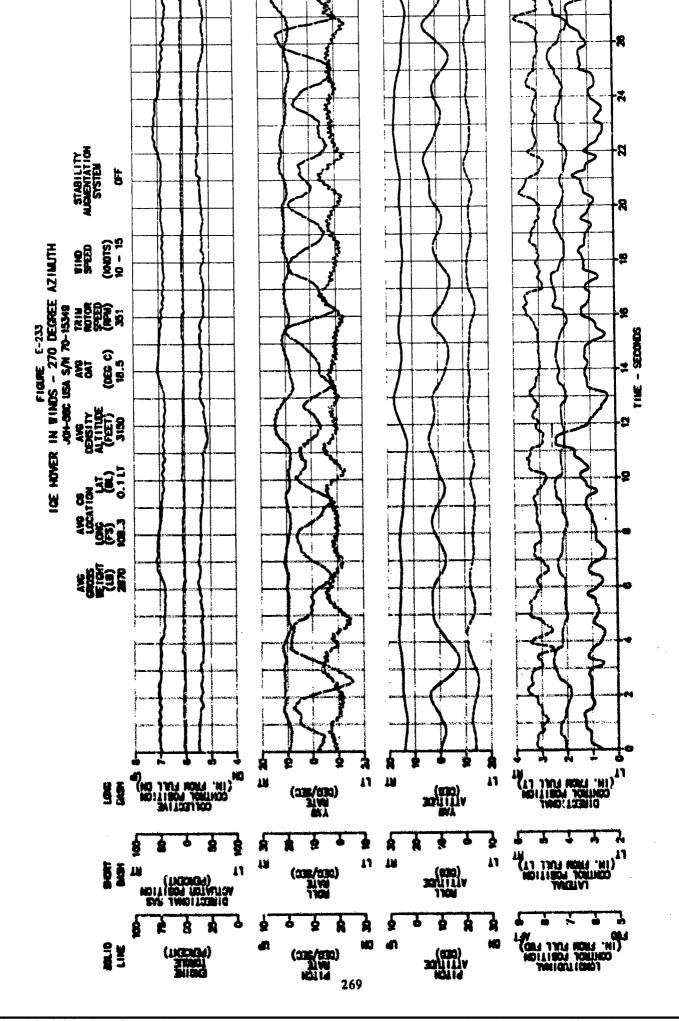


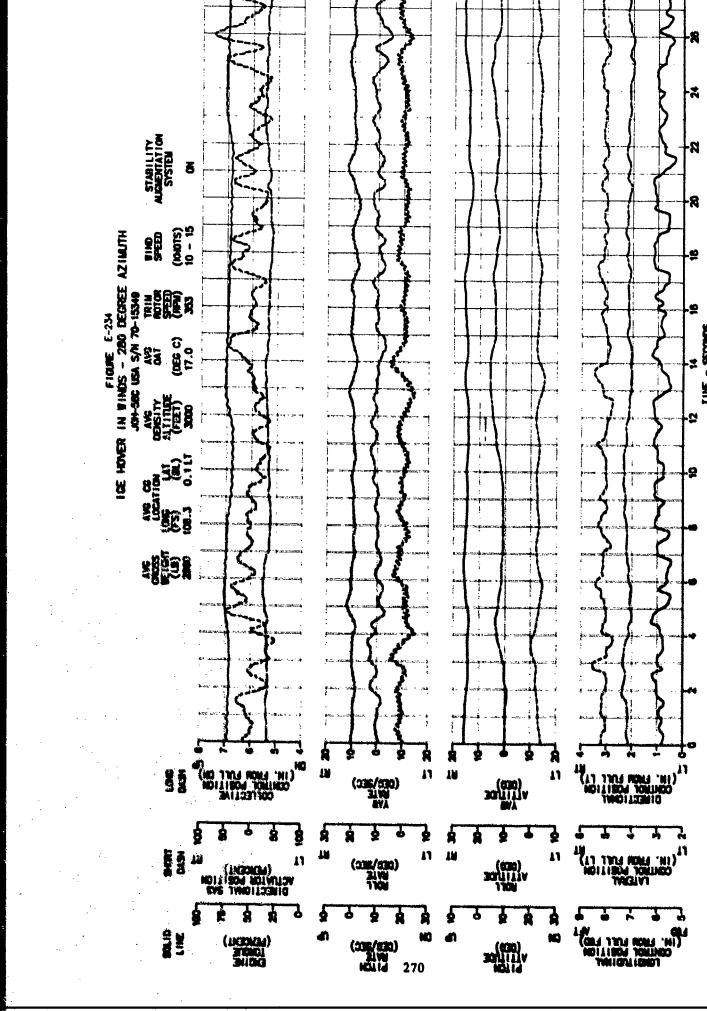


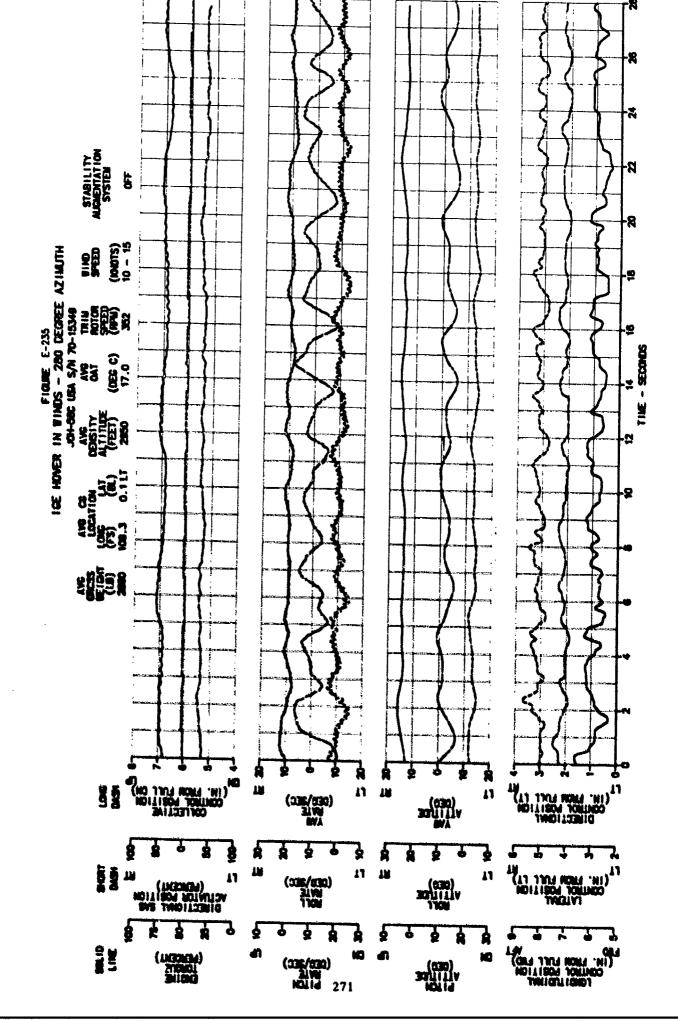


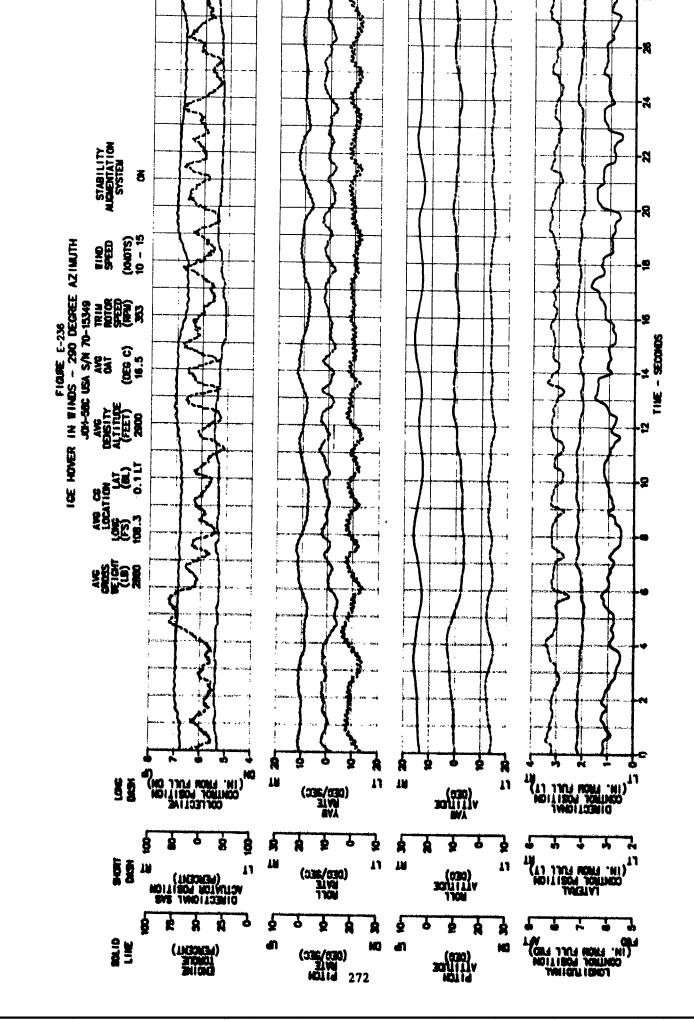


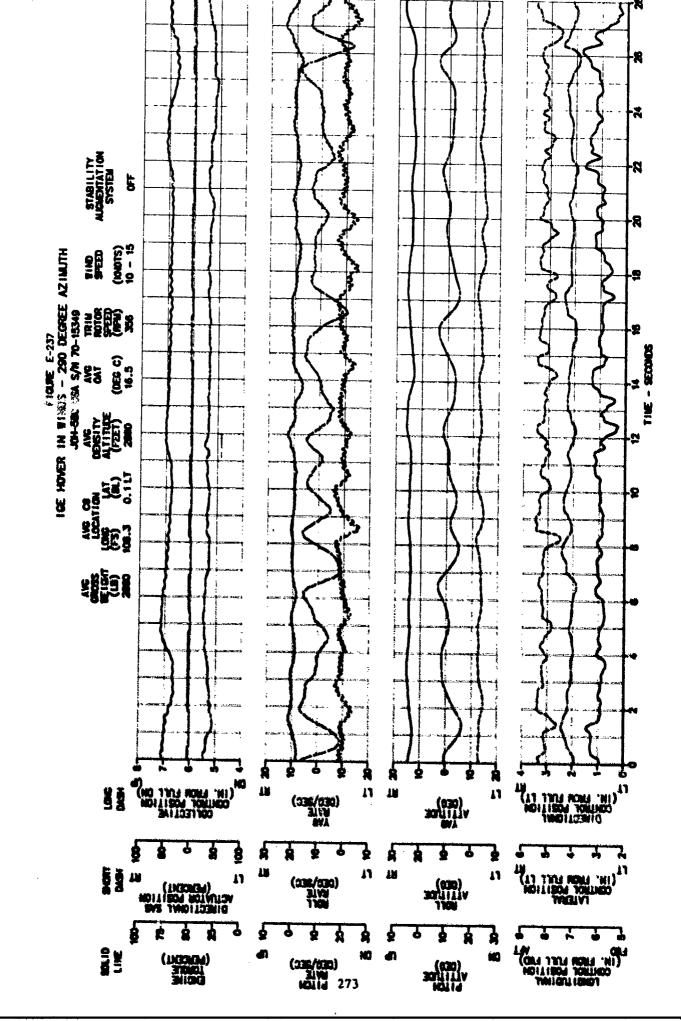


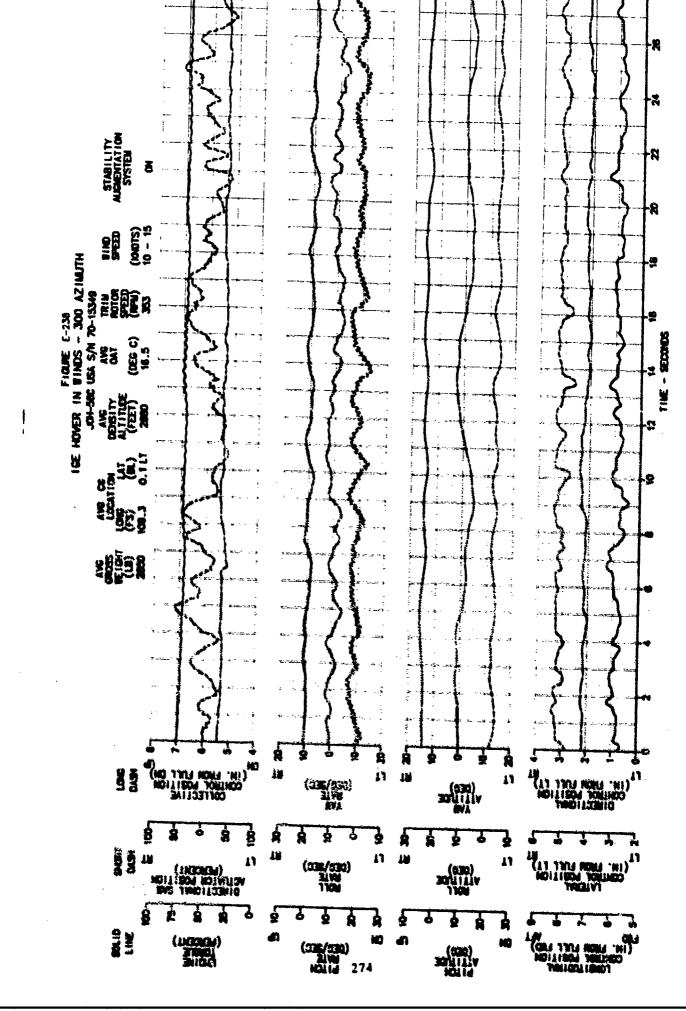


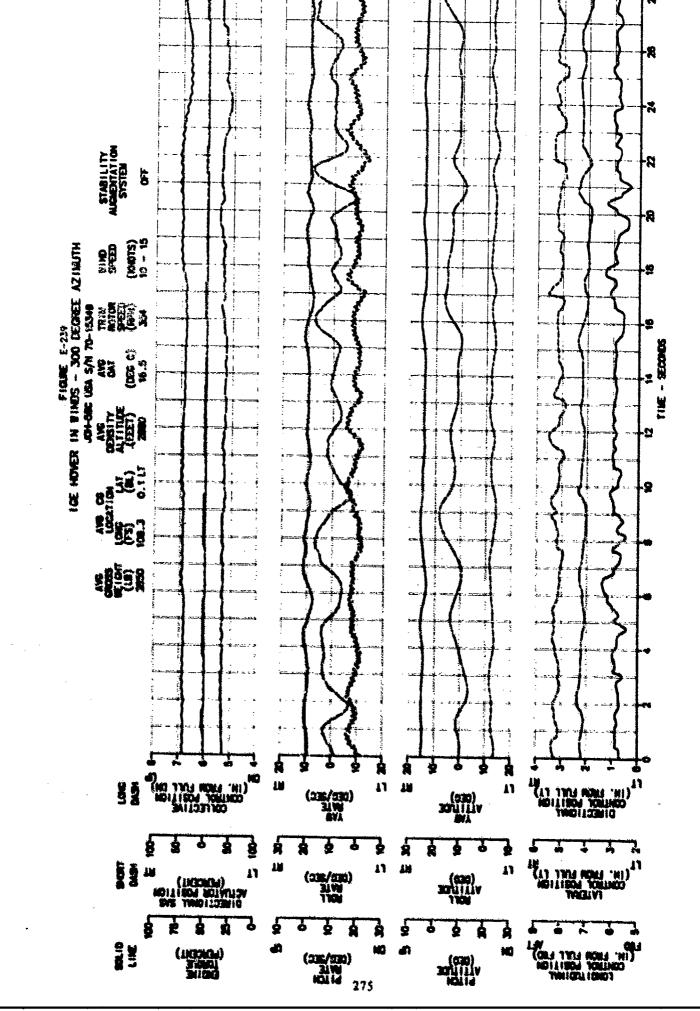


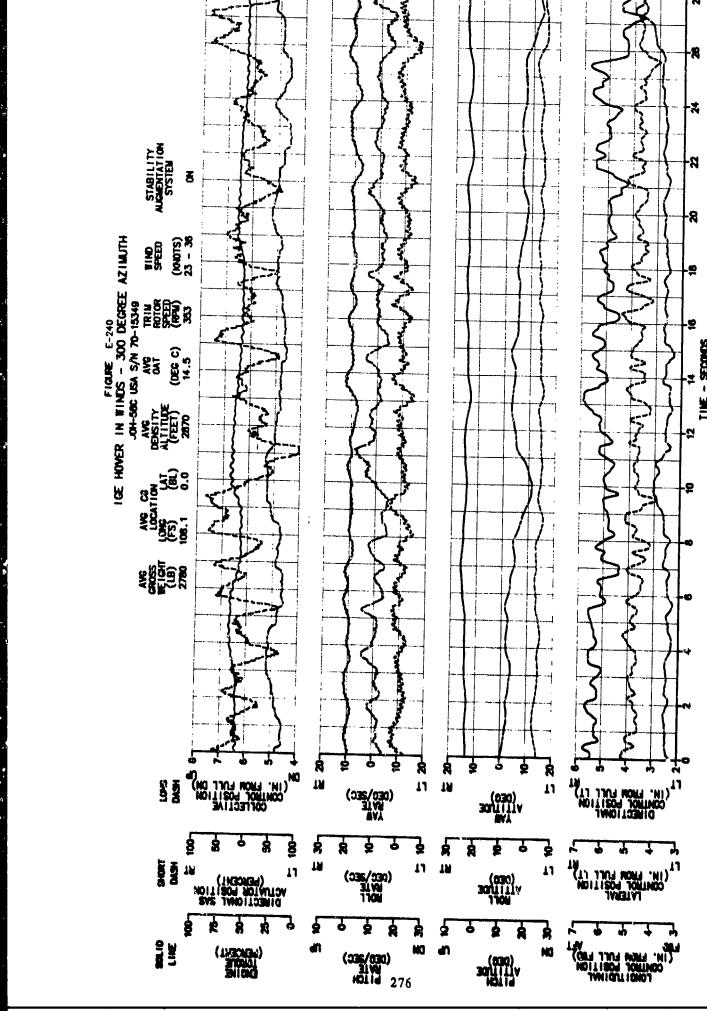


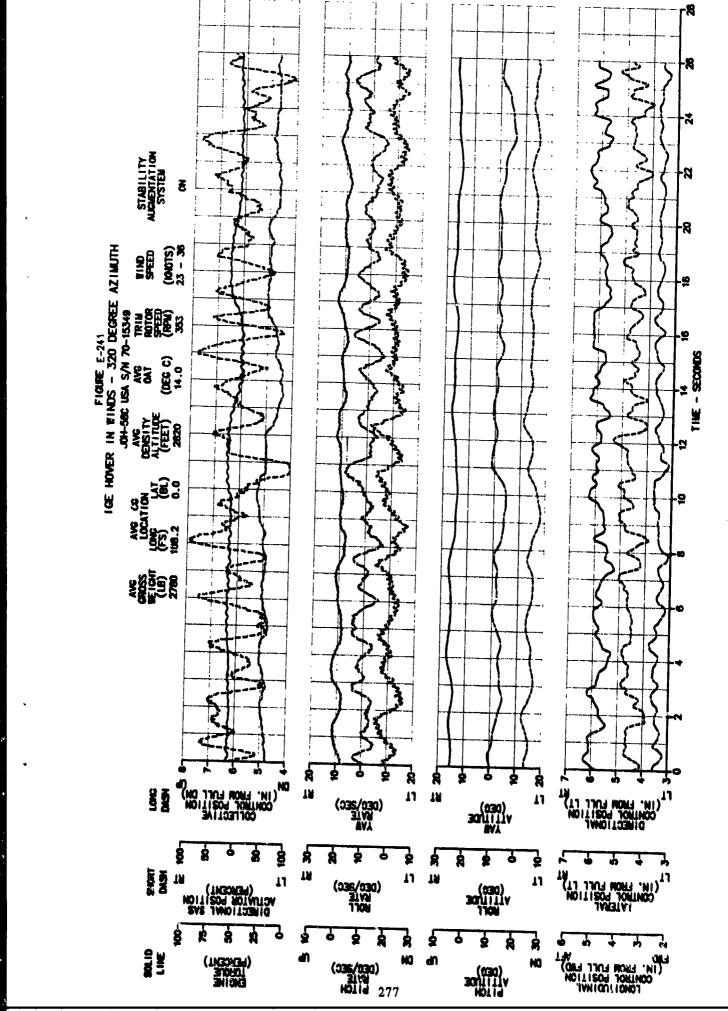


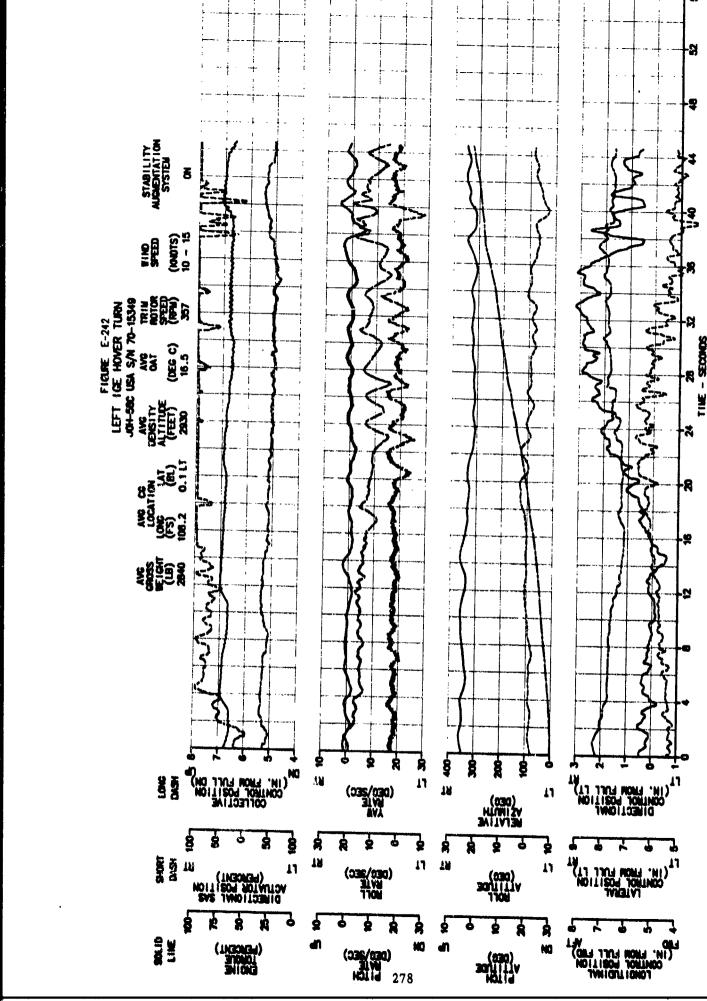


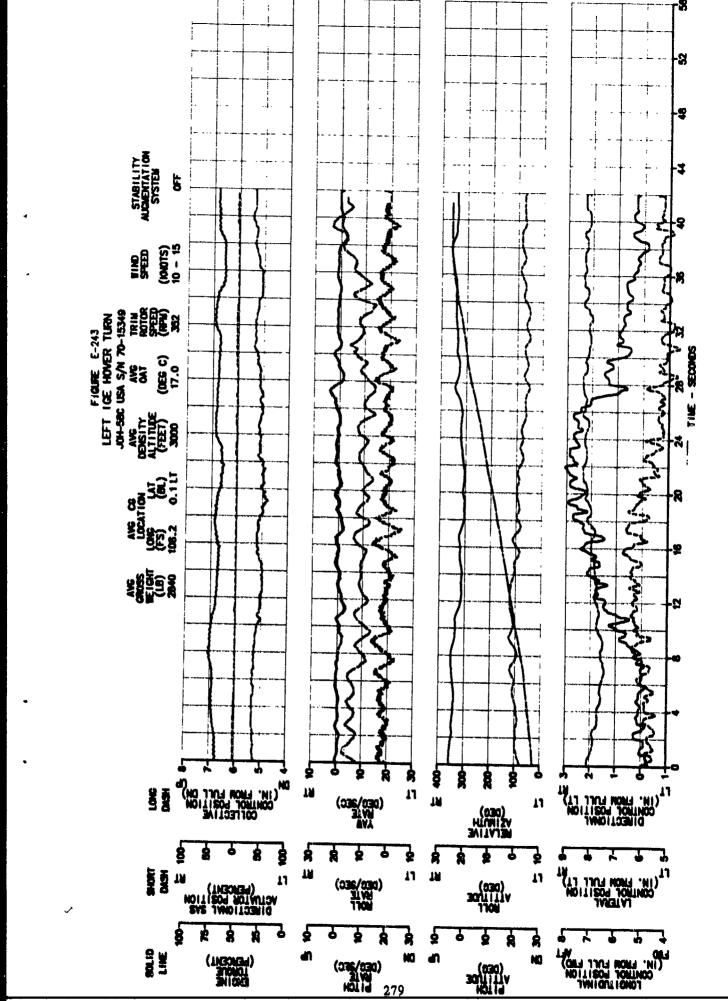


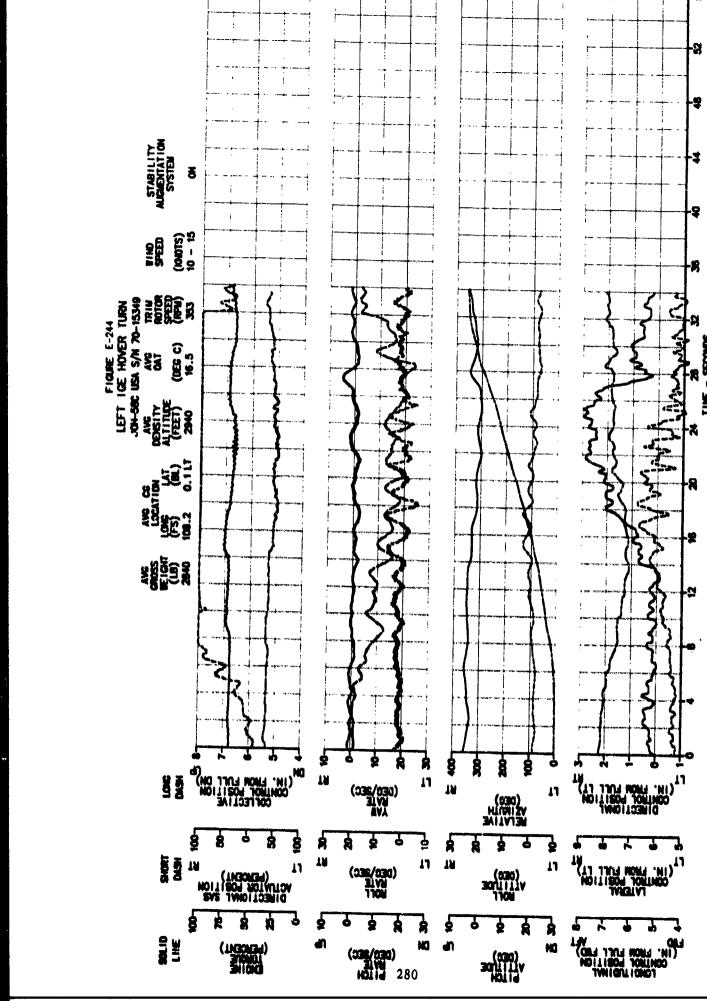


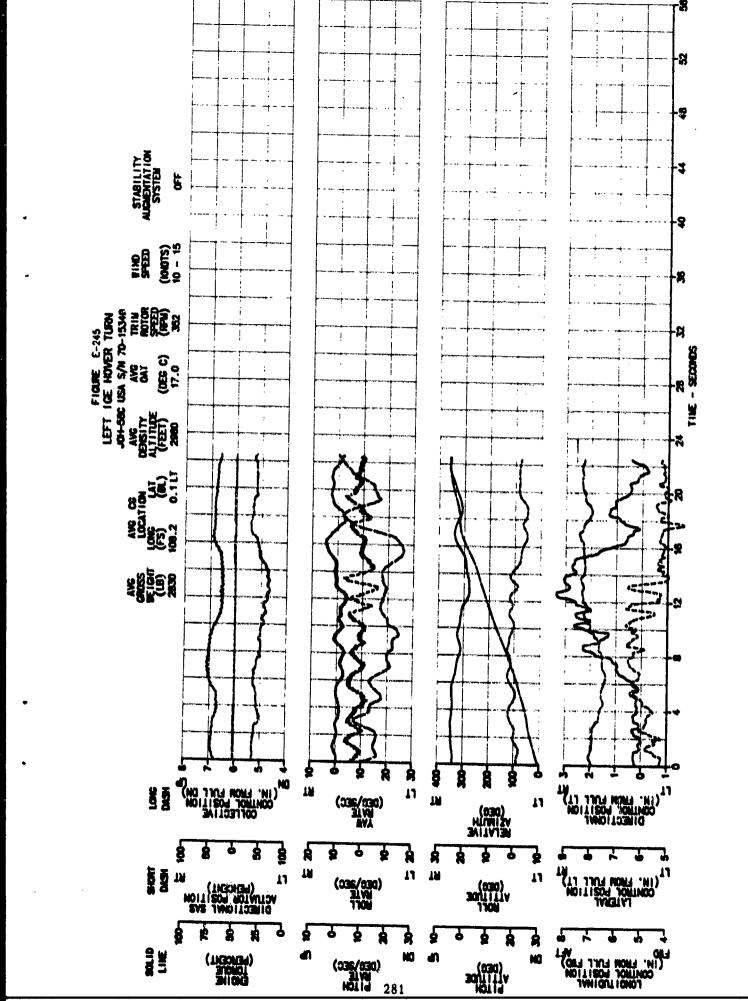


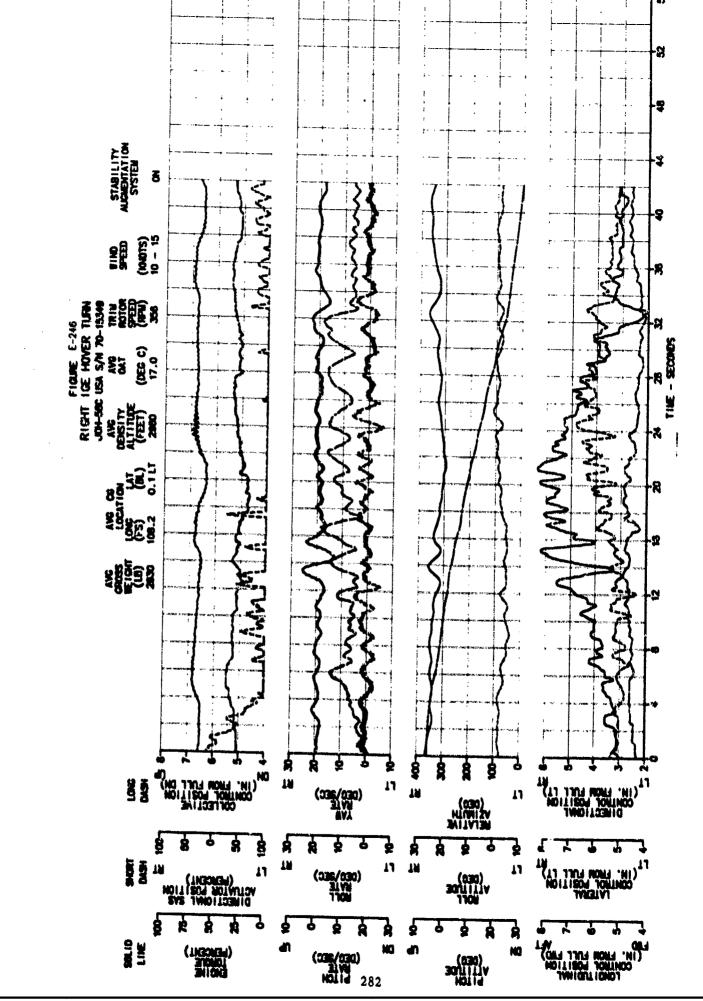


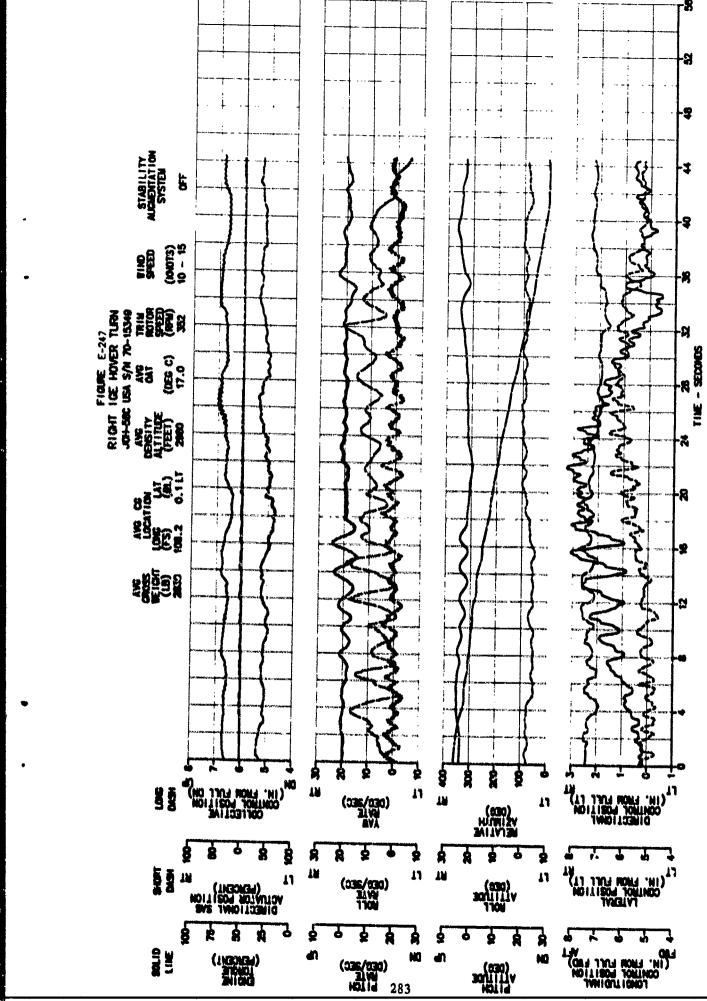


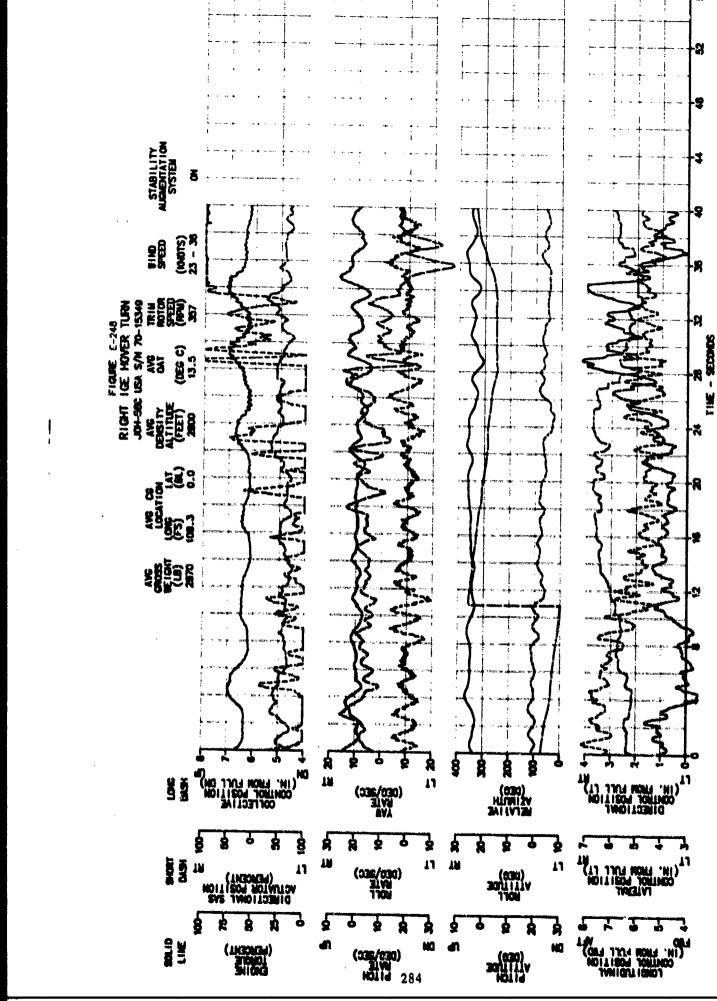


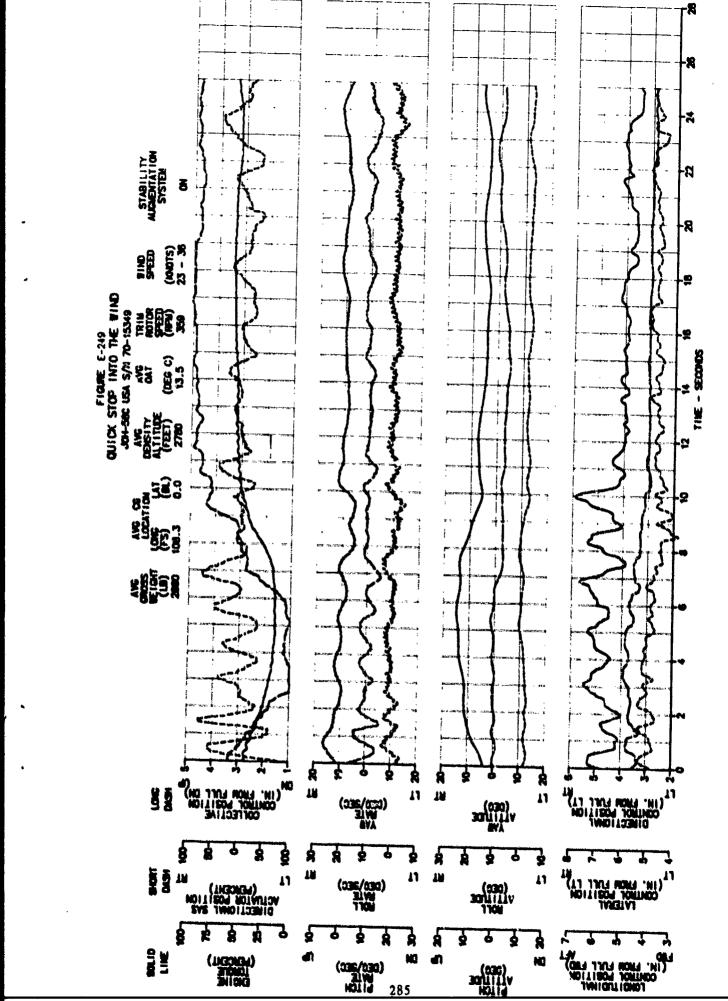


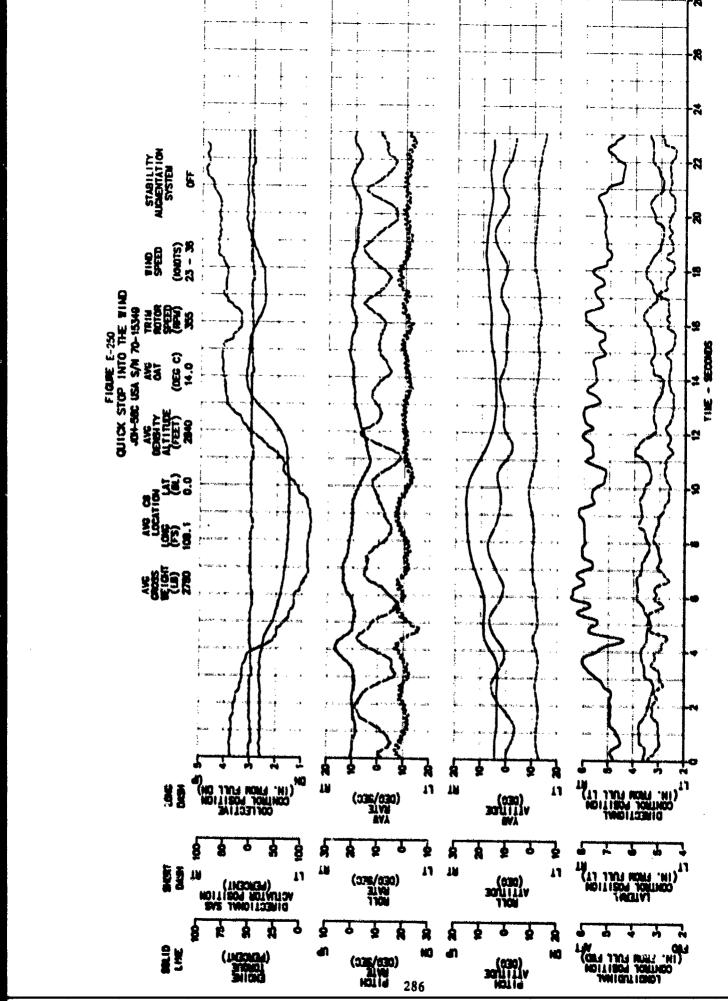


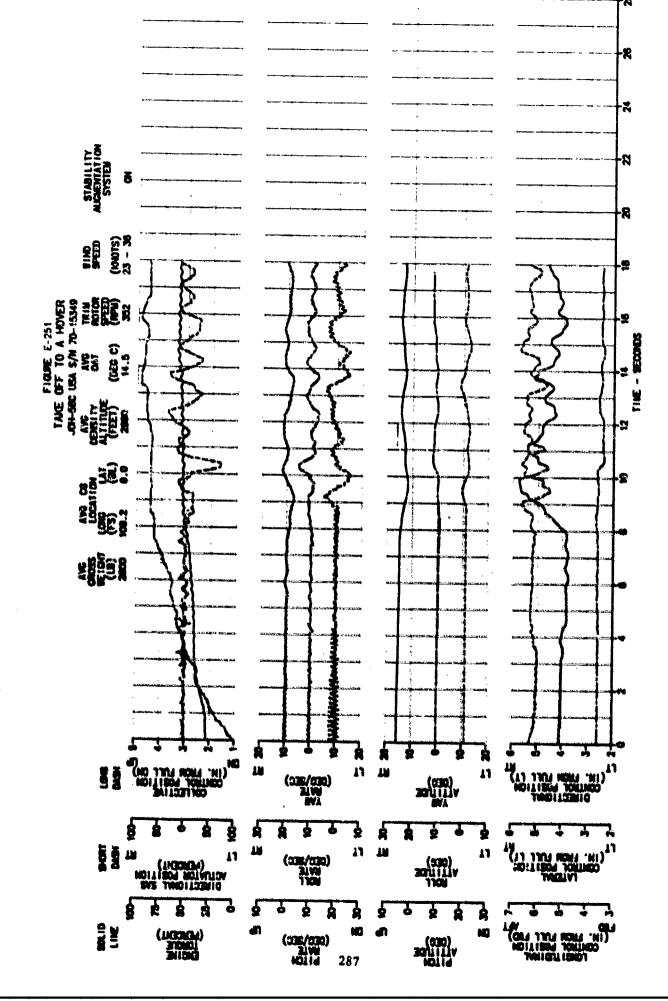


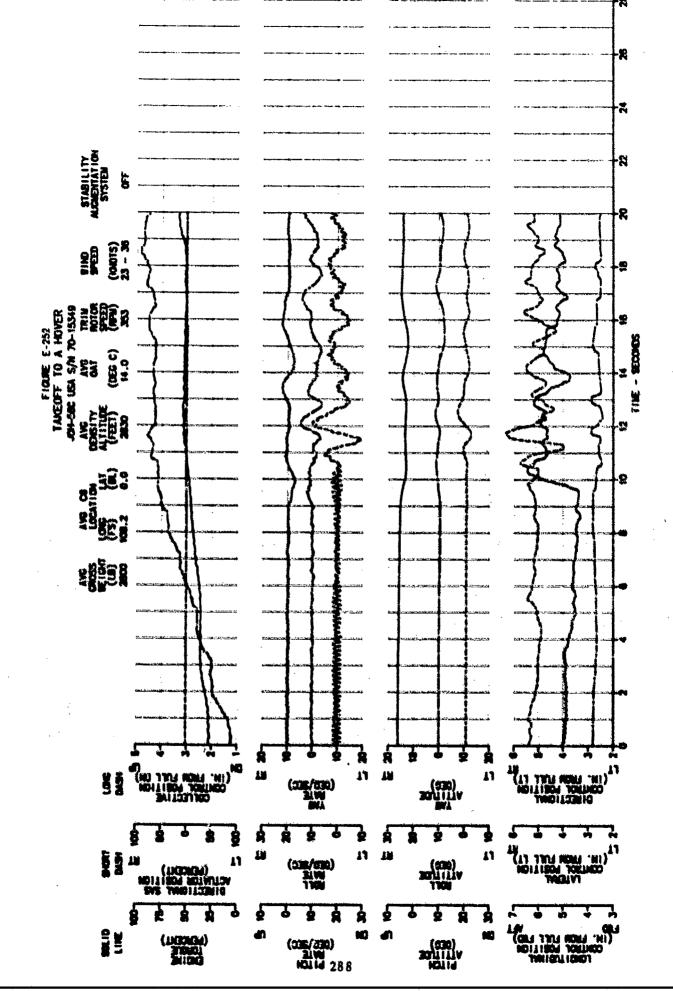


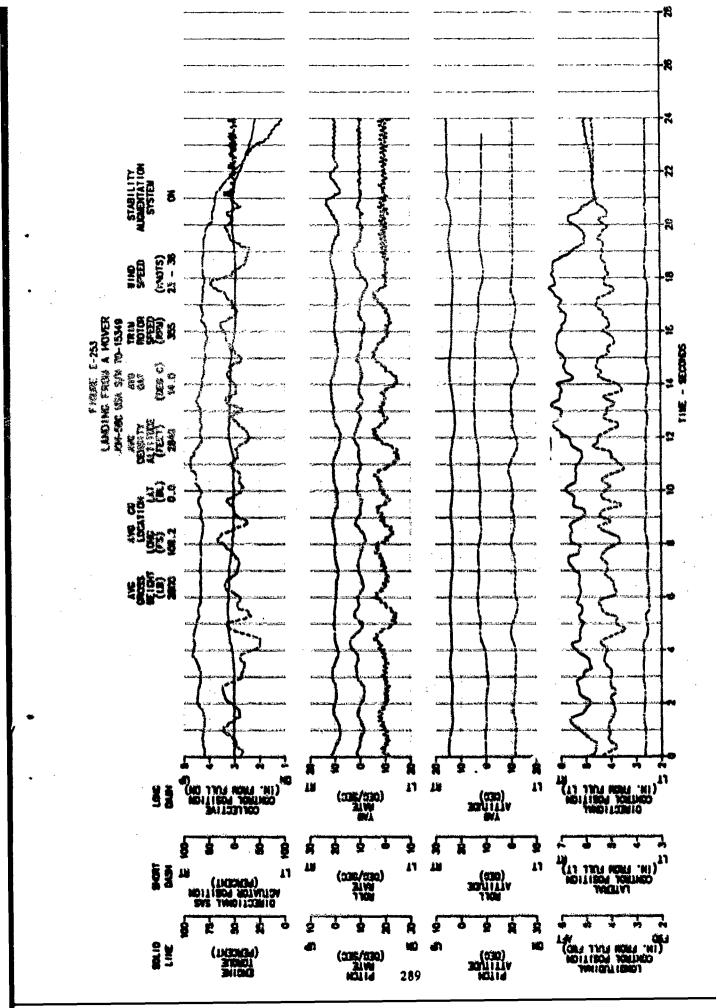












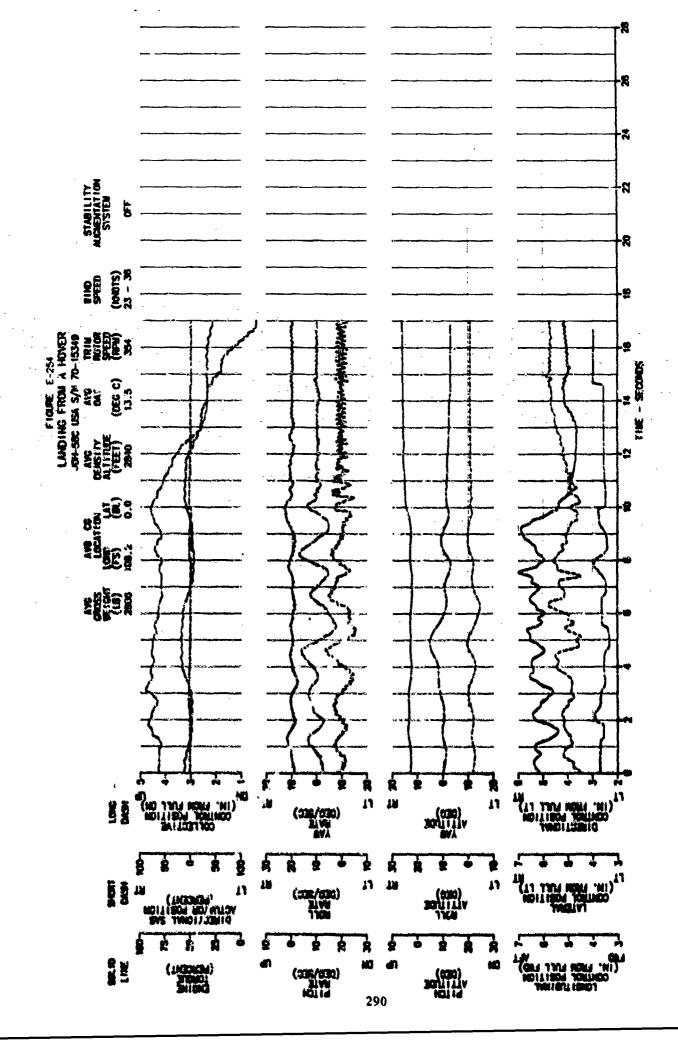


FIGURE E-255 SHIP SYSTEM AIRSPEED CALIBRATION JOH-58C USA S/N 70-15349

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